## JOSHUA HUMPHREYS NOTEBOOK



## 5/1/2015

Rosalie Stewart, Editor

The first 160 pages of Volume 1 of the Joshua Humphreys Papers,
"Principal Dimensions," are available for viewing at the Historical
Society of Pennsylvania website. The remainder are not online.
Additional materials of lesser quality that were also obtained from the Historical Society are still being transcribed.

Joshua Humphreys was born on June 17, 1751, in Haverford, Pennsylvania, to Joshua Humphreys (Sr.) and Sarah (Williams) Humphreys, who owned large amounts of land in Delaware County. In Humphreys' youth, he became a ship carpenter's apprentice in Philadelphia, and after the death of the master, Humphreys was given control of the ship yard. His later creation of his own ship yard made him well-known in the colonies as a naval architect, and he was commissioned by the U. S. government in 1776 to build ships in Philadelphia and prepare them for the Revolutionary War.

After the war, Humphreys was again commissioned by the federal government to build a naval fleet to protect the country from pirates and other attacking ships. These ships needed to be as high quality as those of other European countries, though the fleet would be much smaller. Humphreys made some key changes to improve six frigates that became the foundation of the American Navy. His designs and modifications were approved by the government, and in 1794 he was formally appointed as naval constructor, with the charge to design the frigates. Only the United States was built in Philadelphia under his supervision. All of the ships, however, included the modifications suggested by Humphreys, and became known for their speed and efficiency.

By 1801, the government no longer needed a formal naval constructor, and Humphreys was given the task to build a ship yard for use by the Navy in Philadelphia. He began to participate politically in the city, and was considered a very successful businessman in Philadelphia. Joshua Humphreys' brother Charles was a member of the Continental Congress; his son Samuel was also a naval architect, and worked with the federal government after Joshua Humphreys resigned; and his grandson Andrew Atkinson Humphreys served as a general during the American Civil War. Joshua Humphreys died on January 12, 1838.

The originals are in the collection of The Historical Society of Pennsylvania - see http://www2.hsp.org/collections/manuscripts/h/Humphreys306.html for a description of the collection.

The image below shows a typical example of what we were working with.


Transcription was a team effort by numerous members of the ModelShipbuilder forum, including 42rocker, aew, daves, Winston, bbrockel, Larry_D, Pete38, Michael Mott, Grant Dale, Maurius Meiring, Tim C, garyshipwright, dbharmon64 and Norman (sorry if I missed anyone!)

Individual scans were transcribed, then Rosalie Stewart compiled the transcriptions into a common look and feel, worked to resolve uncertainties, and now, ready for the public, the first set is being published via the ModelShipbuilder Forum. Future efforts may include working through the information at the Papers of the War Department project website (http://wardepartmentpapers.org/) to fill in more of the details around the work of Humphreys between 1784 and 1800.

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Deptford November the 7th
Principal Dimentions \& Scantlings \&c.
Of a Ship of each Class Proposed to be Established in Obedience to the Rt. Honourable the Navy Boards Warrants;
Dated the 5 of June last 1719

| Principal Dimentions |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
|  |  |  | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| Length of keel for tonnage |  |  | 140-7 | 132-5 | 128-2 | 123-2 | 117-7 | 109-8 | 101-8 | 93-8 | 87-5 |
| On the gundeck from the rabit of the stern to the rabit of the post Breadth extream |  |  | 174 | 161 | 158 | 151 | 144 | 131 | 121 | 114 | 106 |
|  |  |  |  |  |  |  |  |  |  |  |  |
| At the aftermost part of the main at wing transom from the out to the |  |  |  |  |  |  |  |  |  |  |  |
| outside of the plank - - | - - - | - | 50-0 | 47-2 | 44-6 | 41-6 | 39-0 | 36-0 | 33-2 | 30-6 | 28-4 |
| At the top of the timber line from the out to the outside of the plank | afore | - | 28-10 | 27-2 | 25-7 | 23-10 | 22-4 | 20-8 | 19-0 | 17-4 | 16-2 |
|  | Midships | - | 32-21/2 | 30-4 | 28-8 | 26-9 | 22-51/4 | 19-8 | 18-11/4 | 16-11 | - |
|  | Abaft | - | $1-71 / 2$ | $1-6^{1 / 2}$ | $1-5^{1 / 2}$ | 1-5 | 1-5 | $1-41 / 2$ | 1-4 | $1-31 / 2$ | 1-3 |
| Of the stem at the fifth rail abaft | From out to out | - | 20-6 | 19-31/2 | 18-2 | 17-8 | 17-0 | 15-11 | 14-10 | 13-8 | 13-0 |
|  | Side of the plank | - | 18-5 | 17-10 | 17-3 | 16-4 | 18-8 | 14-11 | 13-11 | 12-11 | 12-9 |
| Height of the cutting down in the $\square \square$ above the keel | - - | - | $1-71 / 2$ | 1-61/2 | $1-51 / 2$ | 1-5 | 1-5 | $1-41 / 2$ | 1-4 | $1-31 / 2$ | 1-3 |
| The top timber line or upper edge of the waist rail above the bottom of the false keel | Afore <br> Midships <br> Abaft |  | 47-71/2 | 45-8 | 43-6 | 35-3 | 33-111/2 | $31-01 / 2$ | 30-2 | 26-9 | 23-4 |
|  |  |  | 44-43/4 | 42-31/2 | 40-83/4 | $32-111 / 2$ | 31-31/4 | 29-71/2 | 27-101/2 | 25-03/4 | 21-43/4 |
|  |  |  | 55-61/2 | 52-4 | 50-6 | 41-9 | $39-11^{1 / 2}$ | $36-11^{1 / 2}$ | 34-5 | 30-9 | 26-5 |
| Rising of the midships flat |  |  | 0-5 | 0-5 | 0-5 | 0-5 | 0-6 | 0-7 | 0-8 | 0-9 | 0-10 |
| Depth of the hole taken from the strake, next the limber bords |  |  | 20-0 | 18-10 | 18-2 | 17-4 | 16-5 | 15-2 | 14-0 | 12-0 | 9-2 |

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| Strake next ye Limber Boards Thick Broad if can be | 0-8 | 0-73/4 | 0-7 | 0-7 | 0-6 | 0-6 | 0-6 | 0-5 | 0-5 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1-3 | 1-3 | $1-2^{1 / 2}$ | 1-21/2 | 1-2 | 1-2 | 1-1 | 1-1 | 1-0 |
| Burthen in Tons | 186949/94156684/941350 |  |  | 1898 ${ }^{29}$ /94 $95121^{27}$ /94 |  | 75589/94 | $59456 / 9446341 / 94$ |  | $37449 / 94$ |
| Draught of Water Afore | 21-6 | 20-2 | 19-0 | 17-7 | 16-6 | 15-3 | 13-10 | 12-11 | 11-1 |
| Abaft | 22-10 | 21-6 | 20-4 | 18-11 | 17-11 | 16-5 | 14-10 | 13-11 | 12-4 |
| $\text { Orlope } \quad\left\{\begin{array}{l} \text { Beams to round-Two Inches in all Ships } \\ \text { Height from the Upper edge of the beam to the gundeck plank } \\ \text { at the Middle of the beam } \end{array}\right.$ | 6-6 | 6-3 | 6-1 | 5-11 | 5-9 | 5-7 | 5-6 | 5-4 | 5-4 |
| Platform $\left\{\begin{array}{c}\text { abaft } \\ \text { afore }\end{array}\right\} \quad$ height between Plank \& plank | $\begin{aligned} & 6-2 \\ & 6-6 \end{aligned}$ | $\begin{gathered} 6-7 \\ 6-3 \end{gathered}$ | $\begin{gathered} 6-5 \\ 6-1 \end{gathered}$ | $\begin{aligned} & 6-4 \\ & 5-11 \end{aligned}$ | $\begin{aligned} & 6-3 \\ & 5-9 \end{aligned}$ | $\begin{gathered} 6-1 \\ 5-7 \end{gathered}$ | $\begin{aligned} & 6-0 \\ & 5-6 \end{aligned}$ | $\begin{aligned} & 5-11 \\ & 5-4 \end{aligned}$ | $\begin{aligned} & 5-0 \\ & 5-4 \end{aligned}$ |
| Gundeck $\left\{\begin{array}{l}\text { Beams to Round } \\ \text { Plank Thick }\end{array}\right.$ | $\begin{aligned} & 0-5 \\ & 0-4 \end{aligned}$ | $\begin{gathered} 0-43 / 4 \\ 0-4 \end{gathered}$ | $\begin{gathered} 0-4^{1 / 2} \\ 0-3^{1 / 2} \end{gathered}$ | $\begin{aligned} & 0-4^{1 / 4} \\ & 0-3^{1 / 4} \end{aligned}$ | $\begin{aligned} & 0-4 \\ & 0-3 \end{aligned}$ | $\begin{aligned} & 0-3^{3} / 4 \\ & 0-3 \end{aligned}$ | $\begin{aligned} & 0-3^{1 / 2} \\ & 0-2^{1 / 2} \end{aligned}$ | $\begin{aligned} & 0-3^{1 / 4} 4 \\ & 0-2 \end{aligned}$ | $\begin{aligned} & 0-3 \\ & 0-11 / 2 \end{aligned}$ |
|  | $7-2$ $2-4$ $4-51 / 2$ | $\begin{aligned} & 7-0 \\ & 2-4 \\ & 4-5^{1 ⁄ 2} 2 \end{aligned}$ | $6-11$ $2-4$ $4-81 / 2$ | $6-11$ $2-3$ $5-0$ | $6-10$ $2-3$ $5-0$ | $6-91 / 2$ $2-2$ | $6-6$ $1-11$ | $6-0$ $1-9$ | $6-9$ $1-4$ |
| Ports $\left\{\begin{array}{l}\text { Deep } \\ \text { Fore \& Aft }\end{array}\right.$ | $\begin{aligned} & 2-8 \\ & 3-0 \end{aligned}$ | $\begin{aligned} & 2-7 \\ & 2-9 \end{aligned}$ | $\begin{aligned} & 2-7 \\ & 2-9 \end{aligned}$ | $\begin{aligned} & 2-7 \\ & 2-9 \end{aligned}$ | $\begin{aligned} & 2-6 \\ & 2-6 \end{aligned}$ | $\begin{aligned} & 2-4 \\ & 2-5 \end{aligned}$ | $\begin{aligned} & 2-2 \\ & 52-4 \end{aligned}$ | $\begin{aligned} & 2-2 \\ & 2-4 \end{aligned}$ | $\begin{aligned} & 2-0 \\ & 2-4 \end{aligned}$ |
| Forecastle $\left\{\begin{array}{l}\text { Beams to round } \\ \text { Plank Thick }\end{array}\right.$ | 0-7 0-2 | 0-63/4 $0-2$ | $\begin{aligned} & 0-6^{1 / 2} \\ & 0-2 \\ & \text { Platfo } \end{aligned}$ | $0-61 / 4$ $0-2$ m | $0-6$ $0-2$ | $0-53 / 4$ $0-2$ | $0-51 / 2$ $0-2$ | $0-51 / 4$ $0-2$ | $\begin{aligned} & 0-5 \\ & 0-2 \end{aligned}$ |
| Long from $\mathrm{y}^{\mathrm{e}}$ foreside of the stantiants of the beek head | 36-3 | 31-7 | 10-4 | 31-6 | 26-6 | 26-6 | 21-9 | 20-0 | ?- ? |


| ¢ Beams to round | 0-8 | 0-71/2 | 0-71/4 | 0-7 | 0-63/4 | 0-61/2 | 0-61/4 | 0-6 | 0-6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Quarter Height from ye plank to upper edge round house beams in ye mid - afore | 6-8 | 6-6 | 6-2 | 6-5 | 6-5 | 5-5 | 4-8 | - - | - - |
| Deck $\quad$ Height from y ${ }^{\text {e }}$ plank to upper edge round house beams in $\mathrm{y}^{\mathrm{e}} \mathrm{mid}-\mathrm{abaft}$ | 6-10 | 6-8 | 6-4 | 6-7 | 6-7 | 5-7 | 4-10 | - - | - - |
| Height from ye plank to the port cells | 1-7 | 1-7 | 1-6 | 1-6 | 1-6 | 1-6 | - - | 1-6 | - - |
| Ports $\{$ Deep | 2-6 | 2-6 | 2-5 | 2-4 | 2-3 | 2-2 | - - | 2-2 | - - |
| ( Fore \& Aft | 2-9 | 2-8 | 2-7 | 2-6 | 2-5 | 2-4 | -- | 2-2 | - - |
| Long taken in the midships from the aft part of the stern timber | 79-0 | 79-0 | 66-3 | 68-6 | 62-0 | 56-6 | 45-3 | 43-0 | 16-9 |
| Round $\quad$ Beams to round | 0-9 | 0-81/2 | 0-81/2 | 0-81/2 | 0-81/2 | 0-8 | 0-8 | -- | -- |
| House \{ Plank thick | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | -- | - - |
| Round Height from the plank to the upper edge of the topgallant $\{$ Afore | 5-10 | - - | -- | -- | -- | -- | -- | -- | -- |
| House round house beams at middle of the beams $\{$ Abaft | 6-0 | -- | -- | -- | -- | -- | -- | -- | -- |
| Long taken in the midships from the aft of the stern timber | 45-0 | 42-7 | 16-2 | 34-3 | 32-0 | 10-6 | 8-6 | -- | -- |
| Hanging of the deck at the middle line | 2-1 | 1-11 | 1-10 | 1-9 | 1-8 | 1-7 | $1-51 / 2$ | 1-4 | 1-3 |
| Higher abaft than afore from the keel | 0-8 | 0-8 | 0-8 | 0-8 | 0-8 | 0-6 | 0-4 | 0-4 |  |
| ( Beams to Round | 0-7 | $0-63 / 4$ | 0-61/2 |  |  |  |  |  |  |
| Plank thick | 0-3 | 0-3 | 0-3 |  |  |  |  |  |  |
| Middle Height from the plank to the upper edge of the upper deck $\int$ Afore | 7-1 | 6-63/4 | 6-61/2 |  |  |  |  |  |  |
| Deck Beams at the middle of the beams $\quad\left\{\mathrm{Mid}^{\text {s }}\right.$ | -- | - - | - - |  |  |  |  |  |  |
| $\left\{\begin{array}{l}\text { a }\end{array}\right.$ | 7-3 | 7-0 | 6-9 |  |  |  |  |  |  |
| Height from the deck plank to the port cells | 2-2 | 2-2 | 1-11 |  |  |  |  |  |  |
| Ports: $\quad\{$ Deep | 2-9 | 2-8 | 2-8 |  |  |  |  |  |  |
| (Fore \& Aft | 3-3 | 3-1 | 2-11 |  |  |  |  |  |  |
| (Beams to Round | 0-8 | 0-73/4 | 0-71/2 | 0-71/4 | 0-7 | 0-63/4 | 0-61/2 | 0-61/4 | 0-6 |
| Plank thick | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-21/2 | 0-21/4 | 0-2 | 0-2 |

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The back of the false post to rake $21 / 2^{\prime \prime}$ in a foot and the upright of the stem three inches. The stem to rake forward above the gundeck to the top of it two inches in a foot
Scantling of the frame and beams

occasion should require. Mem ${ }^{\text {br }}$ to have always a piece of 4 inch plank at the bottom to preserve it from the storms

The floor and futtock timbers in the bearing of the ship to fill up the rooms and space especially for large ships if can conveniently be got
Floor timbers next the flat sided $\quad 1-2 \quad 1-2 \quad 1-1 \frac{1}{2} \quad 1-1 \frac{1}{4} \quad 1-1 \quad 1-0 \quad 0-11 \quad 0-10 \quad 0-9$
Afore and abaft next in wake of the half timbers

## Scantling of the Frame and Beams

At the wronghed $\square$ wronght in and out
Afore and abaft in \& out
Lower futtocks sided in the midships next the flats a small distance afore \& abaft the bearing of the ship
Sided afore \& abaft

| $1-2$ | $1-1^{1 / 4}$ | $1-03 / 4$ | $1-0$ | $0-11$ | $0-101 / 4$ | $0-10$ | $0-9$ | $0-8$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $1-1$ | $1-01 / 2$ | $0-11$ | $0-11$ | $0-10$ | $0-9$ | $0-8$ | $0-7$ | $0-6$ |
|  |  |  |  |  |  |  |  |  |
| $1-2$ | $1-2$ | $1-1^{1 / 2}$ | $1-1 \frac{1}{4}$ | $1-1$ | $1-0$ | $0-11$ | $0-10$ | $0-9$ |
| $1-0$ | $1-0$ | $0-11^{1 / 2} 2$ | $0-11^{1 / 4}$ | $0-11$ | $0-101 / 2$ | $0-10$ | $0-9$ | $0-8$ |

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| In and out at the heads in the midships |  |
| :---: | :---: |
| Second futtocks sided in the midships Afore and abaft |  |
| Third futtocks sided in the midships Afore and Abaft |  |
| Upper Futtocks sided in the midships Afore and abaft |  |
| At the gundeck in \& out in the Top timbers sided at the heel \& at the upper futtocks heads Heads |  |
| In and out at the top of the side |  |
| Orlope beams moulded Sided |  |
| Gundeck Beams | Sided in the midships and 1 inch less each way afore and afore <br> Moulded |
| Middle Deck Beams | Sided <br> Moulded |
| Upper Deck Beams | Sided <br> Moulded |
| Forecastle Beams | Sided <br> Moulded |


| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft -In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| 0-11 1 /2 | 0-11 | 0-101/4 | 0-10 | 0-9 | 0-8 | 0-7 | 0-6 | 0-5 |
| 1-11/2 | 1-11/2 | 1-1 | 1-03/4 | 1-01/2 | 0-111/4 | 0-101/2 | 0-91/2 | 0-81/2 |
| 0-11 $1 / 2$ | 0-111/2 | 0-11 | 0-103/4 | 0-101/2 | 0-10 | 0-91/2 | 0-81/2 | 0-71/2 |
| 1-1 | 1-1 | 1-01/2 | 1-01/4 | 1-0 | 0-11 | - - | - - | - - |
| 0-11 1 /2 | 0-111/2 | 0-11 | 0-103/4 | 0-101/2 | 0-91/2 | - - | - - | - - |
| 1-1 | 1-1 | 1-01/2 | 1-01/4 | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 |
| 0-11 1 /2 | 0-111/2 | 0-11 | 0-103/4 | 0-101/2 | 0-10 | 0-91/2 | 0-81/2 | 0-71/2 |
| 0-11 | 0-101/2 | 0-10 | 0-91/2 | 0-81/2 | 0-71/2 | 0-61/2 | 0-51/2 | 0-5 |
| 1-1 | 1-1 | $1-01 / 2$ | 1-01/4 | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 |
| 0-91/2 | 0-91/2 | 0-9 | 0-9 | 0-81/2 | 0-71/2 | 0-61/2 | 0-51/2 | 0-5 |
| 0-5 | 0-43/4 | 0-4 | - - | - - | - - | - - | - - | - - |
| 1-4 | 1-31/2 | 1-21/2 | 1-2 | 1-1 | 0-11 | 0-10 | 0-9 | - - |
| 1-4 | $1-31 / 2$ | 1-21/2 | 1-2 | 1-1 | 0-11 | 0-10 | 0-9 | - - |
| 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-10 | 0-8 |
| 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-11 | 0-9 | 0-7 |
| 1-3 | 1-2 | 1-1 | -- | -- | -- | -- | -- | -- |
| 1-1 | 1-0 | 0-11 | -- | -- | -- | -- | -- | -- |
| 1-1 | 1-01/2 | 0-11 | 0-11 | 1-0 | 0-101/2 | 0-91/2 | 0-9 | 0-81/2 |
| 0-11 | 0-101/2 | 0-81/2 | 0-11 | 0-10 | 0-81/2 | 0-71/2 | 0-7 | 0-6 |
| 0-91/2 | 0-91/2 | 0-8 | 0-9 | 0-8 | 0-61/2 | 0-6 | 0-6 | 0-51/2 |
| 0-71/2 | 0-7 | 0-6 | 0-7 | 0-6 | 0-51/2 | 0-5 | 0-5 | 0-41/2 |


| Beams at the forepart of the Forecastle <br> To fasten the cattheads | Sided <br> Moulded |
| :--- | :--- |
| Roundhouse Beams $\quad$Sided <br> Moulded |  |
| Top Gallant Roundhouse Beams | Sided <br> Moulded |


| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft -In | Ft -In | Ft-In | Ft-In |
| 2-6 | 2-5 | 2-4 | 2-3 | 2-2 | 2-0 | 1-10 | 1-9 | 1-2 |
| 0-71/2 | 0-7 | 0-7 | 0-7 | 0-6 | 0-51/2 | 0-5 | 0-5 | 0-5 |
| 0-71/2 | 0-7 | 0-6 | 0-61/2 | 0-61/4 | 0-41/2 | 0-4 | - - | - - |
| 0-51/2 | 0-41/2 | 0-5 | 0-5 | 0-31/2 | 0-3 | - - | - - | - - |
| 0-6 | - - | - - | - - | - - | - - | - - | - - | - - |
| 0-41/2 | - - | - - | - - | - - | - - | - - | - - | - - |

To Determine the Burthen in Tons

First instead of measuring from the back of the main post to the perpendicular or square from the keel at the fore part of the stern at the top thereof, or from a square or a perpendicular from the keel at the fore part of the stern at the upper edge of the lower harpen as hath been usual, both which extreams are liable to many uncertaintizs \& may be considerable vareed by increasing or lessening the main or false post without the rabit abaft, or by raiseing or lowering the harpin, the raking the upper post of the stern more or less or adding or diminishing to the scantlings of the same before the rabit of the stern, none of which are essentials for determining the tunage. Therefore instead thereof erect a square or perpendicular from a line ranging straight with the low'r part of the rabit of the keel to the aft part of the plank or at the upper edge of $y^{e}$ wing transom and also another square or perpendicular from the fore part of the plank or rabbit of the stern at ${ }^{5 / 6}$ parts off the height of the wing transom, then measure the length between those perpendicular lines and add thereto $1 / 24$ of the extream breadth (for the scantlings of the stern before the post abaft the plank without regarding wether there be a fals post or no) from which sum subtract $6 / 25$ of the heigh of the wing transom(for the rake Abaft $)^{3 / 5}$ of the main breadth for the rake forward, and the residue is to be accounted the length for tunage, which multiply by the extream breadth and the product by the $1 / 2$ breadth and that sum divided by 94 give the burthen in tons. This is for square stern ships, but for round stern vessels (or where there is no Wing Transom) off $3 / 5$ of the extream breadth from the lower part of the rabbit of the keel on the aft part of the rabbit of the post from suppos'd height of the wing transom from whence the perpendicular is to be let fall as before from the wing transom. Ye other forward let fall from the fore part of the rabbit of the stern at $15 / 6$ parts of the height \& then to take $y^{e}$ distance of those two perpendiculars and work from them as before directed in square stern ships.

The extream Breadth is taken from the outside to the outside of the thick stuff either or below the wales where the ship shall be broadest always deducting the doubling or sheathing from the said breadth.

## Joshua Humphreys Notebook



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| Abaft the rabbit at the wing transom | 0-11 | 0-10 | 0-9 | 0-8 | 0-71/4 | 0-7 | 0-61/4 | 0-6 | 0-51/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| False the back of it abaft the rabbit of the keel | 2-1 | 2-0 | 1-11 | 1-10 | 1-9 | 1-7 | 1-6 | 1-5 | 1-4 |
| The inner part for \& aft ye top end upwards | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 |
| Fore \& aft on the keel (if can be had) | 1-8 | 1-7 | 1-6 | 1-5 | 1-4 | 1-3 | 1-1 | 0-11 | 0-9 |
| Transom wing sided | 1-3 | 1-2 | 1-11/2 | 1-1 | $1-0^{1 / 2}$ | 1-0 | 0-11 1 /2 | -11 | 0-101/2 |
| Moulded at the ends | 1-8 | 1-7 | 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 |
| Deck transom to lye close to the gundeck for the plank |  |  |  |  |  |  |  |  |  |
| Sided | 1-2 | 1-1 | $1-0^{1 / 2}$ | 1-0 | 0-111/2 | 0-11 | 0-10 | 0-9 | 0-81/2 |

Deck transom moulded as broad as conveniently may be for the better fastening of the plank of the said deck; between the wing \& deck so wide as to leave 2 or $2^{1 ⁄ 2}$ in. air between the wing transom and the gundeck plank.

## Parts of the Frame

Transom under the deck
Transome $\left\{\begin{array}{l}1 \\ 2 \\ 3\end{array}\right\} \quad$ not less than
Half transoms to lye clear of the whole transom not less than 3 inch for air
Raising wood as sufficient number of pieces afore \& abaft

Abaft (if a short piece of keel) to over launch the scarphs at least 6 foot, if a long piece of keel to drop short of the scarphs 8 foot

Broad in the midships 3 in on each side more than the keel (if can be had)

| Knee against ye post upon the lower piece of deadwood, length of the up \& down arm | $7-0$ | $6-6$ | $6-0$ | $5-6$ | $5-0$ | $5-0$ | $4-6$ | $4-0$ | $4-0$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Fore \& Aft arm (if can be had | $9-0$ | $8-6$ | $8-0$ | $7-6$ | $7-0$ | $6-6$ | $6-0$ | $5-6$ | $5-0$ |

## Joshua Humphreys Notebook

Distance apart \& size of bolts

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $22-1 \frac{1}{2}$ | $22-1 \frac{1}{2}$ | $22-13 / 8$ | $22-1 \frac{1}{4}$ | $22-1 \frac{1}{4}$ | $22-1 \frac{1}{4}$ | $22-1 \frac{1}{4}$ | $22-1 / 18$ | $22-1$ |

Bolted thro the knee and post and upon the said knee bring on the rest of the riseing wood fastened in the same manner

Haus pieces number on each side and a piece between or four if can be had

| If in two each pieces to be had | Broad | $2-8$ | $2-7$ | $2-6$ | $2-5$ | $2-4$ | $2-3$ | $2-2$ | $2-1$ | $2-0$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | Holes Diameter | $1-4$ | $1-3$ | $1-2$ | $1-1$ | $1-1 \frac{1}{2}$ | $1-0$ | $0-11$ | $0-10$ | $0-9$ |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  | $2-7$ | $2-7$ | $2-7$ | $2-7$ | $2-7$ | $2-7$ | $2-6$ | $2-5$ | $2-5$ |

Floor \& Futtucks in the bearing of the ship to fill up the room and space especially for large ships (if can conveniently be had)

## Parts of the Frame

Timbers next the flat sided
Timbers afore \&abaft in the wake of the haft timbers 2 in less than in midships from 100 to 60 gun ships 50 gun ships in $1 \not 1 / 2$ and 40 gun ships \& downwards 1 inch less

At the wrongheads wrought in and out at $\square$

| 1-2 | 1-11/2 | 1-03/4 | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 | 0-7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-1 | $1-01 / 2$ | 0-113/4 | 0-11 | 0-10 | 0-9 | 0-8 | 0-7 | 0-6 |
| 0-11/2 | 0-11/2 | $0-13 / 8$ | $0-13 / 8$ | 0-11/4 | 0-11/4 | 0-11/4 | $0-1 /{ }^{1 / 8}$ | 0-1 |
| 1-8 | 1-6 | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 | 1-0 |
| 1-2 | 1-2 | 1-11/2 | 0-11 $1 / 4$ | 1-1 | 1-0 | 0-11 | 0-10 | 0-9 |
| 1-0 | 1-0 | 0-11 $1 / 2$ | 0-111/4 | 0-11 | 0-101/2 | 0-10 | 0-9 | 0-8 |
| 8-0 | 7-9 | 7-6 | 7-2 | 6-10 | 6-6 | 6-2 | 5-10 | 5-2 |
| 0-111/2 | 0-11 | 0-101/2 | 0-10 | 0-9 | 0-8 | 0-7 | 0-6 | 0-51/ |
| 7-9 | 7-5 | 7-0 | 6-10 | 6-9 | 6-4 | 7-6 | 6-41/2 | 5-4 |
| 6-6 | 6-3 | 6-0 | 6-0 | 6-0 | 6-0 | 6-0 | 6-5 | 5-0 |

## Joshua Humphreys Notebook

| $2^{\text {nd }}$ sided the midships | 1-11/2 | 1-11/2 | 1-1 | 1-03/4 | 1-01/4 | 0-111/2 | 0-101/2 | 0-91/2 | 0-81/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Afore \& abaft | 0-11 1 /2 | 0-111/2 | 0-11 | 0-103/4 | 0-101/4 | 0-10 | 0-91/2 | 0-81/2 | 0-71/2 |
| Futtucks $2^{\text {nd }}$ scarphs in the midships long | 7-9 | 7-5 | 7-6 | 6-10 | 6-9 | 6-4 | 7-6 | 6-41/2 | 5-4 |
| Afore \& abaft if to be had not less than | 6-6 | 6-3 | 6-0 | 6-0 | 6-0 | 6-0 | 6-0 | 5-6 | 5-0 |
| $3^{\text {rd }}$ sided in amidships | 1-1 | 1-1 | 1-01/2 | 1-01/4 | 1-0 | 0-11 | - - | - - | - - |

## Parts of the Frame

| Afore \& abaft | 0-11 1 /2 | 0-111/2 | 0-11 | 0-103/4 | 0-101/2 | 0-93/4 | - - | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Scarphs long in the midships | 7-9 | 7-5 | 7-0 | 6-10 | 6-9 | 6-4 | - - | - - | - - |
| Afore and abaft at the heads an inch less than | 6-6 | 6-3 | 6-0 | 6-0 | 6-0 | 6-0 | - - | - - | - - |
| Upper sided in the midships | 1-1 | 1-1 | 1-01/2 | 1-01/4 | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 |
| Afore and abaft at the heads an inch less than | $0-11^{1 / 2}$ | 0-111/2 | 0-11 | $0-103 / 4$ | 0-101/4 | 0-10 | 0-91/2 | $0-81 / 2$ | 0-71/2 |

To reach the upper deck clamps of 2 decks ships \& the middle deck clamps of 3 decks ships and the wake of the channels to turn up as high as the deck if can be had


Timbers in 50 gun ships at the side of the gundeck ports to make top timber and upper futtocks in one and in all other ships in the wake of the channels some (if can be had). The frame bends to every $4^{\text {th }}$ timber from the midships flat to be canting or beveling timbers afore and abaft and then every other timber

In Hold

Keelson Square
Number of pieces if can be had

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $1-7$ | $1-6$ | $1-5$ | $1-4$ | $1-3$ | $1-2$ | $1-1$ | $1-0$ | $0-11$ |
| $6-0$ | $6-0$ | $5-0$ | $5-0$ | $5-0$ | $5-0$ | $7-0$ | $4-0$ | $4-0$ |

Length of the scarphs to reach three floor timbers and to be bolted with bolts of the same size of the floor timbers and two small bolts in the ends of the scarphs standerd upon or under the keelson abaft the up \& down arm to but under the lower transom (if can be had).

| The other arm long Sided at least |  | 9-0 | 8-9 | 8-6 | 8-3 | 8-0 | 7-9 | 7-6 | 7-3 | 7-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1-1 | 1-1 | $1-01 / 2$ | 1-01/4 | 1-0 | 0-111⁄2 | 0-11 | 0-101/2 | 0-10 |
| Limber board | Thick | 0-3 | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-21/2 | 0-21/2 | 0-2 |
|  | Broad | 1-2 | 1-2 | 1-2 | 1-52 | 1-2 | 1-2 | 1-2 | 1-2 | 1-0 |
| Streakes next the limber boards | Thick | 0-6 | 0-5 |  |  |  |  |  |  |  |
|  | Broad if can be had | 1-3 | 1-3 |  |  |  |  |  |  |  |
| Thick stuff at the floor heads | Middle Strake thick | 0-9 | 0-9 | 0-8 | 0-8 | 0-7 | 0-6 | 0-6 | 0-5 | 0-5 |
|  | Broad if to be had | 1-4 | 1-31/2 | 1-3 | 1-3 | 1-3 | 1-3 | 1-2 | $1-11 / 2$ | $1-1 / 1 / 2$ |
| Number and thickness Of the straks | Above the middle | 1-9 | 1-9 | 1-8 | 1-8 | 1-7 | 1-6 | 1-6 | 1-5 | 1-3 |
|  |  | 1-8 | $1-71 / 2$ | 1-6 | 1-5 | 1-5 | 1-4 | 1-6 | 1-5 | 1-3 |
| $\mathrm{D}^{\circ}$ | below the | 1-9 | 1-9 | 1-8 | 1-8 | 1-7 | 1-6 | 1-5 | 1-5 | 1-5 |
|  | Middle straks | 1-8 | 1-7 | 1-6 | 1-5 | 1-5 | 1-4 | 1-5 | 1-5 | 1-5 |

No more than 3 streaks afore \& abaft for those 3 deck ships to be but 4 in the 70, 60, \& 50 gun ships.

## Joshua Humphreys Notebook

In the $40 \& 30$ gun ships, 2 streaks of 3 in. \& the 20 gun ships one streak of $2 ½ \mathrm{in}$.


Broad
Proper for having a Sufficient opening under ye Gun Clamp
Standard knees where there are no fut ${ }^{\mathrm{ks}}$ riders sided the same as the other nees
No. \& Size of Bolts in each the same size as before carling \& leges the same as the Gundeck


The fore \& Aft Arm to be Scored in the Timbers $11 / 2$ in. and to scarph with hook \& but the fore on the spurketting a sufficient length

## Joshua Humphreys Notebook

| Fore \& aft | Long | 20-0 | 19-0 | 18-0 | 17-0 | 16-0 | 14-0 | 18-0 | 12-0 | 10-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Shortest Arm | if can be had | 10-0 | 9-6 | 9-0 | 8-6 | 8-0 | 7-6 | 7-0 | 6-6 | 6-0 |
| Transom nees wing | Distance \& Size of Bolts | $24-13 / 8$ | 24-11/4 | 24-11/4 | 24-11/4 | 24-1/1/8 | 24-1 | 24-1 | 24-0.7/8 | $24-03 / 4$ |
| The deck transom nees | Sided \& Bolted the Same size as the Gundeck nees $\mathrm{y}^{\mathrm{e}}$ number of bolts measuring according to their lengths |  |  |  |  |  |  |  |  |  |
| Length of the Longest Arm |  | 10-0 | 9-0 | 9-0 | 8-6 | 8-0 | 7-0 | 7-0 | 6-6 | 6-0 |
| Distance and Size of Bolts the Same as the Wing Transom Nees |  |  |  |  |  |  |  |  |  |  |
| Riders Floor | Number | 5-0 | 4-0 | 3-0 | 2-0 | 2-0 |  |  |  |  |
|  | Length | 29-0 | 27-6 | 26-0 | 24-6 | 23-0 |  |  |  |  |
|  | Sided | 1-7 | 1-6 | 1-5 | 1-4 | 1-3 |  |  |  |  |
| Deep on the Kelson |  | 1-2 | 1-1 | 1-0 | 1-0 | 1-0 |  |  |  |  |
| At the floor timber heads |  | 1-4 | $1-31 / 4$ | 1-3 | 1-2 | 1-1 |  |  |  |  |
| No \& Size of bolts in each |  | $12-11 / 2$ | $12-11 / 2$ | $10-13 / 8$ | 10-11/4 | 10-13/8 |  |  |  |  |

Distance and size of bolts the same as the wing transom knee below the gundeck sided 2 in . less than the transoms

| Longest Arm Long |  | 10-0 | 9-9 | 9-0 | 8-6 | 8-0 | 7-6 | 7-0 | 6-6 | 6-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lower futt ${ }^{\text {ks }}$ number on each side |  | 8 | 4 | 6 | 5 | 5 | 3 | 3 | 2 | - - |
| To have pieces scarph'd \& hooked on the heels of the across the keelson where there is no floor riders |  |  |  |  |  |  |  |  |  |  |
| Riders low ${ }^{\text {r }}$ futt $^{\text {ks }}$ scarph'd each way from the floor riders | Downwards to the low edge off the orlope beams if can be had |  |  |  |  |  |  |  |  |  |
|  | Upwards | 7-9 | 7-9 | 7-4 | 7-2 | 7-0 | 6-9 | 6-6 | 6-3 | -- |
|  | Sided | 1-5 | 1-41/2 | 1-4 | 1-4 | 1-31/2 | 1-3 | 1-2 | 1-1 | - - |
| Moulded at the floor head |  | 1-4 | $1-31 / 2$ | 1-3 | 1-2 | 1-1 | 1-0 | 0-11 | 0-10 | -- |
| No \& size of bolts in back |  | 9-11/2 | 9-11/2 | 9-1 | 8-1 | 8-11/4 | 8-11/4 | $8-1{ }^{1 / 8}$ | -- | - - |

## Joshua Humphreys Notebook

## Upper futtocks number on each side

Length downwards if can be had to the heads of the floor riders
Upwards to the gundeck lodging knees
Sided

Moulded at the upper end
To be bolted to the orlope beams with 2 bolts the same size as the orlope knees
No \& size of the bolts thr'o the side
Crotches abaft on the sealing - No

Length of each side if can be had Sided

No \& size of bolts in each

Steps main sided to the diameter of main mast in the partners
Deep on the keelson
Foresided to the diameter of the foremast in the partners
Deep on the keelson a sufficient depth
Length if can be had
No \& size of bolts in each

Steps on mizzen sided the diameters at the mizzen mast in the partners
On the keelson a sufficient depth

| No \& size of bolts in each |  |
| :--- | :--- |
| Steps main capstand | Broad |
|  | Deep |


| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $8-9$ | $7-0$ | $6-0$ | $5-0$ | -- | -- | - | -- | -- |
|  |  |  |  |  |  |  |  |  |
| $1-3$ | $1-2^{1 / 2}$ | $1-2$ | $1-2$ | -- | -- | -- | -- | -- |
| $1-1$ | $1-0$ | $0-11$ | $0-10$ | -- | -- | - | -- | -- |


| $8-13 / 8$ | 8-11/4 | 8-11/4 | 8-11/4 | - - | - - | - - | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 2 | 2 | 2 | 1 | 1 | 1 | 1 | 1 |
| 9-0 | 8-6 | 8-0 | 7-6 | 7-0 | 6-6 | 6-5 | 6-0 | 5-0 |
| 1-2 | 1-2 | 1-1 | 1-1 | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 |
| $8-13 / 8$ | 8-11/4 | 8-11/4 | 6-11/4 | 6-1 ${ }^{1}$ | 6-1 | 6-1 | 6-0 | 6-03/ |


| $1-7$ | $1-6$ | $1-5$ | $1-4$ | $1-3$ | $1-3$ | $1-2$ | $1-1$ | $1-0$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| $15-0$ | $14-0$ | $13-0$ | $12-0$ | $11-0$ | $10-0$ | $9-0$ | $8-0$ | $7-0$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $8-1 \frac{1}{2}$ | $8-1^{1 / 2}$ | $8-1^{3 / 8}$ | $8-1^{3 / 8}$ | $8-1^{1 / 4}$ | $8-1^{1 / 4}$ | $8-1^{1 / 4}$ | $6-1^{1 / 4}$ | $6-1$ |


| $8-13 / 8$ | $8-1^{1 / 4}$ | $8-1^{1 / 4}$ | $6-1^{1 / 4}$ | $6-1^{1 / 2}$ | $6-1$ | $6-1$ | $6-0^{7 / 8}$ | $0-3 / 4$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $2-0$ | $1-10$ | $1-9$ | $1-8$ | $1-7$ | $1-6$ | $1-5$ | $1-4$ | $1-2$ |
| $1-4$ | $1-3$ | $1-21 / 4$ | $1-2$ | $1-1$ | $1-1$ | $1-1$ | $1-0$ | $1-0$ |

## Joshua Humphreys Notebook

| Bresthook under the gundeck hook low'r | 1-3 | $1-2^{1 / 4}$ | 1-2 | 1-2 | - - | - - | - - | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2{ }^{\text {nd }} 7$ | 1-3 | $1-2^{1 / 4}$ | 1-2 | 1-2 | - - | - - | - - | - - | - - |
| 3 rd $\} \quad$ Sided | 1-3 | $1-2^{1 / 4}$ | 1-2 | 1-2 | - - | - - | - - | - - | - - |
| $4^{\text {th }} \int$ | 1-3 | 1-21/4 | 1-2 | 1-2 | - - | - - | - - | - - | - - |
| Length if can be had | 17..0 | $16 . .6$ | $16 . .0$ | $15 . .6$ | $15 . .0$ | 14... 6 | $14 . .0$ | 13..0 | 12-0 |
| No \& size of bolts | 13-11/4 | 13-11/4 | $13-13 / 8$ | $11-1{ }^{3 / 8}$ | 11-11/4 | 9-11/4 | 9-11/4 | $9-1 / 1 / 8$ | 9-1 |
| Pillers upright under the beams square | 0-9 | 0-81/4 | 0-8 | 0-8 | 0-71/4 | 0-7 | 0-6 | 0-6 | 0-5 |
| To be placed under the middle of each beam Y in the quarters on the scarphs of the rid | where | here ar | no poin | ters |  |  |  |  |  |
| Pointers Square | 1-0 | 0-11 | 0-10 | 0-+ | $0-81 / 2$ | - - | -- | -- | - - |
| Number of pair to meet wholly under the gundeck beams to be scored $11 / 4$ in into the orlope beams | 5-0 | 4-0 | 3-0 | 2-0 | 2-0 | -- | - - | -- | -- |
| Pillers to be bolted to the gundeck beams with up \& down bolts \& to the orlope beam fore \& aft each pointer to have No. bolts in each end | $2-1 / 4$ | $2-1 /{ }^{1 / 8}$ | $2-1 / 8$ | $2-1 / 8$ | 2-1 | - - | -- | -- | - - |
| Well fore \& Aft | 9-8 | 9-4 | 9-0 | 7-8 | 7-4 | 7-0 | 6-8 | 6-4 | 6-0 |
| Thwartships | 10-1 | 9-11 | 9-10 | 7-7 | 7-3 | 6-10 | 6-5 | 6-1 | 5-8 |
| The plank under the orlope thick | 0-3 | 0-3 | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-2 | 0-2 |
| Shotlockers No one abaft \& the other before ye well | 2-0 | 2-0 | 2-0 | 2-0 | 2-0 | 2-0 | 1-0 | 1-0 | 1-0 |
| Fore \& aft in the clear | 2-6 | 2-6 | 2-4 | 2-4 | 2-2 | 2-1 | 2-0 | 1-11 | 1-10 |
| Plank thick | 0-3 | 0-3 | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/2 | $0-21 / 2$ | 0-2 |

## Joshua Humphreys Notebook

|  |  | $\begin{aligned} & 100 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 90 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 80 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 70 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 60 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 50 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 40 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 30 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 20 \\ & \text { Ft-In } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| At the after bitts ${ }^{0} 0$ |  | 1-0 | 1-0 | 1-0 | - - | - - | - - | - - | - - | - - |
| Bulkheads | Length from the inside of the rabit of $\mathrm{y}^{\mathrm{e}}$ stem on the gundeck to the after bulkhead of the magazine | 36-5 | 34-6 | 29-0 | 27-6 | 25-6 | 23-6 | 21-6 | 19-6 | - - |
|  | Length from $y^{e}$ inside of the rabbit of the post on the gundeck to the foreside of the bulkhead breadroom | 32-0 | 30-6 | 29-0 | 27-6 | 25-6 | 23-6 | 21-6 | 19-6 | - - |
|  | Length from ye bulkhead of the breadroom to the forepart of the bulkhead of the captains storeroom \& pursers sloproom | 21-0 | 20-6 | 19-6 | 18-6 | 18-0 | 17-6 | 16-6 | 15-6 | - - |
|  | The fish bulkhead to be abaft the bulkhead of the captain's Storeroom \& pursers sloproom | 5-0 | 5-20 | 5-0 | 5-0 | 5-0 | 5-0 | 5-0 | 5-0 | - - |

Gundeck

| Clamps thick \& broad | upp ${ }^{\text {r }}$ |  | 9-1-3 | 81/4-1-3 | $81 / 4-1-2^{1 / 2}$ | 8-1-2 | 7-1-2 | - | - | - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $2{ }^{\text {nd }}$ | to be tabled 2 in into | 8-1-1 | 7-1-0 | 71/4-1-0 | 7-1-0 | 6-1-0 | - - | -- | - - | - - |
|  | Lower | each other | 7-1-0 | 61/2-1-0 | 61/4-1-0 | 6-1-0 | 6-1-0 | - - | - - | - - | - - |
| Off in 2 streaks | upper |  | $1-51 / 2$ | 1-5 | 1-5 | 1-41/2 | 1-4 | 6-1-3 | 51/2-1-3 | 5-1-2 | 4-1-2 |
|  | Lower |  | $1-41 / 2$ | 1-4 | 1-4 | $1-31 / 2$ | 1-3 | 5-1-2 | 41/2-1-2 | 4-1-1 | 3-1-1 |
| Length of the scarphs |  |  | -3-8 | -3-7 | -3-6 | -3-5 | -3-4 | -3-3 | -3-2 | -3-1 | 3-3-0 |
| Opening under them |  |  | -0-10 | -0-10 | -0-10 | -0-91/2 | -0-9 | -0-8 | -0-8 | -0-8 | -0-8 |
| Bresthook under y ${ }^{\text {e }}$ haw | ses sided |  | -1-3 | $-1-2^{1 / 4}$ | -1-2 | -1-11/2 | -1-1 | -1-0 | -0-11 | -0-10 | -0-9 |

## Joshua Humphreys Notebook

Length
No \& size of bolts

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $17-0$ | $16-6$ | $16-0$ | $15-6$ | $15-0$ | $14-6$ | $14-0$ | $13-0$ | $12-0$ |
| $13-13 / 8$ | $13-13 / 8$ | $13-1 \frac{1}{4} 4$ | $11-1^{1 / 4} 4$ | $11-1 \frac{1}{2}$ | $9-1 \frac{1 / 8}{8}$ | $9-1$ | $9-0 / 8$ | $9-03 / 4$ |

Under the gundeck to have a large chock \& to be left as much for \& aft as possible for the better fastning, checking \& bolting the plank of the gundeck to the same.

| Beams | Sided in the midships | \& one inch less | 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-10 | 0-8 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Moulded | afore \& abaft | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-11 | 0-9 | 0-7 |

One to be placed under and 1 between each port where it can conveniently be done except in the wake of the hatchways \& masts there to have double arm'd beams, that one part may be proper for a standerd, if the other to come under the ports to be double kneed at each end and with 1 hanging \& 1 lodging knee.

| Knees sided | Lodg'g | foremast, main \& hatch | 0-101/2 | 0-10 | 0-91/2 | 0-6 | 0-81/2 | 0-8 | 0-71/2 | 0-61/2 | 0-51/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Hang'g | to be half inch bigger | 0-11 | 0-101/2 | 0-10 | 0-91/2 | 0-9 | $0-81 / 2$ | 0-8 | 0-7 | 0-6 |
| Hanging arm | can be had |  | 6-6 | 6-4 | 6-2 | 5-9 | 5-6 | 5-3 | 5-0 | 4-9 | 4-6 |
| No \& size of | ls in each $h$ |  | $7-13 / 8$ | 7-11/4 | 7-11/4 | 7-11/4 | $6-1 / 1 / 8$ | $6-1{ }^{1 / 8}$ | 0-1 | $6-0^{7 / 8}$ | 6-03/4 |

To have 4 bolts in the lower arm of the hanging knees, especially in the wake of the masts \& hatchways \& where the hanging knees can be got of a sufficient length for 80,70 , and 60 gun ships.

Three carlings in $y^{\mathrm{e}}$ wake of the main \& for hatches \& main mast room

Carlings number of teer on each side
Broad
Deep
Bolts - Number of pair

The foreside of the foremast to be abaft the rabbit of the stem

Aftermost bitts to be abaft the foreside of the foremast

Distance between them thwartships Foremast Aftermast

| 3 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $0-6$ | $0-5^{1 / 2} 2$ | $0-51 / 2$ | $0-5$ | $0-5$ | $0-4^{1 / 2}$ | $0-4$ | $0-3^{1 / 2} 2$ | $0-3$ |
| $0-5$ | $0-5$ | $0-5$ | $0-5$ | $0-4^{1 / 2} 2$ | $0-4^{1 / 2} 2$ | $0-3^{1 / 2}$ | $0-3$ | $0-2^{1 / 2} 2$ |
| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | -- |
| $29-10$ | $26-2$ | $26-0$ | $26-0$ | $21-3$ | $20-6$ | $16-2$ | $15-0$ | -- |
|  |  |  |  |  |  |  |  |  |
| $11-8$ | $11-2$ | $10-4$ | $10-6$ | $10-1$ | $10-6$ | $9-9$ | $9-4$ | -- |
|  |  |  |  |  |  |  |  |  |
| $4-0$ | $3-10$ | $3-8$ | $3-5$ | $3-2$ | $2-11$ | $2-8$ | $2-6$ | - |
| $4-10$ | $4-7$ | $4-4$ | $4-0$ | $3-8$ | $3-5$ | $3-2$ | $3-0$ | - |

## Joshua Humphreys Notebook

| Crosspiece | Foremast Deep | 1-7 | 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-11 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Fore \& Aft | 1-8 | 1-7 | 1-61/2 | 1-51/2 | $1-41 / 2$ | $1-31 / 2$ | 1-3 | 1-21/4 | 1-2 |
|  | Aftermast Deep | 1-7 | 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 | 0-11 |
|  | Fore \& Aft | 1-8 | 1-7 | 1-61/2 | 1-51/2 | $1-41 / 2$ | $1-31 / 2$ | 1-3 | 1-21/4 | 1-2 |
| Lower edge above the deck | Foremast | 1-10 | 1-91/2 | 1-6 | 1-81/2 | 1-8 | 1-7 | 1-6 | 1-5 | 1-4 |
|  | Aftermast | 1-9 | $1-81 / 2$ | 1-8 | 1-71/2 | 1-7 | 1-6 | 1-5 | 1-4 | 1-3 |
| Scored in deep |  | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/4 | 0-2 | 0-2 | 0-2 | 0-2 |
| Standard knees sided |  | 1-1 | 1-01/2 | 1-0 | 0-11 1 /2 | 0-11 | 0-101/2 | 0-10 | 0-91/2 | 0-9 |
| Elm backs of |  | 0-6 | 0-6 | 0-6 | 0-6 | 0-6 | 0-51/2 | 0-5 | 0-41/2 | 0-4 |
| Square | Foremost | 1-10 | 1-9 | 1-71/2 | 1-6 | 1-41/2 | 1-3 | $1-1 / 1 / 2$ | 1-0 | 0-11 |
|  | Aftermost | 1-11 | 1-10 | 1-8 | 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | 1-1 |

To be sufficiently deep to make the carling if can be had.
Bitts, standerd knees, the arm upon the deck to be as long as the bitts are asunder if can be had \& the forepart to be flush with the deck.

No \& size of bolts in each

Waterway thick in the chine one inch thicker than the plank of the deck.
Plank on flat to be English oak in the wake of the standard
Two strakes must the comings in all ships except those of 20 guns to be one inch thicker than the rest of the deck and to be let down an inch on the beams to be bolted with 2 small bolts to $5 / 8$ of an inch in the great ships and $1 / 2$ inch in all under 70 guns to be 1 inch longer than twice the thickness of the plank

All the rest to be bolted with one bolt in each beam and one treenail in each edge
Thickness on the depth of the cant on the lower cell of the gundeck ports, 3 inch for $100,90,80$ gun ships, $2^{1 ⁄ 2}$ in. for other classes.
Partners, for the masts the main to carlings broad $\quad \begin{array}{lllllllllll}1-5 & 1-41 / 2 & 1-4 & 1-31 / 2 & 1-3 & 1-2 & 1-1 & 1-0\end{array}$

## Joshua Humphreys Notebook

| Deep |  |  | 1-6 | 1-51/2 | 1-5 | $1-41 / 2$ | 1-4 | 1-3 | 1-2 | 1-1 | 1-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Partners for the masts | Foremasts <br> Mizenmast <br> Bowsprit | Thick | 0-7 | 0-7 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 | 0-41/2 | 0-4 |
|  |  |  | no th | ker than | the rest | of the | eck |  |  |  |  |
|  |  |  | 0-10 | 0-10 | 0-9 | 0-8 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 |
| Partner for main capstands |  |  | 0-7 | 0-7 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 | 0-41/2 | 0-4 |
| False $\mathrm{D}^{\circ}$ for the main capstand under the beams thick |  |  | 0-4 | 0-4 | 0-4 | 0-4 | 0-3 | 0-3 | 0-3 | 0-21/2 | -- |
| Step for the main teer capstand thick Triple capstand thick |  |  | 1-4 | 1-3 | 1-2 | 1-11/2 | 1-1 | 1-01/2 | 1-0 | 1-0 | 1-0 |
|  |  |  | 1-0 | 0-111/2 | 0-111/2 | - - | - - | - - | - - | -- | - - |

The steps for the capstands to be no higher above the deck than 4 inch where it can be done

| Hatches | Main fore |  | 8-10 | 8-7 | 8-4 | 8-0 | 7-8 | 7-4 | 7-0 | 6-8 | 5-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thwartsh |  | 6-10 | 6-7 | 6-4 | 6-0 | 5-8 | 5-4 | 5-0 | 4-8 | 4-2 |
| Fore | Fore \& aft |  | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 3-1 ${ }^{\text {spl }}$ |
|  | Thwartsh |  | 4-10 | 4-10 | 4-8 | 47 | 3-8 | 3-7 | 3-7 | 3-2 | -- |
| Next abaft the main mast |  | fore \& aft | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | - - |
|  |  | Thwartships | 4-10 | 4-10 | 4-9 | 4-8 | 4-8 | 3-8 | 3-7 | 3-4 | - - |
| Hatches over $\mathrm{y}^{\text {e }}$ fishroom |  | Fore \& aft | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | 4-8 | - - |
|  |  | Thwartships | 4-10 | 4-10 | 4-8 | 3-8 | 3-7 | 3-3 | 3-3 | 3-2 | - - |
| $\mathrm{D}^{\circ}$ over the steward room for \& aft |  |  | 3-4 | 3-3 | 3-2 | 3-1 | 3-0 | 2-10 |  |  |  |
|  |  | Thwartships | 4-0 | 3-11 | 3-10 | 3-9 | 3-8 | 3-7 | - - | - - | - - |
| Plank thick for them one inch and half to each Height above the deck two inches to each |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| Scuppers lead number on each side Diameter in the clear |  |  | 4 | 4 | 4 | 4 | 4 | 6 | - - | - - | - - |
|  |  |  | 0-4 | 0-4 | 0-4 | 0-4 | 0-4 | 0-6 | -- | -- | - - |
| For the pump dale diameter in the clear |  |  | 0-6 | 0-6 | 0-6 | 0-6 | 0-6 | 0-6 | 0-6 | 0-6 | 0-6 |
|  |  |  |  |  |  |  |  |  |  |  |  |

## Joshua Humphreys Notebook

|  | $\begin{aligned} & 100 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 90 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 80 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 70 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 60 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 50 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 40 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 30 \\ & \text { Ft-In } \end{aligned}$ | $\begin{aligned} & 20 \\ & \text { Ft-In } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Manger plank thick | 0-4 | 0-4 | 0-4 | 0-4 | 0-4 | 0-4 | 0-3 | 0-3 | 0-3 |
| Scupper in $\mathrm{D}^{\circ}$ on each side | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 |
| Scuppers diameter in the clear | 0-5 | 0-5 | 0-5 | 0-5 | 0-5 | 0-5 | 0-41/2 | 0-4 | 0-4 |
| Sperketing number of strakes on each side to be bolted to the next timber To each butt with one bolt | 3 or 2 | 3 or 2 | 3 or 2 | 3 or 2 | 3 or 2 | 3 or 2 | 2 | 2 | 2 |
| Thickness in midships $\begin{aligned} \text { @ the lower edge } \\ \text { @ the upper edge }\end{aligned}$ | $\begin{aligned} & 0-8 \\ & 0-6 \end{aligned}$ | $\begin{aligned} & 0-7^{1 / 2} \\ & 0-6 \end{aligned}$ | $\begin{aligned} & 0-7 \\ & 0-5^{1 / 2} \end{aligned}$ | $\begin{aligned} & 0-6 \\ & 0-4^{1 / 2} \end{aligned}$ | $\begin{aligned} & 0-5 \\ & 0-4 \end{aligned}$ | $\begin{aligned} & 0-4^{1 / 2} \\ & 0-3^{1 / 2} \end{aligned}$ | $\begin{aligned} & 0-4 \\ & 0-3 \end{aligned}$ | $\begin{aligned} & 0-3^{1 / 2} \\ & 0-2^{1 / 2} \end{aligned}$ | $\begin{aligned} & 0-3 \\ & 0-2^{1 / 2} \end{aligned}$ |
| Plank between the middle or upper deck clamps \& sperketing Thick | 0-4 | 0-31/2 | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-21/2 | 0-2 | 0-2 |
| Ports in the counter Number | 4 | 4 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Oar Number | - - | - - | - - | - - | - - | - - | 30 | 24 \& 8 | 36 |
| Deep | - - | - - | - - | - - | - - | - - | 0-81/2 | 0-81/2 | 0-8 |
| Fore \& Aft | - - | -- | - - | -- | - - | - - | 0-8 | 0-8 | 0-71/2 |
| Standard number on each side the foremost pair to be iron sided | 5 | 5 | 4 | 3 | 3 | 2 | -- | - - | - - |

The up \& down arms so long as to take hold of the edge of the middle or upper deck clamps (if can conveniently be had) \& abaft to be placed as ye upper and as conveniently may be had

Shortest arm long (if can be had)
Number \& Size of bolts each

$$
\begin{array}{ll}
\text { Iron standers } & \begin{array}{l}
\text { Breadth } \\
\text { Thickness }
\end{array} \\
& \text { Weight }
\end{array}
$$

Capstand, main, diameter in the partners of $y^{e}$ lower part including the whelps

## Joshua Humphreys Notebook

## Barrs number <br> Length

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| (NOTE: | NO | ENTRIES | HERE | IN | ORIGINAL JOURNAL) |  |  |  |
| 12 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | - |

Number of iron palls four to each where they can be fitted, two of which to fall upon the head or trundale heads, and to answer the pauls upon the deck

| Pillars turn'd in the square | 0-8 | 0-71/2 | 0-71/4 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 | 0-41/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tiller square in the biggest place | 1-1 | 1-0 | 0-11 | 0-10 | 0-40 | 0-91/2 | 0-9 | 0-81/2 |  |
| Sweep to be flush with the beam Thickness | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-21/2 | 0-21/4 | 0-21/4 | 0-21/4 | 0-2 |
| Breadth | 1-0 | 0-11 | 0-10 | 0-9 | 0-8 | 0-71/2 | 0-7 | 0-61/2 | 0-61/2 |
| False transom Deep | 1-0 | 0-11 | 0-10 | 091/2 | 0-8 | 0-71/2 | 0-7 | 0-61/2 | 0-6 |
| Knees Deep | $0-10^{1 / 2}$ | 0-91/2 | 0-9 | 0-81/2 | 0-8 | $0-71 / 2$ | 0-7 | 0-61/2 | 0-6 |
| Arms Fore \& Aft | 11-6 | 11-0 | 10-6 | 10-0 | 9-6 | 9-0 | 8-6 | 8-0 | 7-6 |
| Thwartships | 6-0 | 6-0 | 8-8 | 5-4 | 5-0 | 4-8 | 4-4 | 4-0 | 3-8 |
| Number and size of bolts the same as the middle or upper deck knees |  |  |  |  |  |  |  |  |  |
| Bolts ring \& eye for each port, number and size The additional ring bolts to be placed in the next timber to the port timber | $6-13 / 8$ | 6-11/4 | 6-11/4 | 6-11/4 | 4-11/4 | $1-1 /{ }^{1 / 8}$ | $4-1 /{ }^{1 / 8}$ | 4-1 | - - |
|  |  |  |  |  |  |  |  |  |  |
| Diameter in the clear of the ring | 0-51/2 | 0-51⁄2 | 0-51/4 | 0-5 | 0-5 | $0-43 / 8$ | $0-4{ }^{1 / 8}$ | 0-41/4 | -- |
| The iron of the rings to be somewhat less than the bolts |  |  |  |  |  |  |  |  |  |
| On the flat of the deck for the guns size | $0-1{ }^{1 / 8}$ | $0-1 /{ }^{1 / 8}$ | $0-1 /{ }^{1 / 8}$ | 0-1 | 0-1 | $0-7 / 8$ | 0-7/8 | 0-5/8 | - - |
| The diameter of the rings to be sufficiently only to hook the tackles |  |  |  |  |  |  |  |  |  |
| Stopper size | 0-13/4 | $0-1{ }^{5 / 8}$ | $0-1{ }^{5 / 8}$ | $0-11 / 2$ | $0-11 / 2$ | $0-1{ }^{3 / 8}$ | $0-13 / 8$ | 0-1/4 | 0-11/4 |
| Diameter of rings in the clear | 0-71/4 | $0-71 / 4$ | 0-61/4 | 0-6 | 0-51/2 | 0-51/4 | 0-5 | $0-43 / 4$ | 0-41/2 |
| S Size | 0-11/4 | $0-1{ }^{1 / 8}$ | $0-1{ }^{1 / 8}$ | $0-1{ }^{1 / 8}$ | $0-1{ }^{1 / 8}$ | 0-1 | 0-1 | 0-7/8 | - - |
| Eye over the port for lassing of the guns $\quad$ Diameter of the eye in the clear | 0-21/2 | 0-21/2 | $0-2^{3 / 8}$ | $0-2^{3 / 8}$ | 0-21/4 | 0-21/4 | 0-2 | 0-2 | -- |

Bolts, ring eye \& stopper to be left so well in as only to let $\mathrm{y}^{\mathrm{e}}$ rings have plan. Ring eye \& all other to go thro the side, that are to be fore lock'd the ring to be let in the side as a short thick forelock hole \& about thick point to the bolt.


Knee against the stern post to reach 4 beams (if can be had) with a long carling forcht up under the beam to reach the next the mizzen mast \& give sufficient scarph to the knee \& bolt knee \& carling bolt thro each beam with bots of the same size as the gundeck.
To be sided
1-2 1-1

Centers of masts - the foremast ${ }^{1 / 10}$ of the length of the gundeck abaft the rabbit of the stem and to stand upright.
Mainmast ${ }^{1 / 22}$ of the deck abaft the middle of the deck (its bagg or convex part always aft the rake one inch in a yard Mizenmast mast ${ }^{4 / 23}$ of the length of the deck before the rabbit of the post $\&$ to rake $5 / 8$ of an inch to a foot

The upper edge of the counter rail at the knuckle of the counter must be fair with the top of the middle deck or upper deck.

Middle Deck

| Clamps ${ }^{\text {o }}$ of straps on each side |  |  | 1 | 1 | 1 | - - | - - | - - | - - | - - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| To be wrought anchor stock fashion with hoops or chockes |  |  |  |  |  |  |  |  |  |  |  |
| Thick at the |  | upper edge | 0-7 | 0-61/2 | 0-6 | - - | -- | - - | - - | - - | - - |
|  |  | Lower edge | 0-6 | 0-51/2 | 0-5 | - - | - - | - - | - - | - - | - - |
|  | Depth |  | as much as can be allowed |  |  |  |  |  |  |  |  |
| Beams | Sided |  | 1-3 | 1-2 | 1-1 | -- | - - | - - | - - | - - | - - |
|  | Moulded |  | 1-1 | 1-0 | 0-11 | - - | - - | - - | - - | - - | - - |

## Joshua Humphreys Notebook

To lye one under \& one between each port where they may conveniently be place \& as near as possible over ${ }^{e}$ gundeck beams to have a long carling under the foremast to take hold of the next beam abaft the foremast and that next the foreside of the after bitts


The two upper bolts of the handing knees to be as high up as conveniently can be done \& the likes for the hanging knees of all other decks, for the better keeping the breadth of the knee to the side

| Transoms | s, the deck trans |  | 0-11 | 0-10 | 0-9 | - | -- | - - | - - | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Knees at each en |  | 0-91/2 | 0-9 | 0-8 | - | - - | - - | - - | - - | - - |
|  | Arms fore \& aft | long as lon |  |  |  |  |  |  |  |  |  |
|  |  | Shortest | 4-6 | 4-3 | 4-0 | - |  | - - |  | - - | - - |
|  | At the lower por | deep | 0-8 | 0-71/2 | 0-7 | - | - - | - - |  | - - | - - |
|  | to be tur | each end |  |  |  |  |  |  |  |  |  |
|  | Bresthook, sided |  | 1-3 | 1-2 | 1-1 | - | - - | - - | - | - - | - - |
|  | Long if | had | 17-0 | 16-0 | 16-0 | - | - - | - - | - - | - - | - - |
| Number \& | \& size of bolts |  | 13-11/4 | 13-11/4 | $13-1 / 1 / 8$ | - | -- | - - | -- | - - | - - |
| Carlings, | , Number | $r$ on each side | 3 | 3 | 3 | - | - - | - - | - - | - - | - - |
|  | Broad |  | 0-10 | 0-9 | 0-8 | - |  | - - | - - | - - | - - |
|  | Deep |  | 0-8 | 0-7 | 0-6 | - | - - | - - | - - | - - | - - |

## $\begin{array}{ll}\text { Leges } & \text { Broad } \\ & \text { Deep }\end{array}$

To lye asunder from 9 to 12 inches
Carling short with long coamings of oak pricked down on the beams one inch.

Comings to lye above the deck $\quad$| $0-2$ | $0-2$ |
| :--- | :--- | :--- |

Broad with the rabbit

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| 0-43/4 | 0-41/2 | 0-41/2 | - - | - - | - - | - - | -- | - - |
| 0-41/4 | 0-4 | $0-31 / 2$ | - - | - - | - - | - - | - - | - - |



Partners for the masts the main to be carling broad
Deep
Foremast

| Mizenmast \& whipstaff Teer capstand |  |
| :---: | :---: |
|  | Thick |

To be bolted with bolts of
Capstand main teer diameter in the partners, including the whelps Length of the bars
Number of bars

| 1-5 | $1-41 / 2$ | 1-4 | -- | - - | - - | -- | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-6 | $1-51 / 2$ | 1-5 | - - | - - | - - | -- | - - | - - |
| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| 0-61/2 | 0-61/2 | 0-61/2 | - - | - - | - - | - - | - - | - - |
| 0-4 | 0-4 | 0-4 | - - | - - | - - | - - | - - | - - |
| 0-6 | 0-6 | 0-6 | - - | - - | - - | - - | - - | - |
| 0-3/4 | 0-3/4 | 0-5/8 | - - | - - | - - | - - | - - | - - |
| 2-1 | 2-0 | 1-11 | - - | - - | - - | -- | - - | - - |
| 14-0 | 13-6 | 13-0 | - - | - - | - - | - | - - | - - |
| $121 / 2$ | 12 | 12 | - - | - - | - - | - - | - - | - - |

Iron palls, four to each when they can be fitted, two of which to fall upon the heads of the trundale heads and to answer the palling on the deck where there are 6 whelps, each bolt to be drove through and cleanched, and if 5 whelps to be bolted with small bolts and cleanched on their barril.

Deck flat to be laid with English Oak in wake of the standards from the cook room forward in the middle of the deck flat, two strakes next the comings to be cocked \& bolted down to the hook \& transom to have two bolts in each beam to be prick'd down on the beam an inch
Thick
0-3
0-3
0-3

Plank thick
$0-4 \quad 0-4$
0-4
The rest to be laid with Prussia Deal

## Joshua Humphreys Notebook

Spirketing number of strakes on each side
Thickness in midships at

Plank or deal between spirketing or upper deck clamp Thick
Scupper lead number on each side

## Diameter in the clear

Standards all iron number of pair

The up \& down arm to reach the upper edge of the upper deck clamp \& a batts as near $y^{\mathrm{e}}$ upper end as conveniently may be had

The shortest arm
Long
Breadth
Thickness
Weight

Number and size of bolts in each

Turn'd piller \& the square

Bolts, ring \& eye for the ports, No \& size
Diameter in the clear

On the flat of the deck for the gun
Eye over the ports for lashing the guns

Diameter of their eye in the clear

Navy Office, August 1 ${ }^{\text {st }} 1737$ Dimensions

Length on the gundeck
Breadth extream
Depth in hold

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| 2 or 3 | 2 or 3 | 2 or 3 | -- | - - | - - | -- | -- | - - |
| 0-61/2 | 0-6 | 0-5 | - - | - - | - - | - - | - - | - - |
| 0-51/2 | 0-5 | 0-4 | - - | - - | -- | - - | - - | -- |
| 0-3 | 0-21/2 | 0-2 | - - | - - | - - | - - | - - | - - |
| 6 | 6 | 6 | - - | - - | - - | - - | - - | -- |
| 0-3 | 0-3 | 0-3 | -- | -- | -- | -- | - | -- |
| 7 | 6 | 5 | - - | - - | - - | - - | - - | - |

NOTE: There were no dimensions for breadth, thickness or weight)
$7-1^{1 / 8} \quad 7-1^{1 / 8} \quad 7-1$
$0-7 \quad 0-6^{1 / 2} \quad 0-6$
$4-1^{1 / 4} \quad 4-1 \frac{1}{4} \quad 4-1^{1 / 4}$

$1 \quad 1 \quad 1 \quad$ The rings to be sufficient only for hook \& tackles



| $174-0$ | $166-0$ | $158-0$ | $151-0$ | $144-0$ | $134-0$ | $124-0$ | - | $106-0$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $50-0$ | $47-9$ | $45-5$ | $43-5$ | $41-5$ | $38-6$ | $35-8$ | - | $30-6$ |
| $20-6$ | $19-6$ | $18-7$ | $17-9$ | $16-11$ | $15-9$ | $14-6$ | -- | $9-5$ |

## Joshua Humphreys Notebook

## Upper Deck

Clamps to be wrought anchor stock fashion with hook \& butt

| At the | upper edge thick | 0-6 | 0-51/2 | 0-5 | 0-5 | 0-5 | 0-4 | 0-4 | $0-31 / 2$ | 0-21/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | lower edge thick | 0-5 | $0-41 / 2$ | 0-4 | 0-4 | 0-4 | $0-311 / 2$ | 0-31/2 | 0-3 | 0-21/2 |
| Beams | Sided | 1-1 | $1-01 / 2$ | 0-11 | 0-1 | 0-0 | 0-101/2 | 0-91/2 | 0-9 | 081/2 |
|  | Moulded | 0-11 | $0-101 / 2$ | 0-8 | 0-11 | 0-10 | $0-81 / 2$ | 0-71/2 | 0-7 | 0-6 |

To lye under \& between each port where they can conveniently be placed \& as near as possible of the beams of the middle or gundeck \& under the great cabin in the distance of others to have a long carling under the furnace to take hold of the beam next abaft ye foremost \& that next ye foreside of the afterbitts

| The carlings to be Deep | - - | - - | - - | 1-01/2 | 0-111/2 | 0-101/2 | 0-9 | 0-8 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Broad | - - | - - | - - | 0-9 | 0-81/2 | 0-8 | 0-7 | 0-6 | - - |
| Knees double at each end hangg \& lodgg, sided The up \& down arm to reach the sperketing | $0-81 / 2$ | 0-8 | 0-71/2 | 0-7 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 |
| Shortest arm long if can be had | 3-6 | 3-5 | 3-4 | 3-3 | 3-2 | 3-1 | 3-0 | 2-11 | 2-10 |
| Number \& size of bolts in each | 6-1 | 6-1 | $6-7 / 8$ | 6-7/8 | 6-7/8 | 6-7/8 | 6-3/4 | 6-3/4 | 6-5/8 |

Upper Deck
$\begin{array}{ll}\text { Carlings } & \text { Broad } \\ & \text { Deep }\end{array}$
Carlings number of feet for each side except in the wake of the hatchways \&
Mainmast if there is to be 3 to the $1^{\text {st }}, 2^{\text {nd }} \& 3^{\text {rd }}$ rate ships

Short with long comings of oak on the prick'd down an inch into the beams

Commings above the deck

| $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{11 / 4}$ | $0-2^{1 / 4}$ | $0-2^{1 / 4}$ | $0-2$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $1-0$ | $0-11^{1 / 2}$ | $0-11$ | $0-11$ | $0-101 / 2$ | $0-10$ | $0-91 / 2$ | $0-9$ | $0-81 / 2$ |
|  |  |  |  |  |  |  |  |  |
| $0-4^{1 / 2}$ | $0-4$ | $0-4$ | $0-3^{1 / 2}$ | $0-3^{1 / 2} 2$ | $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-3^{11 / 4}$ | $0-3^{1 / 4}$ |
| $0-4$ | $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-3^{11 / 2}$ | $0-3^{1 / 2}$ | $0-3^{1 / 4}$ | $0-3^{1 / 4}$ | $0-3$ | $0-3$ |

## Joshua Humphreys Notebook

Waterways thick in the chine one inch more than the flat of the deck


| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1} / 2$ | $0-2^{1 / 2} 2$ | $0-2^{11 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2$ | $0-2$ |

Flatt two strakes next the commings to give scarph to each other \& to be pricked down an inch into the beam layed \& hooked into ye transoms \& deck hook \& bolted to $y^{e}$ beams deck hook \& transom to be oak the rest of the deck to be Prusia Deal.

Capstand, Tripple Teer diameter in the partners including the whelps
Barrs long
Number
$\mathrm{N}^{\mathrm{o}}$ of iron pauls

Main teer diameter in $y^{\mathrm{e}}$ partners including the whelps
Barrs long
Number
$\mathrm{N}^{\mathrm{o}}$ of iron pauls
Main heads to answer the pauls on the deck
Sperketing number of strakes on each side
Thickness at the Lower Edge
Upper Edge
Scupper lead number on each side
Diameter in the clear

| 1-7 | 1-6 | 1-5 | - - | - - | - - | - - | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-9 | 0-9 | 0-9 | - - | - - | - - | - - | - - | - - |
| 10 | 10 | 10 | - - | - - | - - | - - | - - | - - |
| 1 | 1 | 1 | -- | - - | -- | -- | - - | - - |
| - - | - - | - - | 1-10 | 1-9 | 1-8 | 1-7 | 1-5 | - - |
| - - | - - | - - | 12-0 | 11-6 | 10-6 | 10-6 | 9-0 | - - |
| - - | - - | - - | 12 | 12 | 12 | 10 | 10 | - |

four to each, two of wich to fall on the trundale

| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $0-4$ | $0-4$ | $0-4$ | $0-4$ | $0-4$ | 03 | $0-3$ | $0-3$ | $0-2$ |
| $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2^{1 / 2}$ | $0-2$ |
|  |  |  |  |  |  |  |  |  |
| 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| $0-3$ | $0-3$ | $0-3$ | $0-3$ | $0-3$ | $0-3^{1 / 2}$ | $0-3^{1 / 2}$ | $0-4^{1 / 2}$ | $0-4^{1 / 2}$ |

## Joshua Humphreys Notebook

Standards Irons number of pairs

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| 4 | 4 | 3 | 4 | 3 | 2 | 2 | 2 | 1 |
| -- | - | -- | -- | -- | - | -- | -- | - |
| -- | -- | -- | - | -- | -- | - | -- | - |
| -- | - | -- | - | -- | -- | - | -- | - |

The up \& down arm to reach $\mathrm{y}^{\mathrm{e}}$ upper edge of \& bolt thro the forecastle \& quarter deck clamps
The shortest arm long
Number \& size of bolts in each
String, in the wast thick in \& out
Collar beams square
Transom at the lower port cells deep

| $3-6$ | $3-5$ | $3-4$ | $3-3$ | $3-2$ | $3-1$ | $3-0$ | $2-11$ | $2-10$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Kneed at the end
Bitts, Main Topsail sheet \& jeer square
Jeer high above the deck
Topsail sheet \& jeer \& the crosspiece fore \& aft
Deep
Scored in the bitts

Bitts the crosspiece of the gallows sided
Deep
Long
Upper edge of it above the deck
Scored in
Bolts, ring \& eye for the ports No \& size of each
Diameter of the ring in the clear
On the flat of the deck for the guns, size
The ring to be only sufficient to hook the takles

| Eye for lashing the blocks on each side of the mainmast \& foremast | Size | 0-1/1/8 | 0-1/1/8 | 0-1/1/8 | 0-1 | 0-1 | 0-7/8 | 0-7/8 | 0-7/8 | 0-3/4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For the tackles | size | $0-13 / 4$ | $0-13 / 4$ | 0-11/2 | 0-11/2 | $0-13 / 8$ | $0-13 / 8$ | $0-13 / 8$ | 0-11/4 | 0-11/4 |

## Joshua Humphreys Notebook

All carling \& leges afore \& abaft where they are shorter to be made lessor than they are in $y^{e}$ midships

Quarter Deck

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |


| Clamps | Upper <br> Lower <br> Broad if can be had |
| :--- | :--- |


| $0-3$ | $0-3$ | $0-3$ | $0-3$ | $0-2^{1 / 2}$ | $0-2$ | $0-2$ | $0-2$ | $0-2$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $1-4$ | $1-3^{1 / 2}$ | $0-3$ | $1-2^{1 / 2}$ | $1-2$ | $1-1^{1 / 2}$ | $1-1$ | $1-01 / 2$ | $0-11$ |

Beams sided to have a small strap of iron round the timber to every $2^{\text {nd }}$ or $3^{\text {rd }}$ beams in the wake of the cabin

| Moulded | $0-91 / 2$ | $0-91 / 2$ | $0-8$ | $0-9$ | $0-8$ | $0-61 / 2$ | $0-6$ | $0-6$ | $0-51 / 2$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

To lye asunder from 2--4to 2--2each where they can conveniently be placed
In the great cabin to be bolded into the clamps at the ends with bolts of

Knees hanging sided

| $0-6 \frac{1}{2}$ | $0-6$ | $0-5 \frac{1}{2}$ | $0-5 \frac{1}{2}$ | $0-5$ | $0-4 \frac{1}{2}$ | $0-4 \frac{1}{2}$ | $0-4$ | - |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $3-0$ | $2-11$ | $2-10$ | $2-9$ | $2-8$ | $2-7$ | $2-6$ | $2-5$ | - |
| $5-7 / 8$ | $5-7 / 8$ | $5-3 / 4$ | $5-3 / 4$ | $5-3 / 4$ | $5-5 / 8$ | $5-5 / 8$ | $5-5 / 8$ | - |

Waterways thick in the chine one inch thicker than the plank of the deck

| String of oak in the great cabbin | Upper edge <br> Lower edge* |  | 0-6 | 0-6 | 0-51/2 | 0-51/2 | 0-51/4 | 0-5 | 0-4 | 0-4 | 0-21/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 0-31/2 | 0-31/2 | 0-3 | $1-2^{1 / 2}$ | 1-21/2 | $1-11 / 2$ | $1-11 / 2$ | $1-11 / 2$ | 1-0 |
| Greatings broad in the clear |  |  | 3-8 | 3-6 | 3-4 | 3-2 | 3-0 | 2-10 | 2-8 | 2-6 | -- |
| Sperketing | lower edge upper edge | thick <br> thick | 0-31/2 | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-2 | 0-2 | 0-2 |
| Quick work birthed up with deal of |  |  | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-11/2 | 0-11/2 | 0-11/2 | $0-1 / 1 / 2$ |
| Bolts Ring \& eye number \& size of each port Diameter of rings in the clear |  |  | 4-1 | 4-1 | 4-7/8 | 4-7/8 | 4-7/8 | $4-7 / 8$ | - - | 4-3/4 | - - |
|  |  |  | 0-4 | 0-4 | 0-3/4 | 0-33/4 | 0-31/2 | 0-31/2 | - - | 0-31/4 | -- |

## Joshua Humphreys Notebook

Forecastle

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |


| Clamps | Thick |
| :--- | :--- |
| Beams | Broad |
| Sided |  |
|  | Moulded |
|  | Asunder |


| $0-41 / 2$ | $0-4$ | $0-4$ | $0-4$ | $0-4$ | $0-3$ | $0-3$ | $0-3$ | -- |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $1-3$ | $1-3$ | $1-3$ | $1-3$ | $1-3$ | $1-2$ | $1-2$ | $1-2$ | -- |
| $0-91 / 2$ | $0-9$ | $0-71 / 2$ | $0-7$ | $0-71 / 2$ | $0-61 / 2$ | $0-6$ | $0-6$ | -- |
| $0-71 / 2$ | $0-7$ | 6 | $0-7$ | $0-6$ | $0-5^{1 / 2} 2$ | $0-5$ | $0-5$ | - |
| $2-0$ | $2-0$ | $2-0$ | $2-0$ | $2-0$ | $2-0$ | $2-0$ | $2-0$ | $2-0$ |

At the bulkhead furnace \& fireplace to be double kneed and all the other to be single kneed

*These numbers are clear in Humphreys' original notes, but the 0 feet for the $100,90 \mathcal{E} 80$ gun ships do not seem correct in proportion to the other specifications.
The up \& down arm long to reach the sperketing Shortest arm long

Number \& size of bolts in each
Waterways thick in the chine - one inch thicker than the deck

| Beams at the forepart of the forecastle | Broad or double | $2-6$ | $2-5$ | $2-4$ | $2-3$ | $2-2$ | $2-0$ | $1-10$ | $1-9$ |
| :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| To fasten the catheads | Deep under y rabbit of y deck | $0-71 / 2$ | $0-7$ | $0-7$ | $0-7$ | $0-6$ | $0-51 / 2$ | $0-5$ | $0-5$ |

To be stept well with a double slope in the collar beam and scored into the stantions at the forecastle beam no more than $1 / 2$ an inch thick \& that to be shouldered into the beams
Cathead Fore \& aft
Stantions for the beakhead square
Up \& down

Bitts foretopsail sheet and jeer square to meet in the middle Height above the deck

Crosspiece Fore \& aft
Deep
Scored in the bitts

| 1-7 | 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | $1-11 / 2$ | 0-11 | 0-91/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0-6 | 0-6 | 0-6 | 0-51/2 | 0-51/2 | 0-51/2 | 0-41/2 | 0-41/2 | - - |
| 1-6 | 1-5 | 1-4 | 1-3 | 1-2 | $1-01 / 4$ | 0-11 | 0-10 | 0-9 |
| 0-111/2 | 0-11 | 0-101/2 | 0-91/2 | 0-81/2 | 0-73/4 | 0-7 | 0-61/4 | 0-6 |
| 3-10 | 3-9 | 3-8 | 3-7 | 3-6 | 3-5 | 3-4 | 3-3 | 3-2 |
| 0-10 | 0-91/2 | 0-9 | $0-81 / 2$ | 0-8 | 0-71/2 | 0-7 | 0-61/2 | 0-6 |
| 0-81/2 | 0-81/2 | 0-8 | 0-71/2 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 |
| 0-11/2 | 0-11/2 | 0-11/2 | 0-11/2 | 0-11/2 | 0-11/2 | 0-11/2 | $0-11 / 2$ | 0-11/2 |

## Joshua Humphreys Notebook

Bolts spanshakles (the corners of the shackles to be rounded) Size of bolts

Eye $\mathrm{D}^{\circ}$ for the main topmast stay

Round House
\(\left.$$
\begin{array}{ll}\text { String } & \begin{array}{l}\text { Thick } \\
\text { Broad }\end{array}
$$ <br>
Beams \& \left.\begin{array}{l}Sided <br>
Moulded <br>

Asunder\end{array}\right\}\end{array}\right\}\)| to have a small strap of ;iron round the timber, |
| :--- |
| bolted to every other beam |

To be bolted into the clamps at each end with bolts of
Knees at the bulkhead Hanging Sided
Up \& down arm to reach the sperketing
Shortest arm Long

Number \& size of bolts

Waterways thick in the chine one inch thicker than the plank of the deck
Top Gallant Roundhouse

| String or clamps | Thick <br> Broad |  |
| :--- | :--- | :--- |
| Beams $\quad$Sided <br> Moulded <br> To lye asunder | to have a small strap of ;iron round the timber, <br> bolted to every other beam |  |
| Waterways thick in the chine |  |  |


| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $0-17 / 8$ | 0-14 3 /4 | $0-13 / 4$ | 0-11/2 | $0-13 / 8$ | $0-13 / 8$ | $0-13 / 8$ | 0-11/4 | $0-11 / 4$ |
| 0-11/4 | 0-11/4 | 0-11/4 | $0-1{ }^{1 / 8}$ | $0-1^{1 / 8}$ | $0-1{ }^{1 / 8}$ | 0-1 | 0-1 | 0-1 |


| 0-4 | 0-4 | 0-3 | 0-4 | 0-4 | 0-3 | 0-2 | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-1 | 1-01/2 | 1-0 | 0-111/2 | 0-11 | 0-101/2 | 0-10 | - - | - - |
| 0-7 | 0-7 | 0-6 | 0-61/2 | 0-61/2 | 0-41/2 | 0-4 | - - |  |
| 0-51/2 | 0-51/2 | 0-41/2 | 0-5 | 0-5 | 0-31/2 | 0-3 | - - |  |
| 2-0 | 2-0 | 2-0 | 2-0 | 2-0 | 2-0 | 2-0 | - - | - - |
| 0-5/8 | 0-5/8 | 0-5/8 | 0-5/8 | 0-5/8 | 0-1/4 | 0-1/4 | - - | - - |
| 0-51/2 | 0-5 | 0-41/2 | 0-4 | 0-4 | 0-4 | $0-31 / 2$ | - - | - - |
| 2-6 | 2-5 | 2-3 | 2-4 | 2-3 | 2-3 | 2-3 | - - | - - |
| 5-5/8 | 5-5/8 | $5-5 / 8$ | 5-5/8 | 5-5/8 | $5-5 / 8$ | 5-5/8 | - - |  |


| 0-3 | - | - - | - - | - - | - - | - | - - | - - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-0 | - - | - - | - - | -- | - - | - - | - | - - |
| 0-6 | - - | - - | - - | - - | - - | - - | - - | - - |
| 0-41/2 | - - | - - | - - | - - | - - | - - | - - | - - |
| 2-0 | - - | - - | - - | - - | - - | - - | - - | - - |
| 0-3 | - - | - - | - - | - - | - - | - - | -- | - - |

## Top Gallant Roundhouse

To be bolted into the string at each end with bolts of

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :---: | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |

Flatt of the deck thick
0-5/8
0-2
Gunnel to the toprail deep0-6

NB No holes to be board in the timber when first cut up except one for a wianclog nor any trunails holes in the wake of the ring \& eyebolts for the ports, chain bolts or any other bolts that may sufficiently fasten the work without trunails. All thick stuff, plan, \&c of 10 in . broad \& under to be only cross board cabin \& all other joynes work to be fram'd and pannel'd with deal from where it may conveniently be done. The port cells on each deep to cant out $1 / 2$ an inch from a level from the inside height, all beams to be moulded ${ }^{1 / 12}$ less at the ends than in the middle.

Without Board

Whales, main \& the stuff between to be of an equal thickness to be worked with hook \& butt

| Deep from the upper to the lower edge | 5-2 | 4-10 | 4-6 | 4-2 | 3-10 | 3-6 | 3-2 | 2-10 | 2-6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thick | 0-10 | 0-9 | 0-81/2 | 0-71/2 | 0-7 | 0-51/4 | 0-5 | 0-5 | 0-4 |
| rake above them Thick | 0-8 | 0-7 | 0-61/2 | 0-6 | 0-51/4 | 0-4 | 0-4 | 0-4 | 0-3 |
| To be cypher'd at the upper edge | 0-1 | 0-1 | 0-1 | 0-1 | 0-1 | 0-1 | 0-1 | 0-1 | 0-1/2 |
| strakes below the whales number | 7 | 6 | 5 | 5 | 4 | 2 | 2 | 1 | 1 |
| ess of the upper edge of the upper strake | 0-8 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-4 | 0-4 | 0-4 | 0-3 |
| Low D ${ }^{\text {o }}$ | 0-4 | 0-4 | 0-4 | 0-4 | 0-4 | 0-3 | 0-3 | 0-3 | 0-2 |

The rest of the plank under the thickstuff to be brought full to these thickness at the floorheads

Whales, Channels, Broad from the upr to the lowr ${ }^{r}$ edge
To be wrought all of a thickness
Thick
The strake above \& below them thick \& to increase gradually to the cypher'd strake above the whales

| -- | $0-4$ | $0-4$ | $0-4$ | $0-4$ | $0-3$ | $0-3$ | $0-3$ | $0-2$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $2-9$ | $2-8$ | $2-6 \frac{1}{2}$ | $2-5$ | $2-4$ | $2-2^{1 / 2}$ | $2-2^{1 / 2} 2$ | $2-0$ | -- |
| $0-5^{1 / 2}$ | $0-5^{1 / 2}$ | $0-51 / 4$ | $0-5$ | $0-4$ | $0-4$ | $0-3^{11 / 2}$ | $0-3^{11 / 2}$ | -- |
| $0-4$ | $0-4$ | $0-4$ | $0-4$ | $0-3$ | $0-3$ | $0-2^{11 / 2}$ | $0-2^{11 / 2}$ | -- |

## Joshua Humphreys Notebook

| $\begin{array}{ll}\text { Sheer or string in too strakes } & \begin{array}{c}\text { Broad } \\ \text { Thick }\end{array}\end{array}$ | 2-3 | 2-2 | 2-1 | - - | - - | - - | -- | -- | -- |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0-4 | 0-4 | 0-4 | - - | - - | - - | - - | -- | -- |
| Strake above \& below them thick | 0-3 | 0-3 | 0-3 | - - | - - | - - | - - | - - | - - |
| Deal in the wast at the top of the side Thick | 0-21/2 | 0-21/2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 |
| Channels Main long (if ports well admitted) | 38-0 | 35-6 | 33-0 | 30-6 | 28-0 | 25-6 | 23-0 | 20-0 | 17-0 |
| Broad at the foremost end | 2-10 | 2-6 | 2-8 | 2-6 | 2-4 | 2-2 | 1-11 | 1-9 | 1-7 |
| but sufficient to carry the shrouds clear of the gunnell \& fife rail Thickness at the inner edge | 0-6 | 0-6 | 0-51/2 | 0-51/2 | 0-51/2 | 0-5 | 0-41/2 | 0-4 | 0-4 |
| Outer $\mathrm{D}^{\circ}$ | 0-41/2 | 0-41/2 | 0-41/2 | 0-4 | 0-4 | 0-31/2 | 0-3 | 0-23/4 | 0-21/2 |
| No \& size of bolts for fastening | $10-1{ }^{1 / 8}$ | 10-11/8 | 9-1 | 9-1 | 8-1 | 7-7/8 | 7-7/8 | 6-3/4 | 5-3/4 |
| Fore long (if the ports will admit) | 31-10 | 29-- | 27-0 | 05-0 | 23-0 | 21-0 | 19-0 | 17-0 | 15-0 |
| Breadth at the after end but however sufficient to carry the shrouds clear of the gunnell | 2-8 | 2-6 | 2-4 | 2-2 | 2-0 | 1-10 | 1-8 | 1-6 | 1-4 |
| Thickness at the Inner Edge <br> Outer Edge | 0-6 | 0-6 | 0-53/4 | 0-51/2 | 0-51/4 | 0-5 | 0-41/2 | 0-4 | 0-4 |
|  | 0-41/2 | 0-41/2 | $0-41 / 2$ | 0-4 | 0-4 | 0-31/2 | 0-3 | 0-23/4 | $0-2^{3 / 4}$ |
| No \& size of bolts for fastning | $9-1 / 1 / 8$ | $9-1 /{ }^{1 / 8}$ | 8-1 | 8-1 | 7-1 | $6-7 / 8$ | $6-7 / 8$ | 5-3/4 | 5-3/4 |
| Mizen Long But however sufficient to carry the | 17-6 | 16-0 | $14^{*} 6$ | $13-6$ | 12-6 | 11-6 | 10-6 | 9-0 | 7-6 |
| $\text { Breadth }\{\quad \text { shrouds clear of the gunnels \& fife rails }$ | 2-1 | $1-11112$ | 1-10 | $1-81 / 2$ | 1-7 | $1-51 / 2$ | 1-4 | $121 / 2$ | 1-1 |
| Thickness at the Inner Edge Outer Edge | 0-5 | 0-5 | 0-4/4 | 0-41/4 | 0-4 | 0-31/2 | 0-3 | 0-23/4 | 0-21/2 |
|  | 0-31/2 | 0-31/2 | 0-31/4 | 0-3 | 0-3 | 0-21/2 | 0-2 | 0-2 | $0-13 / 4$ |
| No \& size of bolts for fastning | 5-7/8 | $5-7 / 8$ | 5-7/8 | 5-7/8 | 4-7/8 | 4-3/4 | $3-3 / 4$ | 3-3/4 | 3-3/4 |

## Joshua Humphreys Notebook

| Chain plates main \& fore broad | 0-4 | 0-4 | $0-3 / 1 / 8$ | 0-33/4 | 0-31/2 | 0-31/4 | 0-3 | 0-23/4 | 0-21/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thick In the middle | 0-11/2 | 0-11/2 | 0-11/2 | 0-13/4 | 0-13/4 | 0-1/4 | $0-1{ }^{1 / 8}$ | 0-1 | 0-7/8 |
| At the eye | 0-1 | 0-1 | 0-1 | $0-7 / 8$ | 0-7/8 | $0-7 / 8$ | 0-3/4 | 0-3/8 | 0-1/4 |
| Size of the bolt | -15 | 0-11/2 | -11/2 | $0-11 /$ | 0-13/ | 0-11/4 | 0-11/4 | -1 | 0-11/ |

Platings \& backstays for the main \& fore chains to have the breadth \& thickness \& the same sized as the mizzen chainplates


## Joshua Humphreys Notebook

|  | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| Lower pintle only to be | 1-5 | 1-41/2 | 1-31/2 | 1-21/4 | 1-2 | 1-11/4 | 1-03/4 | 0-11 1 /4 | 0-11 |
| Braces for straps for pintles broad | 0-5 | 0-43/4 | 0-41/2 | 0-41/4 | 0-4 | $0-33 / 4$ | 0-31/2 | 0-31/4 | 0-3 |
| Thick in the shoulder at the return | 0-21/8 | 0-2 | 0-1/78 | 0-13/4 | 0-15/8 | 0-11/2 | 0-11/4 | 0-11/4 | 0-1/8 |

To have a strap of iron on the back \& at each corner an eye well clenched on the inside of the straps of sufficient bigness to receive an oval ring

| ChaftersFenders |  | - - | - - | - - | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 | 0-41/2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 0-4 | 0-4 | 0-4 | 0-3 | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-2 $2^{1 / 2}$ |
| Against the hatchways asunder |  | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 | 1-4 |
| Linings of the anchor | Thick | 0-3 | 0-3 | 0-3 | 0-21/2 | 0-21/2 | 0-21/2 | 0-2 | 0-2 | 0-2 |
| Navelings between the hold | Thick | 0-9 | 0-81/2 | 0-8 | 0-71/2 | 0-7 | 0-61/2 | 0-61/2 | 0-51/2 | 0-51/2 |
| Bolt holes to be bored | Size | 0-1 | 0-1 | 0-1 | 0-1 | 0-7/8 | 0-3/4 | 0-3/4 | 0-5/8 | 0-5/8 |
| Rails on the beakhead the shear Broad |  | 0-101/2 | 0-10 | 0-91/2 | $0-81 / 2$ | 0-8 | 0-71/2 | 0-7 | 0-61/2 | 0-51/2 |
|  | Thick | 0-4 | 0-33/4 | 0-31/2 | 0-31/4 | 0-3 | 0-3 | $0-23 / 4$ | 0-21/2 | 0-21/4 |
| Afterdrift | Broad | 0-71/2 | 0-7 | 0-61/2 | 0-6 | 0-51/2 | 0-5 | 0-43/4 | 0-41/2 | 0-4 |
|  | Thick | 0-33/4 | 0-31/2 | 0-31/4 | 0-3 | 0-3 | 0-23/4 | 0-23/4 | 0-21/2 | 0-21/2 |
| Plank shier in the wast Drift | Thick | 0-3 | 0-3 | 0-21/2 | 0-3 | 0-2 $\mathbf{2}^{1 / 2}$ | 0-21/2 | - - | -- | - - |
|  | Thick | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 | 0-2 |
| Waist Rail | Broad | 0-81/2 | 0-71/2 | 0-61/2 | 0-6 | 0-51/2 | 0-5 | 0-43/4 | 0-41/4 | 0-4 |
|  | Thick | 0-41/2 | 0-4 | 0-33/4 | 0-33/4 | 0-33/4 | ---- | plan | here - |  |

To be struck with a astride within and without the square to overhang the plank or deal half an inch within the board or without

| Shank painter chains | Long | 20-6 | 19-0 | 17-6 | 16-0 | 15-0 | 14-0 | 13-0 | 12-0 | 10-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Size of links | 11/16 | 1 | 15/16 | 15/16 | $7 / 8$ | $7 / 8$ | 10/16 | 10/16 | $3 / 4$ |
| Port hinges for the gundeck | Broad | 0-3/18 | 0-37/8 | 0-33/4 | 0-3/8 | 0-31/2 | $0-33 / 8$ | 0-31/4 | 0-27/8 | - - |
|  | Thick | $0-1 /{ }^{1 / 8}$ | $0-1{ }^{1 / 8}$ | 0-1 | 0-1 | 0-7/8 | 0-3/4 | 0-3/4 | 0-5/8 | - - |
|  |  | 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
|  |  | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |

## Joshua Humphreys Notebook



## Joshua Humphreys Notebook

The Head

Head - place the upper edge of the upper rail of the head on the first and second rails at height of the upper deckline \& for third, $4^{\text {th }}, 5$ \& 6 rail at $\mathrm{y}^{\mathrm{e}}$ height of the lower port cells of the upper deck that the chase guns may fire over the rail. You may place the throat of the knee of the head at the height of the gundeck \& crown of the lyon as high as the upper sheer rail afore \& between the throat of the knee and the crown of the lyon divided into five parts and set one of them down by a perpendicular from the top of the lyon for the upper part of the knee of the head and middle between the top of the knee \& throat of $\mathrm{D}^{\circ}$ for the lower part of the lyon.

Length of the head from the foreside of the stem to the
Foreside of the knee of the head

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $1-66$ | $15-6$ | $13-6$ | $11-6$ | $10-6$ | $9-6$ | $8-6$ | $7-6$ | $7-0$ |
| $9-0$ | $8-6$ | $8-0$ | $7-0$ | $6-6$ | $6-0$ | $5-6$ | $5-0$ | -- |
| $1-1$ | $1-0$ | $0-11$ | $0-10$ | $0-9$ | $0-8$ | $0-71 / 2$ | $0-61 / 2$ | $0-6$ |
| $1-2$ | $1-1$ | $1-1$ | $0-11$ | $0-10$ | $1-91 / 2$ | $0-81 / 2$ | $0-71 / 2$ | $0-61 / 2$ |
|  |  |  |  |  |  |  |  |  |
| $13-6$ | $12-6$ | $11-6$ | $10-6$ | $9-6$ | $9-0$ | $8-6$ | $7-6$ | $6-6$ |
|  |  |  |  |  |  |  |  |  |
| $1-2$ | $1-1$ | $1-1 / 2$ | $0-11^{1} / 2$ | $0-101 / 2$ | $0-91 / 2$ | $0-9$ | $0-8$ | $0-7$ |
| $0-101 / 4$ | $0-93 / 4$ | $0-91 / 4$ | $0-83 / 4$ | $0-8$ | $0-71^{1 / 4}$ | $0-6^{3 / 4}$ | $0-6$ | $0-51 / 4$ |

Rails to
And the foremost end to be $2 / 3$ of the after end and the rest of the rails to be $2 / 3$ of one another at the afterend, \& to diminish in the same proportion
The timbers of the head sided $\left\{\begin{array}{l}\text { From } \\ \text { To }\end{array}\right.$

Gallerys

The length fore \& aft to be as long as the head is from the fore part of the stem, and the rails to follow the shear of the ship and to answer with stern rails. But now it is customary to make the gallery so little that there is hardly any rule exactly followed, but commonly according as approved of when the ship is built.

## Of Placing of Drifts

Place the drift at the entering place $5 / 9$ of the length of the lower deck from afore, but some place the center of the mast that is the mast drive $1 / 2$ the length of your lower deck and twice the diameter and $1 / 4$ the mast more abaft the middle but observe that you have not upper deck port in the wake of your steps.

Place your foremast drift as you may have two ports close in the forecastle, and three in the steerage besides one in the cabin. Depth of drifts as you design to get height for a roundhouse or not, but let you midship drift cover your mast. Set off your length on the gun deck and so square the breadth of the steps up to the top of the side or to the middle deck and space a port just afore or just abaft. Then space a bow port with regards to the lining of the anchor \& abaft the gunners cabin then space the rest at an equal distance one from another.

Dimensions of Jeer Capstands

Six whelps in the upper jeer barrel \& five whelps in the lower, diameter of upper barrel, diameter of the partners, proportions for the whelps and size of the barr holes to be as the main capstand.

Length of the upper barrel to the lower part of $y^{e}$ drumhead
Diameter of the lower barrel when brought into $y^{e}$ square
Diameter of the drumhead
Half thickness of the drumhead
Sett in hole in the drumhead square
Diameter of the spindle $1 / 2$ the lower barrel
Trundale head Thickness of the Upper piece
Lower piece

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| 3-0 | 3-0 | 3-0 | 3-01 | 3-0 | 3-0 | 3-0 | 3-0 | 3-0 |
| 2-3 | 2-2 | 2-1 | 2-0 | 1-11 | 1-10 | 1-9 | 1-8 | 1-5 |
| 5-0 | 4-101/2 | 4-9 | 4-71/2 | 4-6 | 4-41/2 | 4-3 | 4-1/2 | 4-0 |
| 0-7 | 0-7 | 0-7 | 0-7 | 0-61/2 | 0-61/2 | 0-6 | 0-51/2 | 0-51/2 |
| 1-5 | 1-5 | 1-41/2 | 1-4 | 1-31/2 | 1-3 | 1-2 | 1-01/2 | 1-0 |
| 1-11/2 | 1-1 | 1-01/4 | 1-0 | 0-111/2 | 0-111/2 | 0-101/2 | 0-91/2 | $0-81 / 2$ |
| 0-6 | 0-6 | 0-6 | 0-53/4 | 0-51/2 | 0-51/4 | 0-5 | 0-5 | 0-43/4 |
| 0-5 | 0-5 | 0-5 | $0-43 / 4$ | $0-41 / 4$ | $0-41 / 4$ | 0-4 | 0-4 | 0-33/4 |

Main Capstand
Diamiter of the barril
Ditto of the partners
Length of the upper barrel to the lower part of the drumhead
Diamiter of the spindle $2 / 3$ of the partners
In the steps
Number of whelps

| $2-5$ | $2-4$ | $2-3$ | $2-2$ | $2-1$ | $2-0$ | $1-11$ | $1-9$ | $1-7$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $2-1$ | $2-0$ | $1-11$ | $1-10$ | $1-9$ | $0-8$ | $0-7$ | $1-5$ | $1-3$ |
|  |  |  |  |  |  |  |  |  |
| $3-3$ | $3-3$ | $3-3$ | $3-3$ | $3-3$ | $3-3$ | $3-3$ | $3-3$ | $3-3$ |
|  |  |  |  |  |  |  |  |  |
| $1-5$ | $1-4$ | $1-3^{1 / 3} 3$ | $1-2^{2 / 3}$ | $1-2$ | $1-1^{1 / 3}$ | $1-0^{1 / 3}$ | $0-11^{2 / 3}$ | $0-10$ |
| $1-1^{1 / 2}$ | $1-1$ | $1-0^{1 / 2}$ | $1-0$ | $0-11^{1 / 2} 2$ | $0-11$ | $0-10^{1 / 2}$ | $0-91 / 2$ | $0-81 / 2$ |
| 6 | 6 | 6 | 66 | 6 | 6 | 6 | 6 | 6 |

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Whelps deep at the lower end $1 / 2$ the diameter of the barrels at the upper end $2 / 3$ of the lower end; also at the surge end $2 / 3$ of the lower end

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft -In | Ft -In | Ft -In | Ft -In | Ft -In | Ft -In | Ft -In | Ft -In |

Length of the surge (blank) of the length of the whelps

| Diamiter of the drumheads |  | 5-11/2 | 5-0 | 4-101/2 | 4-9 | 4-71/2 | 4-6 | 4-41/2 | 4-3 | 4-0 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Barr holes square at the outside |  | 0-43/4 | 0-43/4 | 0-43/4 | 0-41/2 | 0-41/4 | 0-4 | 0-4 | 0-4 | 0-4 |
| Inner end |  | 0-31/2 | 0-31/2 | 0-31/2 | 0-31/2 | 0-31/2 | 0-3 | 0-3 | 0-3 | 0-3 |
| Chocks | Upper thick | 0-21/2 | 0-21/2 | 0-21/2 | 0-21/2 | 0-21/2 | 0-2 | 0-2 | 0-2 | 0-2 |
|  | Lower Thick | 0-4 | 0-4 | 0-4 | 0-33/4 | 0-31/2 | 0-31/4 | 0-3 | 0-3 | 0-23/4 |

For a jeer capstand, the upper barrel not to exceed 3 feet in length, the lower end of the whelps to be $1 / 2$ the diameter of the barrel; the whelps to surge 2 inches in a foot.
The length of the head $1 / 3$ the length of the whelps.
Allowing $21 / 2$ or 3 inches for the stop of the head, and let the upper part of the head to be one inch shallower than the lower part of the head. Let all the whelps taper 1 $1 / 2$ inches on each side in a foot drop.
The partners ought to be at least 2 inches of a side less than the upper barrel and of a sufficient length to be left the capstand high enough for to shift the vial.
The lower barrel to be $3 / 4$ of an inch bigger on each side than the partners that the whelps may not be set to far into the barrel, the lower whelps to be $5 / 9$ of the length from the end of the upper whelps, the lower end of the whelps to be $3 / 5$ of the lower barrel and to taper 2 inches in a foot in the length of the surge the head to follow the same tapering, allowing at least 3 inches slop
The length of the head something less than $1 / 3$ the length of the whelps. The spindle ought at least to be $1 / 2$ the lower barrel in length as you please \& conveniently will serve.
The drum head ought to overhand the lower end of the whelps 2 inches round and the thickness according to the bigness of the barr holes.
These proportions differ somewhat from the Old Rule but our opinions make much handsomer capstands.

## Dimensions for Main Capstand

For a main capstand but little to be said, for there is no reason why it should be any bigger in the partners than the Jeer, considering that the number of men that will heave the jeer to pieces will not be able to wrong the main; for considering the distance from the barrs to the vial in the jeer capstands \& how near together they are in the main, the whelps of the main capstand may be something longer than 3 feet because there is the use in the deck as with the jeer. The lower edge of the spindle is to be half the partners then proceeding in everything else as with the upper barrel of the jeer.

An abstract of numbers, natures, lengths \& weight of cannon

An abstract of numbers, natures, lengths \& weight of cannon according to several rates of ships as proposed at a meeting of Flag Office and established by His Majestic Council on the $6^{\text {th }}$ of July, 1716.

| Rates | Guns | Decks | No. of guns on each deck | Nature of gunsPounders | Length |  | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Ft | In |  |
| $1^{\text {st }}$ | 100 | Lower | 28 | 42 or 32 | 10 | 0 | 55 |
|  |  | Middle | 28 | 24 | 10 | 0 | 48 |
|  |  | Upper | 28 | 12 | 9 | 6 | 34 |
|  |  | Quarter | 12 | 6 | 9 | 0 | 24 |
|  |  | Forecastle | 4 | 6 | 9 | 0 | 24 |
| $2^{\text {nd }}$ | 90 | Lower | 26 | 32 | 9 | 6 | 52 |
|  |  | Middle | 26 | 18 | 9 | 6 | 42 |
|  |  | Upper | 26 | 9 | 9 | 6 | 29 |
|  |  | Quarter | 10 | 6 | 9 | 0 | 24 |
|  |  | Forecastle | 2 | 6 | 9 | 0 | 24 |
| $3^{\text {rd }}$ | 100 | Lower | 26 | 32 | 9 | 6 | 53 |
|  |  | Middle | 26 | 12 | 9 | 6 | 34 |
|  |  | Upper | 24 | 6 | 9 | 0 | 24 |
|  |  | Quarter | 14 | 6 | 9 | 0 | 20 |
| Rates | Guns | Decks | No. of guns on each deck | Nature of gunsPounders | Length |  |  |
|  |  |  |  |  | Ft | In | Weight |
| $3^{\text {rd }}$ | 70 | ¢ Lower | 26 | 24 | 9 | 6 | 46 |
|  |  | Upper | 26 | 12 | 9 | 0 | 32 |
|  |  | \{ Quarter | 14 | 6 | 8 | 0 | 20 |
|  |  | Forecastle | 4 | 6 | 2-9 |  | 24 |
|  |  | ( |  |  |  |  | 20 |
| $4^{\text {th }}$ | 60 | ¢ Lower | 24 | 24 | 9 | 6 | 46 |
|  |  | U Upper | 26 | 9 | 9 | 0 | 29 |
|  |  | \{ Quarter | 8 | 6 | 8 | 0 | 20 |
|  |  | Forecastle | 2 | 48 | 8 | 0 | 20 |
|  |  |  |  |  |  |  |  |

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| $4^{\text {th }}$ | 50 | Lower | 22 | 18 | 9 | 0 | 36 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Upper | 22 | 9 | 8 | 6 | 26 |
|  |  | Quarter | 4 | 6 | 8 | 0 | 20 |
|  |  | Forecastle | 2 | 6 | 9 | 0 | 24 |
| 5th | 40 | \{ Lower | 20 | 12 | 9 | 0 | 31 |
|  |  | \{ Upper | 20 | 6 | 8 | 6 | 32 |
| $5^{\text {th }}$ | 30 | \{ Lower | 8 | 9 | 8 | 6 | 26 |
|  |  | $\{$ Upper | 20 | 6 | 8 | 0 | 20 |
|  |  | Quarter | 2 | 4 | 7 | 6 | 16 |
| $6^{\text {th }}$ | 30 | Upper | 20 | 6 | 7 | 6 | 18 |

Dimensions of ships carriages, etc.

Dimensions of ships carriages, exeltress different length According to the new regulations

## Pounders

Guns Length (Feet)
Brackets $\begin{cases}\text { Wooden keys for the bottom } & \left\{\begin{array}{l}\text { Length } \\ \text { Breadth } \\ \text { Thickness }\end{array}\right. \\ \text { Key Pins } & \left\{\begin{array}{l}\text { Length } \\ \text { Breadth }\end{array}\right.\end{cases}$

Trucks for the under mentioned cannon of

| 32 | 24 | 18 | 12 | 9 | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 10.0-9.6 | 10.0-9.6 | 9.6-9.0 | 9.6-9.0-8.6 | 9.6-9.0-8.6 | 9.6-9.0-8.6 |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| 0-103/8 | 0-93/4 | 0-91/4 | 0-81/4 | 0-81/4 | 0-71/4 |
| 0-4 | 0-4 | 0-4 | 0-31/4 | 0-31/4 | 0-31/4 |
| 0-11/2 | 0-11/2 | 0-11/4 | $0-1 /{ }^{1 / 8}$ | $0-1^{1 / 8}$ | 0-1 |
| 0-7 | 0-7 | 0-7 | 0-7 | 0-61/2 | 0-6 |
| 0-3/4 | 0-3/4 | 0-3/4 | 0-3/4 | 0-3/4 | 0-3/4 |

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| Stepps $\quad\left\{\begin{array}{l}\text { Length }\end{array}\right.$ | $0.51 / 2-0.5$ | $3.7{ }^{1 / 8}-0.6^{7 / 8}$ |  | 0.7-0.6 ${ }^{3} / 4$ | $0.6112-0.613 / 4$ |  | $0.61 / 2-0.61 / 40.6-0.51 / 2$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |
|  |  | 0-41/2 | 0-4 | 0-33/4 | 0-31/4 | $0-31 / 8$ | 0-23/4 |
| Iron joints center from the fore port |  | 0-11 | 0-101/2 | 0-101/2 | 0-91/4 | 0-8 | 0-8 |
| Sinking of the iron joints center |  | $0-1{ }^{1 / 8}$ | $0-1{ }^{1 / 8}$ | 0-1 | 0-1 | 0-1 | 0-1 |
| Iron joints semidiamiter |  | $0-31 / 8$ | $0-2^{7 / 8}$ | $0-2^{5 / 8}$ | $0-2^{3 / 8}$ | $0-2^{1 / 8}$ | $0-1{ }^{7 / 8}$ |
| Wooden keys for bottom | $\int$ Length | 0-8 | 0-8 | 0-8 | 0-8 | 0-8 | 0-8 |
|  | \{ Breadth | 0-5 | 0-5 | 0-5 | 0-41/2 | 0-41/2 | 0-41/4 |
|  | Thickness | 0-13/4 | 0-11/4 | 0-11/4 | $0-1{ }^{1 / 8}$ | $0-1{ }^{1 / 8}$ | 0-11/2 |

The Rule Whereby the Proportions of Masts \& Yards is Cast

To find the length of the masts.

Multiply the extream breadth of $1^{\text {st }}, 2^{\text {nd, }} 3^{\text {rd }}$ rates of 80 guns by 2.28 ,
$4^{\text {th }}$ rates of 50 guns by 2.36
$6^{\text {th }}$ rates of 20 guns by 2.42
The foremast
Bowsprit
9/10 of the mainmast of the $1^{\text {st }}$ and 2 rates ${ }^{11 / 18}$ and

| Maintopmast | $13 / 18$ of the mainmast | Foretopmast |
| :--- | :--- | :--- |
| Mizzen topmast | $6 / 7$ of the maintopmasts | Spritsail topmast |

$3^{\text {rd }}$ rates of 70 guns by 2.32
$5^{\text {th }}$ rates of 40 guns by $2.38 \quad 5^{\text {th }}$ rates of 30 guns by 2.4
This gives the length of the mainmast in feet.

Mizenmast of all but $6^{\text {th }}$ rates ${ }^{11 / 13}$
the 6 rates ${ }^{8 /} 10$ of the main mast.
of all other rates ${ }^{13 / 19}$ of the mainmasts
15/ 16 of the maintopmast $\quad$ Top gallant masts 30/61 of their topmasts
$3 / 8$ of the bowsprit where used

Flying gibboom 6 feet less than breadth of the ship

To find the diameter of the masts
For the main \& foremasts of the $1^{\text {st }}, 2^{\text {nd }}, 3^{\text {rd }}$ rates of 80 guns of 4 rates of 60 guns of $5^{\text {th }}$ rates of 40 guns $\& 30$ guns

Maintopmast $\quad 9 / 10$ of an inch to a yard.
$\left.\begin{array}{l}\text { One } \\ 27 / 28 \\ 9 / 10\end{array}\right\}$ Inch to a yard $\left.\begin{array}{cc}3^{\text {rd }} \text { rates of } 70 \text { guns } & 31 / 33 \\ \text { of } 4 \text { th rates of } 50 \text { guns } \\ \text { of } 6 \text { rates of } 20 \text { guns } & 9 / 10 \\ 9 / 10\end{array}\right\} \quad$ Inch to a yard

Foretopmast to be as big in the cap as the maintopgallant masts Spritsail topmast an inch to a yard

## Joshua Humphreys Notebook



The Poling of the Masts
The head of the foremast must pole $3 / 5$ of the head of the mainmast upwards. The head of the mizzen mast must pole to the upper or side of the main tressletrees in all ships to the 50 guns; the 40 guns to be 18 inches shorter, the 30 guns 20 inches \& the 20 guns 30 inches shorter. Bowsprit to be $3 / 7$ of the mainmast afore the stern.
$\left.\begin{array}{lll}\text { Head of } & \text { Mainmast } & 43 / 4 \\ & \text { Foremast } & 5 \\ \text { Mizenmast } & 3 \frac{3}{4} \\ & 31 / 2\end{array}\right\} \quad$ All topmast \& topgallant masts $\quad$ Inches to a yard

The quarter of all masts \& yards to be set off by semicircles or a rule agreeable thereto
NB The main foremasts to be quartered from the upper partners to the hounds, but the mizenmast to be from the upper partners to the middle of the hounds
To Find the Length of the Yards
Multiply the length of the gundeck by $5 / 9$ to give the length of the main yard in feet.
The fore yard is $7 / 8$ of the main yard

Main \& fore topsail yard $18 / 25$ of their lower yards | Mizen yard $5 / 6$ of the main yard |
| :---: |
| Crossjack yards \& spritsail yards the length of the foretopsail yard |

## Joshua Humphreys Notebook

Proportions for Masts \& yards and Bowsprit at the several places of their setting off

The heads of all standing masts that are cheaked to ${ }^{4 / 7}$ square of their diameter in the partners, at the hounds ${ }^{9 / 13}$ fore \& aft \& $5 / 6$ thwartships of the diameter in the partners and at the heal to be the bigness is at the $2^{\text {nd }}$ quarter.

The heads of the top masts square ${ }^{6 / 18}$ and at the hounds $9 / 13$ of the diameter of the cap. All main \& fore yards $2 / 5$ of their diameter in the slings for the bigness at the yard arm and all other yards on third of the diameter in the slings for the yarn arm except the mizzen yards lower and $8 / 13$ of the diameter in the slings its upper end one third. Topsail yard arm to be so long as to take in the lower reef, the sails to be made no bigger than the length the yard arm will spread when the reef is taken in.

The quarters of all masts, yards \& bow
Sprits in the following manner. Viz A represents a rule or battin on which set off half the diameter at the hounds as $\mathbf{F}$ \& take the half between $\mathbf{B} \& \mathbf{F}$ for the diameter of the masts at the per quarter as $\mathbf{E}$ the medium between the $2 / 3$ and $1 / 2$ of $\mathbf{B E}$ for the $2^{\text {nd }}$ quarter as $\mathbf{D} \&$ the $2 / 3$ of $\mathbf{B D}$ for the first quarter as $\mathbf{D}$.

The same for all bowsprits \& yards only having regard for bowsprits to divide between the diameter \& half the diameter to keep the same bigness at the upper and quarter as if the head was half the diameter in the bed but to diminish from the upper quarter to $2 / 5$ at the end. All standing masts to be quartered from the upper part of the hounds to the upper partners where they are wedged, topmast \& topgallant mast from the upper part of the hounds to the cap bowsprits from the head to the outer gammoning; yards to the end of the slings.


A to $\mathbf{B}$ represents $1 / 2$ the diameter of the mast in the partners
NB This rule answers the same end as the Semicircle.

NOTE: The above graphic is copied directly from Humphreys' notes to ensure correct scale.

Standing masts cheaks the length of the cheeks $3 / 7$ the length of the masts.
The thickness of the cheek at the upper part of the head the $1 / 3$ of $6 / 7$ of the mast, the lower part of the hounds the same
At the lower end of the cheak the $1 / 2$ thickness of the head the stop $1 / 2$ the cheek at the lower part of the head, fore \& aft the $9 / 13$ of the mast.
The upper part of the head the $5 / 8$ of the thwartships way. To end the lower part of the cheeks the fore \& aft way the $11 / 12$ to the middle \& the $2 / 3$ to the end

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NB For the masting such ships as have dimentions agreeable to the Old Establishments, the following alterations are to be observed (Viz).
The mainmast of the $80,60,50,40, \& 30$ gunships shortened 2 foot from this proportion the bowsprit,

Top mast, topgallant masts \& all yards not be altered from this proportion for ships of the like classes but for all ships that differ much in their dimentions from both the old \& this new established their dimentions for their masts \& yards were cast by for this establishment all main \& fore yard made of New England Tress to be cast at ${ }^{8 / 11}$ of an inch diameter to their length in yards.

Navy Office August 1737 Dimentions

| Dimentions <br> Guns |  |
| :--- | :--- |
|  |  |
| 100 | Main Mast |
| 90 | Main D $^{\circ}$ |
| 80 | Main D $^{\circ}$ |
| 70 | Main D $^{\circ}$ |
| 60 | Main D $^{\circ}$ |
| 50 | Main D $^{\circ}$ |
| 40 | Main D $^{\circ}$ |


| Masts |  |
| :--- | :--- |
| Length | Inches |
| Yd-In | Diamiter |
| $38-0$ | $38-0$ |
| $35-20 / 26$ | $35-7 / 8$ |
| $34-18$ | $34-1 / 4$ |
| $30-0$ | $32-0$ |
| $31-17$ | $30-3 / 8$ |
| $29-10$ | $26-3 / 8$ |
| $27-18$ | $24-7 / 8$ |

Yards
Length Inches Yd-In Diamiter 33-35/8 23-0 $31-7{ }^{1 / 6} \quad 14-1 / 4$ 30-2 $\quad 20-3 / 4$ 28-27 20-0 27-14 19-0 25-18 17-5/8 24-34 17-3/8

The Proportions for Capps
All capps (except the capps for the flying gibb booms) to be twice the diameter of their topmasts or topgallant masts for their breadth and twice their breadth for their length. The thickness of the capps for the main \& foremasts ${ }^{9 / 10}$, the mizenmast capps ${ }^{3 / 7}$ and the top mast capps ${ }^{2 / 5}$ of their breadth. The capps for the flying gibb booms to be 5 times the diameter of the boom for their length, twice the diameter for the breadth, and $9 / 20$ of the breadth for the thickness

Main Capps Length for all Rates

| Length | $6-71 / 2$ | $6-3$ | $5-11$ | $5-7$ | $5-31 / 2$ | $4-11$ | $4-7$ | $4-3$ | $3-11$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Breadth | $3-3^{1 / 4}$ | $3-1^{1 / 2}$ | $2-111 / 2$ | $2-91 / 2$ | $2-73 / 4$ | $2-51 / 2$ | $2-1^{1 / 2}$ | $2-1^{1 / 4} 4$ | $1-111^{3 / 4}$ |
| Depth | $1-1^{5 / 8}$ | $1-4^{3 / 8}$ | $1-3^{7 / 8}$ | $1-3$ | $1-2^{1 / 4}$ | $1-1^{1 / 4}$ | $1-0^{3 / 8}$ | $0-11^{3 / 8}$ | $0-10^{1 / 4}$ |

Proportions for Topps
The main \& foretops thwartships to be ${ }^{1 / 3}$ of the length of the topmasts, the mizzen topps to be ${ }^{7 / 30}$ of the length of the mizentopmast, the spritsail topps to be ${ }^{7 / 8}$ of the length of the spritsail topmast. All the tops to be $3 / 4$ fore \& aft of what they are thwartships.

Proportions for Trestletrees
The tressletrees where there are topps to reach the overhanging of the top rings the depts. at the main \& fore trestletrees to be ${ }^{25 /} / 26$ of an inch to a foot of their length \& their breadth to be $5 / 7$ of their depth, the depth of the mizzen trestletrees to be $6 / 7$ of an inch to a foot of their length \& their breadth to be ${ }^{11 / 16}$ of their depth. The main \& foretopmast trestletrees to be $1 / 3$ as long as their top gallant masts \& the depth to be ${ }^{25 / 26}$ of an inch to a foot in their length and the breadth to be ${ }^{18 / 25}$ of their depth, the mizentopmast trestletrees to half the length of the main topmast trestletrees \& their depth to be an inch to a foot in their length and their breadth ${ }^{11 /}{ }_{13}$ of their depth, the depth of the spritsail \& trestletree to be ${ }^{26 / 29}$ of an inch to a foot of their length \& their breadth ${ }^{17 /} / 19$ of their depth.

The Proportions for Crosstrees
The crosstrees (where there are topps to reach the overhangings of the toprims) the length of the main \& fore topmasts crosstrees to be $4 / 15$ of their top gallant masts, the mizzen topmasts crosstrees to be the same length as their tressletrees, the breadth of their crosstrees to be the same as their trestletrees; \& half the depth of their trestletrees for their depth.

Iron work for masts, yards \& Capps
Bolts for the heads \& cheaks for the main \& foremasts
Size
Streight for clamps for the main \& fores
Capps No in each \& size thick
Eye bolts in the main \& for capps $\quad \mathrm{N}^{\circ}$ in each Size

Streights for the mizzen \& spritsail caps
No in each \& size
Eye in $\mathrm{D}^{\circ}$ number in each \& size
Streight for the main \& foretop mast
No \& size in each

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft -In |
| 26 | 26 | 22 | 20 | 19 | 18 | 17 | 15 | 14 |
| 0-11/4 | 0-11/4 | 0-1/1/8 | 0-11/8 | 0-1 | 0-7/8 | 0-7/8 | 0-7/8 | 0-3/4 |
| 8 | 8 | 8 | 8 | 8 | 6 | 6 | 6 | 6 |
| 0-11/4 | 0-11/4 | 0-1/1/8 | 0-11/8 | 0-1 | 0-7/8 | 0-7/8 | 0-7/8 | 0-3/4 |
| 4 | 4 | 4 | 4 | 4 | 2 | 2 | 2 | 2 |
| 0-13/4 | $0-13 / 4$ | 0-1/8 | 0-1/5 | 0-1 | 0-7/8 | 0-7/8 | 0-7/8 | 0-7/8 |
| 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 0-1 | 0-1 | 0-1 | 0-1 | 0-1 | 0-7/8 | 0-7/8 | 0-7/8 | 0-7/8 |
| 2-11/4 | 2-11/4 | 2-11/4 | $2-1 /{ }^{1 / 8}$ | $2-1 / 8$ | $2-1 /{ }^{1 / 8}$ | 2-1 | 2-1 | 2-1 |
| 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 0-7/8 | 0-7/8 | 0-7/8 | 0-3/4 | 0-3/4 | 0-3/4 | 0-3/4 | 0-3/4 | 0-5/8 |

## Joshua Humphreys Notebook



## Joshua Humphreys Notebook

The Proportions for Merchant Ships, Masts \& Yards
To find the length of the mainmast - Rule:

Take the length of the gundeck or lower deck, the main breadth \& the depth in hold \& add them together. Half of that product is the length of the main mast, only subtracting the main step out of it, which is $1 / 6$ of the depth of the hold.

To find the diameter of the masts for ships of the largest size for ships of the middle size
of the smallest size
To find the quartering of the masts - Rule:
The first quarter
The second $\mathrm{D}^{\circ}$
The third
The fourth quarter
Length of the foremasts
Mizzen mast

Bowsprit

Foretop mast
Main topmast
Mizzen topmast
Topgallant masts
Spritsail topmast

## Joshua Humphreys Notebook

The Proportions for Merchant Ships, Masts \& Yards

| Main yard | $7 / 8$ of the main masts |
| :--- | :--- |
| Fore D | $7 / 8$ of the main yard |
| Mizzen D ${ }^{\circ}$ | $7 / 8$ of the main yard |
| Diameter | $1 / 2$ an inch for a yard in length. |
|  |  |
| Main topsail yard | $5 / 9$ of main yard |
| Fore topsail yard | $5 / 9$ of fore yard |
| Mizen topsail | $1 / 3$ mizzen yard, allowing $3 / 4$ inch to a yard for the bigness. |
| Crossjack yard | something longer than the main topsail yard, allowing $1 / 2$ inch to a yard in length |
|  |  |
| Spritsail yard | $5 / 7$ of the fore yard |
| Spritsail topsail yard | half of the spritsail |

All standing masts to be quartered from the upper part of the hounds to the partners, Topmasts \& topgallant masts from the upper parts of the hounds to the capp Bowsprit from the head of the gammoning yards to the end of the slings

Proportions for masts yards bowsprit at their several places of setting off.
The heads of all standing masts that are cheaked to be $4 / 7$ square of the diameter in the partners; at the hounds $2 / 13$ fore \& aft and $5 / 6$ thwartship of the diameter in the partners and at the heel to be as big as the mast is in the $2^{\text {nd }}$ quarter.
Boats Masts

For boats masts that goes with a boom length 3 times the breadth of the boat or something more.
Diameter $5 / 7$ of an inch to a yard bigness at the partners \& half as big at the upper end, boom $3 / 4$ of the mast. Bow sprit half the mast.
For shoulder of mutton sail 4 times the breadth of the boat. Length of the boom $3 / 5$ of the mast.


NOTE: The above graphic is a scan of Humphrey's Page 130. Transcription of this page would add nothing to the manuscript.

Dimensions for Drawing of Ships And Boats
First for Boats - Draw a straight line at the bottom of the paper representing the middle line, then raise a square at one end of the paper \& sett of your length of your boat. Then sett off the half breadth of your boat moulded, and then sett of your depth of your keel up \& down (that is $1 / 2$ inch to a foot in breadth) then set of the rake off your stem according to proportion that is half the breadth level to the frame. Then middle the boat for $\square$ \& square it up, then your depth in midships is $1 / 2$ of the breadth. The sheer abaft is 2 inches or more to every foot in breadth. Rake the post $1 / 4$ of the height of the line and set off the bigness of the post below them from the line sett down the breadth of the upper strake. At both ends of your boat shear forward one inch to a foot in breadth, rising of the floor from 2 to 4 inches at $\square$ rising at the tuck aft lies $1 / 2$ of the straight up, afore answerable to it. The rising of your breadth at $\square$ the lower edge of your upper strake and abaft in the middle of $\mathrm{D}^{\circ} \&$ forward almost the lower part of $D^{\circ}$ then sett of your $1 / 2$ breadth of transom $1 / 3$ of the $1 / 2$ breadth and draw your narrowing to $\square$ \& keep it as full as you can, then draw your bow to the after part of the stem the sett of your room \& space as you please then take the half breadth of your boat a $\square$ \& your height of breadth from the upper edge of the keel at $\square \&$ please yourself with a midships timber or divide the $1 / 2$ breadth \& height into 10 equal parts and cross them where the lines intersect \& them is your sett you go by for your midships timber then sett off your dead rising \& draw it across \& that will give you the half breadth of floor.

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## To Crop the Molds for a Boat

By whole molding, first make a mould to your midships bend and to your rising line then sett of all your rising and narrowing of main breadth and place the mold well with the narrowing of breadth and straight with the rising of the floor at each timber severally and draw them by the mould then please yourself with the hollow to your after timber so as to lower the tuck make a mould to it and mark the upper edge of the keel then mark the ending of the hollow and divide it into as many parts as you have timbers to hollow marking them with their proper names, then lay a straight battin with the bottom of the heel and the bagg of the midship timber and where it breaks off on the midship timber is the floor surmark them strike a line through the body of timbers of the surmark to the tuck \& lay that line down for a ribbon line to prove the body.

Square Tucks (for ships or boats) for the tuck you must set of breadth height abaft the half breadth of transom, and divide the whole breadth of transom into 3 equal parts and let one of them be the sweep for the tuck then hollow it \& sett of the height of the side \& round of your term to your mind. Height of tucks of ships or boats $1 / 8$ the breadth of the boat from the top of the keel proportions for a long boat - Let the length of the boat be what it will the breadth must as 10 is to 34 for boats from 37 to 34 feet long but for those boats you must allow $1 / 4$ an inch to a foot in length, rake of the stem $7 / 20$ of the breadth depth in midships $5 / 13$ of the breadth shear from the depth in midships $1 / 7$ an inch to a foot in length rake of the post $21 / 4$ of the height, of breadth of $\square^{10} / 38$ of the breadth, breadth of transom $2 / 3$ of breadth, floor sweep ${ }^{4 / 11}$ of the breadth rising of the floor $21 / 2$ inches, abaft the height of the tuck (which is $1 / 8$ of the breadth) \& a little higher afore height of breadth afore at the stem the upper part of the upper frame \& at $\square \&$ aft lower edge of the lower lance on the middle between the whales the narrowing of the breadth and with the $1 / 2$ breadth of transom the keel up \& down $5 / 8$ of an inch to every foot in length \& thwartships one inch less breadth of the post below twice the breadth of the keep \& the heads ${ }^{1 / 3}$ of what is below.

Proportions for Pinaces

Lett the length be what it will the breadth must be as 6 is to 28 from a boat of 28 feet of or upwards but for upward 28 you must allow one inch more than the proportion (rake the stem $5 / 7$ the breadth $D^{\circ}$ the post $1 / 4$ of the length). Breadth of the post $2 / 3$ of the rake below, the keel $3 / 4$ of an inch deep to a foot in length, and the upper and $1 / 4$ of the lower depth in the midships ${ }^{5 / 12}$ of the breadth \& sheer abaft 2 inches to every foot in breadth \& afore one inch less; rising of the floor abaft is $3 / 10$ of the breadth, $\mathrm{D}^{\circ}$ afore $2 / 6$ of the breadth, breadth of the transom ${ }^{4 / 11}$ of the breadth Space of timbers $2 / 10$ floor sweep ${ }^{2 / 6}$ breadth sweep $1 / 3$ breadth of the floor ${ }^{11 / 13}$ of the breadth.
Instructions for Drawing of Ships
Let the breadth be what it will, the length of the keel is 3 times the breadth \& the ${ }^{3 / 5}$ of the breadth added to it for the rake from the forepart of the stem to the rabbit of the post abaft at the upper edge of the keel is $1 / 2$ an inch to a foot in breadth. Rake of the stem $1 / 4$ or $2 / 5$ or $3 / 5$ of the breadth. Length of the sweep for a stem with one sweep is $3 / 5$ of the breadth but for a stem with 2 sweeps the lower sweep $4 / 9$ of the breadth, the upper sweep $1 / 3$ of the breadth.

Rake of the post $31 / 2$ to a foot post abaft the rabbit below is commonly as much as the keel \& falls keel is deep abaft $1 / 4$ of what is below.
First sett of your depth in hold but observe to allow for your floor timber \& cealing and allow downwards what your beams rounds because it is the line of the side, then lay your beam mould well with your deck line that is your depth in hold in midships and let it lay the depth of your keel \& false keel lower afore than abaft. Then sett of your transom from the deck, or work $3 / 5$ of the breadth for the height of your wing transom, if you have wales, place the middle of the middle wale with the deck then sett of your upper \& lower wales from that, but if you have but 2 wales, place the upper edge of the lower wales well with the deck and for height in midships for Man of War as your supports on the lower deck comes just above the wales but for other ships place it a little above the deck then sett off the middle \&

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lower wales from the upper and for the upper edge of the lower wales abaft place it as you think fit below the wing transom chain bolts \& channel wales for Men of War you place the lower edge of your chain bold wales so as to make the steps of the lower deck ports in the midships \& you may carry a parallel shear or you may lift it a little as you see it convenient, but for merchant ships you must be guided by your deck. Your wooden scuppers the wales in midships then sett of your channel wales in midships, then sett of your channel wales from your chain bolts wales shear raile for men of war you have a shear rail in the middle of your upper deck ports in the midships \& carry a parallel shear fore \& aft from the channel whales.

Sheer Streak

You must first sett of the height of your wast from the upper deck, then your shear strake is commonly so broad as to make the shape of your upper deck ports in the midships, \& you must carry is parallel to the channel whales fore \& aft \& the lower edge of it is the using of the double depth because your nuccle lies well with the lower edge of it.

Riseing of the floor Line. Height of the rising of the floor abaft is ${ }^{18 / 32}$ of the breadth \& at $\otimes$ from 4 to 10 inches rising height of the rising afore ${ }^{4 / 13}$ of the breadth.
Narrowing of the Floor Line Breadth of the floor $1 / 2$ or $2 / 5$ of the breadth \& if you work by the narrowing of the floor line you may take from the $1 / 4$ breadth you did by the $1 / 2$ breadth of the floor in midships \& carry it parallel with the half breadth fore \& aft, or you may thin it abaft if you please.

Lower Height of breadth when two for merchant ships place it well with the lower wale in the midships, but for Man of War at the upper edge of the upper whale and abaft it you have 3 whales at the upper edge of the lower whales, but if you have but two whales at the lower edge of the lower whale and afore take for your dead rising to your height of breadth line the midships \& carry it parallel with the rising of the floor line \& then you will have no reconcileing molds for it. Weight of Breadth line when you place your height of breadth in the midships pretty near the middle of your whales or a little higher \& abaft about a foot or more above the wing transom or at the after frame to be a little above the upper edge of the upper whale \& at the foremast frame a little above the upper edge of the upper whale. Narrowing of the Breadth Line Breadth abaft for Man of War $2 / 3$ of the breadth in midships or something less, but for merchant ships it must be something more than the proportion \& for your bowline draw is full or lean as you fancy

Upper height of breadth line when two first set of what straight you intent to have your futtock then sett of your using $1 / 2$ narrowing If your foremast \& aftermast timbers then draw a straight line from the midship height to the half breadth of your foremast \& aftermast timber then square them up from the half breadth of each timber to that line then where they cross the first line there is the height of breadth of each timber then draw them across for your use Riseing of the Double Depth Your riseing of the double depth line ties with the lower edge of the waste rail or shear streak because of the nuccle. Narrowing of the Double Depth Tumbling home of $\otimes$ is commonly ${ }^{1 / 14}$ of the breadth or something more \& abaft within the half breadth abaft half of what it is in midships \& afore $2 / 3$ of what it is in midships .

To Place $\otimes \mathbf{N}, \mathbf{B}$ middle gundeck \& place it afore $7 \mathrm{ft} 4 \mathrm{in}, 7 \mathrm{ft} .2 \mathrm{in}, .7 \mathrm{ft} .1 \mathrm{in}, .6 \mathrm{ft} 10 \mathrm{in}, 6 \mathrm{ft} .9 \mathrm{in}, 6 \mathrm{ft} .7 \mathrm{in}, 6 \mathrm{ft} . .5 \mathrm{in}, 6 \mathrm{ft} .3 \mathrm{in}, 6 \mathrm{ft} .3 \mathrm{in}$, or you may place it $4 / 9$ of gundeck from afore the rabbit.

To Lay Down the Midship Bend

Breadth of the floor $1 / 3$ or $2 / 5$ or $1 / 2$ of the breadth dead riseing from 4 to 10 inches (as before mentioned) floor sweep ${ }^{5 / 22}$ of the breadth (or something more \& less as you please) and for your under breadth sweep open your compasses on the height of breadth line till it reconciles with your floor sweep, under breadth the sweep (if you have 3 sweeps is $1 / 3$ of the breadth reconcileing sweep is $3 / 5$ of the breadth sweep above the breadth $1 / 3$ of the breath back sweep above the breadth for the hollow of the toptimber $1 / 3$ or a $1 / 4$ of the breadth but for full ships draw it fair with an elliptical mold from the bagg of your floor sweep up to your half breadth and you'll want no lower breadth sweep only aft.

To Shorten your Under Breadth Sweep when you have your under breadth sweep that reconciles with $\otimes$. Sett with your half breadth where you begin to narrow your breadth, then for your sweep abaft divide the half breadth of transom into 3 parts and sett one of the off from the middle line \& draw a diminishing line, butt observe if you would mould that if you have more sweep at the after frame than you have distance between the rising of the floor \& the rising of the breadth, take something less distance \& draw from that. To work out your hollow abaft you must first please yourself with a hollow so your after-most timber as near the foot of the fashion pieces as you can, then you must work by a riseing of a straight line or work it out by a progression of lines. That is, lay the straight of your hollow mould by a perpendicular then work of your after timber. Set the lower end then strike a parallel line and divide both lines into as many equal parts as there is timbers as far as your hollow \& where they cut the mould that is the lipping of each timber then keep the mould at the breadth of the keel \& the upper edge and to the bagg of its proper timber. Rake of the fashion piece on the flatt at the upper edge of the keel $1 / 14$ of the breadth \& for abaft at the wing transom see how much you will round your wing transom forward \& how big you will have it fore \& aft at the end \& add them together and that is the distance abaft on the floor.

To Lay Down the Buttuck of a Ship
First sett of the height of your transom then sett of the [indecipherable\} rabbit of the post \& the rake. Then sett of the rake of the fashion piece in the flat but if you intend to cant your fashion piece you must take out as much as you intend to cant the fashion $p^{s}$ out of the end of the transom height of lower transom $3 / 5$ of height of wing. Then you must sett of your transom on the post \& draw them parallel to the upper edge of the keel till the cut of the fashion $\mathrm{p}^{s}$. Square down all the transoms to the middle line for the brick of your transom then square down all the transoms where they butt the height line butt on the cant you have no need to square down only the wing transoms \& the lower end \& the wing transoms 3,4 or 5 less flight if you cant your fashion piece but the lower transom the same then draw your post as you intend to taper it then take of your boddy the breadth of each timber of the height of each transom singly and sett them of upon the room \& space of each timber as you sett for your buttuck upon their one prop timbers and so force them by fair lines till they come to your spots at the end of your rabbit \& where the square lines that come from the rake of your fashion piece cut the fore \& aft lines that is cut through the body of your timbers that is the half breadth of your transom or the fore part of the transom for your fashion piece to lye on when your fashion piece is on the flat but on the cant you must not allow your wing transom flight not so much as on the flat by 3 or 4 or 5 inches or more or less. The flight below at the lower transom may be the same as one the flat to strike the cant line is thus you must take the half breadth of the wing transom from the boddy \& sett off below \& where the square line of the flight of wing transom cuts it is the spot \& where the flight of the lower transom squared down will cut the waterline of the lower transom is the after spott then strike a line from spott to spott \& that is the cant line and where the cant line cuts the rest of the rakes line between the wing \& lower transom is the half breadth of the rest of the transoms with spott must be squar'd up with an essing flight line the rest as on the flat.

To Make the Fashion Piece Mould
You must take the height of all your transoms according to the rake of the fashion piece \& sett them of on a square on the body of timbers downwards from the height of breadth \& strike the lines across the body, then take the half breadth of your transoms \& sett them on the proper height of the transoms sett down then take the shortning of your under breadth sweep at the transom \& set it of from the half breadth on the height of breadth line in the body towards the middle line \& swap it downward then take your hollow mold or elliptical mold \& see if your setts of the half breadth of your transom comes fare with your [under breadth edge] \& the transoms \& if nott draw a fair line with your hollow mould \& take the half breadth of your fashion piece at that transom that does not come fare \& carry to your water line or for or aft line that you forst for your transoms \& so make them some fare.

To take the beveling of transoms \& fashion piece
Lay a bevel with the line that goes athwartships \& cut of the end of the transoms below at the half breadth that is the flight or cants line) and open your bevel to the thickness of your fashion piece on the fore \& aft line that is forst fair \& that will give you the beveling of the fashion piece at every transom. To bevel the end of the transoms for the fashion piece to lay on lay a bevel well with the fore \& aft of the transom \& open it to the rake of the of the fashion piece and that will give it; to level the transoms lay a bevel well with the fore \& aft line of the transom \& [shade] it to the rabbit of the post.


Scan of graphic from Humphreys' Page 145

To take the beveling of the timbers from the body of after your ribband lines on your body are prov'd fair lay a battin well with your ribband line across your body \& take the lipping of every timber of on your battin butt observe that you must strike two parallel lines one from the other [ $\mathcal{E}$ divide] as the exact [room $\mathcal{E}$ space] is then make a square at one end $\&$ sett of your lipping of timbers on each side then line from the square then strike a straight line from the square of the first lipping on the other side to follow each spott one after another and that will give you the true beveling of each timber then take them from that \& sett them upon a board. But let your board be parallel that you may take them off for the timbers that are standing as well as under.

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## To Lay Down the Midship Bend

Breadth of the floor $2 / 5$ for great ships above fourth rates $\& 1 / 3$ for $4^{\text {th }}, 5 \&$ sixth rates of the main breadth moulded length of the floor sweep $1 / 4$ of the main breadth but may after [this proportion]. In great ships to make the boddy fuller; reconciling sweep between the floor \& underbreadth sweep $5 / 9$ of the main breadth underbreadth sweep in midships $1 / 3$ of the main breadth \& underbreadth sweep $1 / 2$ of the midships \& afore $2 / 3$ of the midships \& then you may shorten them from the midships aft $\&$ forward by a diminishing line sweep above the breadth is $2 / 5$ for $1^{\text {st }} 2^{\text {nd }} \& 3^{\text {rd }}$ rates and $1 / 4$ of the main breadth for $4^{\text {th }} 5^{\text {th }} \& 6$ rates. Back sweep of the toptimber $5 / 9$ for first second \& third rates $\& 2 / 5$ for $45 \& 6$ rates of the main breadth moulded.

Length of sweeps for the hollow abaft for $1^{\text {st }}$ rates 18 feet, for $2^{\text {nd }} 17$ feet, for $3^{\text {rd }} 16$ feet, for $4^{\text {th }} 15$ feet, for $5^{\text {th }} 12.6$ feet, for $6^{\text {th }} 10.63$ feet. But if your ship is to be a full ship for burthen you must make your sweep the shorter and work of your hollow out to a straight sooner but afore you will have no occasion of [indecipherable text] any rule for which it is so customary to make so much or so little hollow that there is very seldom any used only to make the waterline fare.

To work out your hollow abaft
You please yourself with a hollow to your after timber as near the foot of your fashion piece as you can then mark the mould at the upper edge of the keel with the proper name of the timber then mark the ending of the hollow with that name as you designated your hollow. Then draw a straight line and parse a perpendicular in the middle of the line \& turn the mould on the edge up the perpendicular \& mark the other spott on the perpendicular then with them distances sweep a simmecircle to the straight line \& divide each quadrant into as many equal parts as you have timbers to come in between them \& draw a line to each spott turn the mould upon the edge and mark them on the [indecipherable text] that gives it to lip one more than another keep the spots down to the keel.

NB To find the bevlings of transoms you must draw as many lines as you see convenient, parrel to the middle line through your boddy laid down then take the height of each timber up that perpendicular and carry it to the respective timbers on your room \& space in your shear draught you can also draw those parrillels through your boddy of transoms laid down and take the round forward of each transom \& sett of on each height of transom down from your post. Then with your elliptical mold force all these spots fair (it gives you the true sections of your vessel at those places) then lay your bevel on your line drawn for the upper side of your transom and open your bevel to your curve line forst it gives you the bevelings at these places.

To work out your hollow abaft of your top timber
When you have got your hollow at flat reconcile one end of it to what hollow you designe your after frame shall have then mark the double depth line $4 \otimes$ and the breaking of the hollow at the upper breadth sweep \& extend that distance upwards above the double depth at $\otimes$ and that is the after frame then mark it with its proper name. Then divide that timber to $\otimes$ into as many equal parts as you have timbers to come in between keeping every part down to double depth at $\otimes \&$ to the narrowing \& breaking of the proper timber you are laying down.

To work out your knuckle afore
You must first make your mould to the same hollow as you did for $\otimes$ abaft then reconcile your mould at the other end with the shape you designe your foremast nuckle timber to be then draw your foremast nuckle \& mark the double depth of its one timber on the mould and mark it with a $\otimes$ upon your mould where you begin to degenerate from your upper deck sweep then divide them two distances into as many equal as you have timbers in the wake of your foremast drift and keep every part well with the riseing of the double depth and the breaking off the back of the upper breadth sweep and its one timber.

## For Pink Stern Vessels

In working out lute stern you must work you proportions as you do for ships only draw a narrowing of breadth line home to the post abaft \& the riseing of breadth flies up to the lute but if it be a flagg boat it lies with the upper deck \& for the working out your after timber you must make a joint mould where your tumbling home begins to decline \& to work it out by your half breadth aft all the rest as ships, the stern post rakes [ 4 inches] or $41 / 2$ in a foot.

To find the floor sirmark in all ships first sett off your depth of keel \& falls keel in midships \& the half breadth of keel then lay a battin well with the bottom of the keel and where it touches the bagg of the mould that is the floor surmark.

To find the floor ribbin afore \& abaft the height of the floor at the stern \& at the post and sett them off on the middle line \& so draw a straight line to floor sirmark then divide the after and foremast timbers up to the height of board surmark as you did at $\otimes$ and draw a straight line to the middle line.

Shear Mould by a $1 / 4$ Seate
The length of your sweep for first and second rates 14 feet or $13-6$ feet for third rates $13-6$ feet or 13 feet for 4 rates 12 feet or 11-6 feet for 5th rates 10 or $9-6$ feet for 6 rates 9-6 feet or 9 feet .

## To Make a Ships Rother

Take the $1 / 8$ of the extreme breadth of the ship for the breadth below (that is $11 / 2$ inches to a foot) for the lower hance $2 / 3$ of the lower end which height lies half the ships breadth from the bottom of the keel, \& for the bigness of the head fore \& aft take from 16 to 20 of from your of numbers \& carry to the bigness of the post athwartships \& extend it forward \& that will give you your bigness at the head fore and aft, to beard your rother take $3 / 5$ of the thickness lot from the middle line or $1 / 3$ sett from the upper edge of your tiller hold thwartships $1 / 3$ of the rother $\&$ up \& down 1 inch more the after part of the hole $2 / 3$ of the forepart. The tiller at the foremast line $1 / 2$ of what it is at the after end.

To measure a ships sheathing
Take the length of your ship from stem to post $1 / 2$ the height between the keel \& whale, then take the girt of the body in every 10 foot as there is to length and add them together \& divide by the number of so many 10 feet as there is in the length \& that the girt of the body then measure as you do com-on measure but you must allow the thickness of the sheathing in your girt \& measure the keel \& whales stem \& post by themselves.

Principal Dimentions of $y^{e}$ Garland of 24 Guns

|  | Ft | In |
| :---: | :---: | :---: |
| Depth on the gundeck | 112 | 0 |
| $\mathrm{D}^{\circ}$ of the keel for tonnage | 92 | 9 |
| Breadth extream | 32 | 0 |
| Depth in hold | 11 | 0 |
| Height of wing transom | 18 | 2 |
| Breadth of the shear rail abaft | 14 | 3 |
| Height of the lower whale Afore | 18 | 0 |
| Abaft | 22 | 6 |
| Breadth of the wing transom | -- | -- |
| Height of the stem | 22 | 6 |
| Cutting down Afore | 2 | $71 / 2$ |
| Abaft | 3 | $11 / 2$ |
| Midships | 4 | 7 |
| Riseing of the midships flat | 0 | 11 |
| Height of top timberline or Afore | 16 | 2 |
| upper edge of waste rale Abaft | 29 | 6 |
| Upper edge of the keel midships | 23 | 0 |
| Hanging of ye gundeck at the middle line | 1 | 4 |
| Higher abaft than afore from the keel | 0 | 5 |
| Gallery stools wide | 3 | 0 |
| Height of topraile from quarter deck | 4 | 9 |
| Dimentions of $\mathrm{y}^{\text {e }}$ Garlands Masts \& Yards |  |  |

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| Main | $\left\{\begin{array}{l}\text { Mast } \\ \text { Topmast } \\ \text { Top gallant mst }\end{array}\right.$ |
| :---: | :---: |
| Fore | $\left\{\begin{array}{l}\text { Mast } \\ \text { Topmast } \\ \text { Top gallant mast }\end{array}\right.$ |
| Mizen | $\left\{\begin{array}{l}\text { Mast } \\ \text { Topmast } \\ \text { Top gallant mast }\end{array}\right.$ |
|  | Bowsprit <br> Spritsail topmast <br> Crossjack yard <br> Flying Gibb boom |
| Flagstaff | $\left\{\begin{array}{l}\text { Main } \\ \text { Fore } \\ \text { Mizen }\end{array}\right\} \quad$ Topmast |
| [Studonsails boom] | $\left.\begin{array}{l}\text { Main } \\ \text { Topmast } \\ \text { Top gal mast } \\ \text { Fore } \\ \text { Topmast } \\ \text { Top gallant mast }\end{array}\right\}$ <br> Driver |


| Masts |  | Yards |  |
| :---: | :---: | :---: | :---: |
| Length | Diameter | Length | Diameter |
| Yd In | In | Yd In | In |
| 250 | 23 | 220 | $15^{1 / 2}$ |
| 1518 | $131 / 2$ | 160 | $91 / 2$ |
| 80 | $71 / 4$ | 110 | $6^{1 / 4}$ |
| $22 \quad 24$ | 201/2 | 200 | 14 |
| 139 | $13^{1 / 8}$ | 146 | 9 |
| 718 | 7 | 100 | 6 |
| 216 | $14^{1 / 2}$ | $18 \quad 22$ | 101/2 |
| 108 | $8^{5 / 8}$ | 1017 | $61 / 2$ |
| 1417 | $51 / 2$ | 812 | $4^{3 / 4}$ |
| 1430 | 23 | $14 \quad 6$ | 9 |
| - - - | - - | 923 | $53 / 4$ |
| - - - | - - | 146 | 9 |
| $10 \quad 24$ | $91 / 2$ | - - | - - |
| 80 | $53 / 4$ | - - - | - - |
| 70 | $5^{3 / 8}$ | - - - | - - |
| 618 | $4^{3 / 4}$ | -- - - | - - |
| -- - | -- | $9 \quad 511 / 2$ | $5^{1 / 4}$ |
| $10 \quad 331 / 2$ | $6^{1 / 8}$ | 718 | $4^{1 / 2}$ |
| -- | - - | 51 | 3 |
| - - - | -- | 81 | $4^{7 / 8}$ |
| 923 | $53 / 4$ | 76 | $4^{3 / 8}$ |
| - - - | -- | 50 | 3 |
| 140 | $83 / 4$ | $9 \quad 51 / 4$ | [indecipherable] |

## Joshua Humphreys Notebook

Principal Dimentions of the Establishment in the year 1745

Length of the keel for tonnage
$\mathrm{D}^{\circ}$ on the gundeck from the rabbit of the post to the rabbit of the stern
Breadth $\left\{\begin{array}{l}\begin{array}{l}\text { extream } \\ \text { at the aftermost part of the wing transom } \\ \text { At the top timberline front outside to outside plank }\end{array}\left\{\begin{array}{l}\text { afore } \\ \text { Midships } \\ \text { Abaft }\end{array}\right.\end{array}\right.$
Weight $\left\{\begin{array}{l}\text { of the cutting down in the midships above the keel } \\ \text { Of top timberline or upper edge of the } \\ \text { Waist raile above the keel }\end{array}\left\{\begin{array}{l}\text { Afore } \\ \otimes \\ \text { Abaft }\end{array}\right.\right.$

Riseing of $\otimes$
Height $\left\{\begin{array}{r}\text { Gundeck from the plank to the upper edge } \\ \text { of the middle or upper } \\ \text { deck beam } \\ \text { From the plank to the port cells }\end{array}\right.$

Ports

Deep
Fore \& aft
$\left\{\begin{array}{l}\text { Afore } \\ \otimes \\ \text { Abaft }\end{array}\right\}$

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $144-6 \frac{1}{2} 2$ | $168-4$ | $134-101 / 4$ | $131-4$ | $123-0 \frac{1}{4} 4$ | $117-8^{1 / 2} 2$ | $108-10$ | $93-4$ |
|  |  |  |  |  |  |  |  |
| $178-0$ | $170-3$ | $169-0$ | $160-0$ | $150-0$ | $144-0$ | $133-0$ | $114-0$ |
|  |  |  |  |  |  |  |  |
| $51-0$ | $48-6$ | $47-0$ | $45-0$ | $42-8$ | $41-0$ | $37-6$ | $32-0$ |
| $33-0$ | $31-0$ | $30-5$ | $27-\mathrm{t}$ | $26-0$ | $25-0$ | $22-9$ | $18-4$ |
| $33-0$ | $31-0$ | $30-5$ | $27-6$ | $26-0$ | $25-0$ | $22-11$ | $19-0$ |
| $36-6$ | $34-9$ | $33-6$ | $32-6$ | $32-0$ | $30-9$ | $28-1$ | $26-0$ |
| $23-6$ | $22-4$ | $21-8$ | $21-0$ | $20-0$ | $19-2$ | $17-6$ | $14-9$ |


| $1-8$ | $1-7^{1 / 2}$ | $1-61 / 2$ | $1-6$ | $1-51 / 4$ | $1-5$ | $1-5$ | $1-4 \frac{1}{2}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $47-0$ | $45-4^{3 / 4}$ | $44-6$ | $36-7$ | $34-1$ | $33-5$ | $30-9$ | $25-4$ |
| $43-7$ | $42-4$ | $40-11$ | $34-0$ | $32-4$ | $31-0$ | $28-11$ | $23-1$ |
| $59-8$ | $52-1 / 4$ | $50-2$ | $42-8$ | $40-3$ | $37-9$ | $34-4$ | $28-3$ |
|  |  |  |  |  |  |  |  |
| $0-4$ | $0-4$ | $0-4$ | $0-5^{1 / 2}$ | $0-6$ | $0-6^{1 / 2}$ | $0-8$ | $0-9$ |


| $7-2$ | $7-0$ | $7-0$ | $7-0$ | $6-10 \frac{1}{2}$ | $6-9$ | $6-8$ | $6-1$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $2-4$ | $2-4$ | $2-4$ | $2-4$ | $2-3$ | $2-3$ | $2-1$ | $1-10$ |
|  |  |  |  |  |  |  |  |
| $2-9$ | $2-8$ | $2-8$ | $2-8$ | $2-8$ | $2-7$ | $2-6$ | $2-2$ |
| $3-7 \frac{1}{2}$ | $3-5$ | $3-5$ | $3-5$ | $3-4$ | $3-3$ | $2-11$ | $2-6$ |

Principal Dimentions of the Establishment in the year 1745
Hanging of the deck at the middle line
\(\left.$$
\begin{array}{l}\begin{array}{l}\text { Height from } \\
\text { the upper } \\
\text { deck plank }\end{array}\end{array}
$$\left\{$$
\begin{array}{l}\begin{array}{l}\text { Beams to round } \\
\text { From the upper deck to the upper edge } \\
\text { Of the quarter deck beams } \\
\text { At the waste } \\
\text { To the port cells } \\
\text { To the upper edge of the forecastle beams } \\
\text { Ports }\end{array}\end{array}
$$ \begin{array}{l}Afore <br>
Afore <br>

Abaft\end{array}\right\} $$
\begin{array}{l}\text { Abaft }\end{array}
$$\right\}\)| Deep |
| :--- |
| Fore \& Aft |

Forecastle beams to round length of $D^{\circ}$ from the foreside beakhead stantions
Quarterdeck as long as the main jeers will allow
Length from the foreside of the toprail at the height of the fiferail to the Foreside of the figure of the head bylines parrel to the keel

| 100 | 90 | 80 | 70 | 60 | 50 | 40 | 30 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In | Ft-In |
| $2-1 \frac{1}{2}$ | $2-0$ | $1-11$ | $1-10$ | $1-9$ | $1-8$ | $1-7$ | $1-6$ |
|  |  |  |  |  |  |  |  |
| $0-81 / 2$ | $0-81 / 4$ | $0-8$ | $0-73 / 4$ | $0-71 / 2$ | $0-71 / 4$ | $0-7$ | $0-63 / 4$ |
| $7-0$ | $6-10$ | $6-8$ | $6-8$ | $6-7$ | $6-7$ | $6-6$ | $6-5$ |
| $7-4$ | $7-1$ | $6-11$ | $6-11$ | $6-9$ | $6-81 / 2$ | $6-71 / 4$ | $6-7$ |
| $5-8$ | $5-7$ | $5-6$ | $5-10$ | $5-3$ | $5-0$ | $4-8$ | $4-7$ |
| $1-10$ | $1-10$ | $1-8$ | $1-11$ | $1-9$ | $1-9$ | $1-8$ | $1-8$ |
| $6-8$ | $6-6$ | $6-0$ | $6-4$ | $6-2$ | $5-10$ | $5-5$ | $5-3$ |
| $2-8$ | $2-8$ | $2-7$ | $2-8$ | $2-7$ | $2-7$ | $2-4$ | $2-4$ |
| $3-0$ | $2-9$ | $2-9$ | $2-10$ | $2-8$ | $2-8$ | $2-5$ | $2-5$ |
|  |  |  |  |  |  |  |  |
| $38-0$ | $36-0$ | $36-0$ | $33-0$ | $28-0$ | $27-0$ | $25-6$ | $18-0$ |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| $212-9$ | $203-0$ | $196-0$ | $186-0$ | $175-0$ | $167-0$ | $154-0$ | $131-0$ |

Principal Dimentions of the Establishment in the year 1745


The back of the fals post to rake $21 / 2$ in a foot and the upright of the stern 3 inches in a foot. The floor \& futtock timbers in the bearing of thickness to full up the room \& space especially in large ships the stem to rake forward above the gundeck 2 inches in a foot.

## Weight of Turpentine

Memorandum, Turpentine Ought to Weigh 321 Ct per Barrel if it is Survey'd and branded at Carolina.

Dimentions of the Randolph Frigate of 23 guns built at Philad ${ }^{\text {a July }} 101776$

|  | Feet |  |
| :--- | ---: | ---: |
| Length of the gundeck from the aft side apron to the foreside rudder | 137 | 3 |
| Keel for tonnage | 112 | 0 |
| Extream breadth | 34 | 6 |
| Depth in Hold | 11 |  |
| Breadth of transom | 21 | 6 |
| Rising of mids $\otimes$ | 1 | 9 |
| Breadth of floor | 14 |  |
| Tumbling home top timber | 3 |  |
| Hanging gundeck | 1 | 7 |
| Height between decks | 5 | 2 |
| Waste amids | 5 | 2 |
| Port cells from deck | 1 | 8 |
| Up \& down in the clear | 2 | 3 |
| Fore \& aft Do $\sim \sim \sim$ | 2 | 6 |
| Distance between the ports | 7 | 5 |
| 13 ports on the gundeck | 6 | 10 |
| Height from upper part gundeck to the upper part of Qutr deck at fore end | 6 |  |
| Height forecastle to the top of the beam at the after end | 6 |  |
| Quarter deck short of the center main mast but should run within 2 feet of it | 7 | 1 |
| Beakheads from the apron | 3 | 9 |
| Foremost port abaft the beakhead | 4 | 1 |
| After port from the side rudder | 9 | 6 |
| Length of forecastle | 27 | - |
| Center foremost abaft the apron | 19 | 3 |
| Do of cable bitts abaft the center for mast but should be at least 2 ft more | 9 | 6 |
| Center main mast abaft center foremast | 59 | 6 |
| Center of mizenmast abaft center main mast | 36 | 6 |
| Center of D $\sim$ D $\sim$ before the rudder | 22 | - |

Dimentions of capstand
\(\left.\begin{array}{cc}Quarterdeck up drumhead <br>
lower \mathrm{D}^{\circ} \sim \& \mathrm{ft} 1 diam^{\mathrm{t}} by 4 high <br>

3 \mathrm{ft} 10 in by 8\end{array}\right\}\)| thickness |
| :--- |
| Filling |$\quad 12 \mathrm{in}$

Length barrel under the drumhead $\quad 3^{\mathrm{ft}} 2^{\text {in }}$ by 1 ft 8 in
Whelps at bottom $10 \frac{1}{2}$ at surge $61 / 2$
at top $91 / 2$
from the bottom to the surge 2 feet 5 in
Lower capstand, upper drumhead 4 to 9 lower sided as above barrell 2 feet diam ${ }^{r}$ height as above
Whelps at bottom 12 at surge $71 / 2$ at the top $101 / 2$
The amo $^{t}$ of ship carpenter \& laborer wages is $£ 2289$ when wages was at 7 shillings per day $\&$ the ship joyners work am't to $£ 380$ \& used 22 thousand feet boards \& scantling.
Dimensions of the Delaware Frigate of 28 Guns
Ft I
Length of Gun deck from the aft side of the apron to fore side rudder ..... 119
Keel Length for tonnage ..... 96
Extream breadth ..... 32
Depth in hold ..... 106
Height between decks ..... 5
Breadth of Transom
Breadth of floor
Rising of $\mathrm{D}^{\circ}$
Tumbling home top timber
Hanging Gundeck
Wake amidships ..... 10
Port Cills from deck ..... 7
$D^{\circ}$ Up \& down ..... $11 / 2$
$\mathrm{D}^{\circ}$ Fore \& aft ..... 24
Distance between the ports ..... $7 \quad 1$ ½
12 ports on the gun deck
Height under the $2^{\text {nd }}$ deck from plank to plank ..... 6
$\mathrm{D}^{\circ}$ under the forecastle from plank to plank ..... 59
Length of $\mathrm{D}^{\circ}$ ..... 21
Beak head abaft the apron36
Fore mast part abaft the beak head ..... 36
After port before the rudder ..... 8
Center foremast abaft the apron ..... 16
$\mathrm{D}^{\circ}$ of cable bitts $\mathrm{D}^{\circ}$ of foremast ..... 11
$\mathrm{D}^{\circ}$ of capstand $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$$2301 / 2$
$\mathrm{D}^{\circ}$ of main mast $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ ..... 53
$\mathrm{D}^{\circ}$ of capstand abaft main mast ..... 15
$\mathrm{D}^{\circ}$ of mizzen mast $\mathrm{D}^{\circ}$ ..... 32
$\mathrm{D}^{\circ}$ of before rudder ..... 19
Brest of the figure before the hawse piece ..... 12
Dimensions of the Languedoc of 90 guns
Length of the keel from the foot of the post to the rear of the stem ..... 165
Length of the ship from stem to stern ..... 184
Rake of the stern post ..... 2
$\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ stem ..... 17
Breadth mid ${ }^{1}$ frame ..... 48 ..... 4
Length of mid ${ }^{1}$ beam ..... 46
Height port keelson lower deck ..... 2Distance between the ports78
Height on the gun deck under the beams ..... 56
Height of the port cells on the second deck ..... 10
Distance between the ports ..... 9
Height of the hold asunder the beams ..... 51
Depth of the hold ..... $23 \quad 2$ ..... 2
Breadth of the ship on the lower deck ..... $46 \quad 8$ ..... 8
$\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ on the outside $\mathrm{D}^{\circ}$ ..... 50
Thickness of the ships side ..... 2922

| Dimentions of her Masts \& Yards | Feet In. | Diameter | Head of L |
| :---: | :---: | :---: | :---: |
| Length of main mast | 116 | $38^{2 / 3}$ | 13 2/3 |
| Foremast | 108 | 36 | $123 / 4$ |
| Mizen $\mathrm{D}^{\text {o }}$ | $80^{1 / 2}$ | 23 | $91 / 2$ |
| Bow spritsail | 71 | $37^{1 / 3}$ | - - |
| Main topmast | 723/4 | $21^{2 / 3}$ | $71 / 4$ |
| Fore $\mathrm{D}^{\mathrm{o}} \sim \mathrm{D}^{\mathrm{o}} \sim$ | $6^{3 / 4}$ | $19^{2 / 3}$ | $6^{2 / 3}$ |
| Mizen $\mathrm{D}^{\mathrm{o}} \sim \mathrm{D}^{\text {o }}$ ~ | $46^{1 / 2}$ | $133 / 4$ | $4^{2 / 3}$ |
| Main TG mast | 49 | $11^{1 / 3}$ | $16^{2 / 3}$ |
| Fore | $43^{1 / 2}$ | $10^{1 / 4}$ | $14^{2 / 3}$ |
| Mizen | $35^{1 / 2}$ | 8 | $12^{1 / 4}$ |
| Gibb boom | $51^{1 / 2}$ | 14 | yd arms |
| Main yard | $106^{2 / 3}$ | $26^{2 / 3}$ | $92 / 3$ |
| Fore Do ~ | 97 | $241 / 4$ | 9 |
| Mizen yard | 95 | $181 / 2$ | 2 |
| Spritsail yard | 69 | $15^{1 / 4}$ | 6 |
| Main topsail yard | 81 | 17 | 1611 |
| Fore T Y | 74 | $151 / 2$ | 15 |
| Crossjack yard | 74 | $143 / 4$ | 6 |
| Mizen F Do ~ | 58 | $92 / 3$ | $91 / 2$ |
| Main TG yard | $531 / 4$ | $92 / 3$ | $91 / 2$ |
| Fore TG $\mathrm{D}^{\circ} \sim$ | $48^{1 / 2}$ | 8 | $4{ }^{1 / 4}$ |
| Mizen F $\mathrm{G}^{\mathrm{l}} \mathrm{D}^{0}$ ~ | $42^{1 / 2}$ | 7 | $33 / 4$ |
| Main T G Royal Yard | $351 / 2$ | 6 | 3 |
| Fore $\mathrm{D}^{\circ}$ | $32^{1 / 2}$ | $5^{1 / 2}$ | 3 |
| Height of Ensigne Staff | $48^{1 / 2}$ |  |  |
| Sails their Dimentions | Extent | Drop | Foot |
| Main Sail | 97 | 48 |  |
| Fore ${ }^{\circ}$ | 88 | 42 |  |
| Main top sail | $64^{2 / 3}$ | 2 | 94 |
| Fore $\mathrm{D}^{\circ}$ | $58^{2 / 3}$ | 57 | 85 |
| Mizen $\mathrm{D}^{\circ}$ | $481 / 2$ | 32 | $62^{2 / 3}$ |
| Sprit Sail | 63 | $311 / 2$ | 63 |
| Main T G Sail | $481 / 2$ | 32 | $62^{2 / 3}$ |
| Fore $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ | $44^{1 / 4}$ | 29 | $56^{2 / 3}$ |
| Main T G R Sail | $381 / 4$ | 23 | 46 |
| Fore $\mathrm{D}^{\circ}$ | $32^{1 / 3}$ | 14 | 46 |
| Mizen ${ }^{\text {o }}$ | $291 / 2$ | $121 / 2$ | 42 |
| Anchors their Weight |  |  |  |
| 1 best bower | 7750 |  |  |
| $1 \mathrm{D}^{\circ}$ | 7650 |  |  |
| 1 small D ${ }^{\text {o }}$ | 7500 |  |  |
| 1 Stream anchor | 2480 |  |  |
| $1 \mathrm{D}^{\circ}$ | 2340 |  |  |
| 2 spare anchors in the hole, | er 7150 |  |  |

Cables

| Seven 23 inch | Weight 15500 each |  |
| :---: | :---: | :---: |
|  |  |  |
| Four 12 D ${ }^{\circ}$ Stream Cables | $5000 \mathrm{D}^{\circ}$ |  |
|  | Inch | 36 pounders on lower Deck |
| Main Shrouds | $10^{1 / 2}$ | $26 \mathrm{D}^{\circ}$ Second deck |
| $\mathrm{D}^{\circ} \mathrm{TGG}{ }^{\circ}$ | $51 / 4$ |  |
| $\mathrm{D}^{\circ} \mathrm{TM} \mathrm{D}^{\circ}$ | 3 | $12 \mathrm{D}^{\circ}$ fore castle \& $2^{\text {nd }}$ Deck |
| Main Shrouds | $10^{1 / 2}$ |  |
| $\mathrm{D}^{\circ} \mathrm{TGG}{ }^{\circ}$ | $15^{1 / 2}$ |  |
| $\mathrm{D}^{\circ} \mathrm{TM} \mathrm{D}^{\circ}$ | $10^{1 / 2}$ |  |
| Main Stay | $15^{1 / 2}$ |  |
| Fore Shrouds | $10^{1 / 2}$ |  |
| $\mathrm{D}^{\circ} \mathrm{TM} \mathrm{D}^{\circ}$ | 5 |  |
| $\mathrm{D}^{\circ} \mathrm{TG}$ | $23 / 4$ |  |
| D ${ }^{\text {S Stay }}$ | 15 |  |

The Languedoc with six months provisions on board \& 2 months wages amounts to 1,100000 French Livres

183333
$81 / 3$
14666664
61111
1527775
76388.75 per M

## Joshua Humphreys Notebook

Dimensions \&c of a Twenty Five Gun Ship Built by Joshua Humphreys for the Honorable Navy Board

| Feet | Inch |  |  | Feet | Head |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 147 |  | Keel | Main Mast | 112 | $16^{1 / 2}$ |
| 149 |  | Beam | Fore Mast | 101 | $14^{1 / 2}$ |
| 19 |  | Hold | Mizen Mast | 94 | 13 |
| $311 / 2$ |  | Feet Transom | Bow Sprit | 80 |  |
| $22^{1 / 2}$ |  | Floor | Main top mast | 76 | 11 |
| 2 |  | Rising | Fore $\mathrm{D}^{\circ}$ | 10 |  |
| 7 |  | Between Deck | Mizen ${ }^{\text {o }}$ | 60 | $81 / 2$ |
| 2 | 6 | Port cills from beams | Main Top Gal mast | 38 | $301 / 2$ |
| 8 | 1 | Distance between the ports | Fore D ${ }^{\text {o }}$ | 35 | 28 |
| 3 |  | Ports in the clear for \& aft | Mizen ${ }^{\text {o }}$ | 30 | 24 |
| 2 | 7 | Up \& down | Main Yard | 108 |  |
| 17 | 10 | After port from rabbet post | Fore D ${ }^{\text {o }}$ | $941 / 2$ |  |
| 15 | 9 | Fore port $\mathrm{D}^{\circ}$ Stem | Mizen $\mathrm{D}^{\circ}$ | 86 |  |
| 5 | 6 | Masts | Main Top Sail Yard | 77 |  |
| 2 | 4 | Port cills from beams | Fore D ${ }^{\text {o }}$ | 67112 |  |
| 8 | 7 | Distance between the ports | Mizen ${ }^{\text {o }}$ | 58 |  |
| 2 | 6 | Fore \& aft clear | Main Top Gallant Yard | 47 |  |
| $2^{1 / 2}$ |  | Up \& Down | Fore D ${ }^{\text {o }}$ | 42 |  |
| 6 | 10 | Under the quarter deck | Mizen $\mathrm{D}^{\circ}$ | 36 |  |
| 6 | 4 | Fore Castle |  |  |  |
| $431 / 2$ |  | Length |  |  |  |

Quarter Deck within 2 feet of the main mast
5 Tumbling home
2 Hanging Gun Deck
66 Beak head abaft the rabbet
$3 \frac{1}{2}$ Fore port abaft $\mathrm{D}^{\circ} \quad$ For the honorable Navy Board

Joshua Humphreys Notebook

| Dimensions of Frigate Confederacy Hull | Feet | Inches |  |
| :---: | :---: | :---: | :---: |
| Length of Keel Straight Rabbet (133) | 133 |  |  |
| Breadth of Beam | 36 | 8 |  |
| Depth of Hold | 12 | 6 |  |
| Height between Decks | 6 | 3 |  |
| Gun Deck from Stem to Stern | 160 |  |  |
| Length from one point of the stern to the afterpart of the rabbet | 158 |  |  |
| Length of the quarter deck | 84 |  |  |
| Length of the forecastle | 40 |  |  |
| Height of the fore part of the quarter deck | 6 |  |  |
| Height of the afterpart of the forecastle | 6 | 4 |  |
| Masts |  |  |  |
|  | Diam | Length | Lgth of yd |
|  | Inch | Feet | Feet |
| Foremast | 27 | 82 | 111/2 |
| Main Mast | 28 | 88 | $12^{1 / 2}$ |
| Mizen Mast | 21 | 77 | $91 / 2$ |
| Bowsprit | 27 | 55 |  |
| Fore Top Mast | $181 / 4$ | 48 | 7 |
| Main Top Mast | 19 | 53 | $71 / 2$ |
| Mizen Top Mast | 13 | 38 | 61/2 |
| Fore Top Gallant Mast | $111 / 2$ | 26 | 21 |
| Main $\mathrm{D}^{\text {o }}$ | 12 | 281/2 | 23 |
| Mizen ${ }^{\text {o }}$ | $81 / 2$ | 20 | 16 |

Proportion for poling the Main Mast - 4 times the length of the Beam from the top of the keelson to the top Gallant Hounds

| Yards | Diam | Length |  |
| :---: | :---: | :---: | :---: |
|  | Inch | Feet |  |
| Fore Yard | 18 | 76 |  |
| Main Yard | 19 | $86^{1 / 2}$ |  |
| X Jack Yard | $12^{1 / 2}$ | 60 |  |
| Fore Top Sail Yards | 12 | 58 |  |
| Main ${ }^{\text {o }}$ |  | $12^{1 / 2}$ | 64 |
| Mizen ${ }^{\text {o }}$ | 10 | 46 |  |
| Fore Top Gallant Yard | 61/2 | 34 |  |
| Main ${ }^{\text {o }}$ |  | $71 / 4$ | 38 |
| Mizen $\mathrm{D}^{\text {o }}$ | $51 / 2$ | 28 |  |
| Jibb Boom | 13 | 41 |  |
| Mizen Derrick | 12 | 40 |  |
| Spritsail Yard | $11_{1 / 2}$ | 58 |  |
| Spritsail Top sail yard | $71 / 4$ | 38 |  |
| Fore Royal Yard |  |  | 18 |
| Main ${ }^{\circ}$ |  |  | 24 |
| Driver Boom | 10 | 52 |  |



TRANSCRIPTIONIST NOTE: There are 2 lines of text on the bottom of this page which are blacked out and completely indecipherable. There is also a signature on the bottom of the page that has been partially blacked out but is recognizable to this transcriptionist as Thomas Truxton.

Memorandum for the Weight of any Rope
Multiply the circumference by itself and divide the product by 4 gives the weight in lbs of one fathom of hauser lay'd ropes, but not so much in a cable by $1 / 10$ part, as in a hauser laid rope.

Of our common yarns in each strand for 4 Inch $\& 3 / 4$ hauser lay'd rope. Yarns in each strand for 6 inch \& $1 / 4$ hauser lay'd rope.

To warpe yarns for a stay 7 times the length of the stay to be brought about in four

3 |  | 19 | 3 | 19 | $4^{1 / 2}$ | 3 |
| :--- | :--- | :--- | :--- | :--- | :--- |

$\frac{19}{38}$ yarns for the inch
19
319
$\frac{91 / 2}{47}$
19
f 3:19:6
3:19:6
19
19
19
19
19
19
76 yarns a hook
$91 / 2$
85 thread for $6^{1 / 2}$ a hook
$\begin{array}{ll}3 & 19 \\ 7\end{array}$
19
19
19
19
95 threads a hook for 7 Inch, hawser lay'd rope, by this rule at the rate of 19 thread a hook for three Inch.

## To proportion yarns for any size Rope

If 3 Inch Rope take 19 thread a hook, how many will a four Inch require, as 3 is to 19 so is 4 to 25 the direct proportion; then say as 3 is to 25 so is four to the quantity of yarns required, which is 33 \& so for any other rope.

These proposals was made \& agreed upon by the Master and Journeyman in the Year of our Lord 1694.
Master to have but two apprentices in a ground at a time \& to take no Covenant Servants; but to serve three times under three masters Roof as an Apprentice ought to do, \& to employ none but what hath served a lawful time and if spinners do want Employ to hire no Labourers, but a wheel heaver.

Item for spinning to spin out nine threads together. To spin 24 threads of Riga hemp 22 of Riga \& pass 20 of all pass or Raffia of 160 fathom for a days work.

To warp Crankhalls of 180 threads 5 men 6 a day for capstand halls of 360 threads 8 men a day.
To tarr crank halls of 180 threads with a capstand, 5 men at the barr, 8 a day; with a crank 8 men at the crank, 12 a day Capstand Halls of 360 threads 8 men at the barn 8 a day.

To warpe \& lay top Sheets 4 pair a day. 6 tack strands from 5 in \& upwards ready warp'd for $1 / 4$ of a day \& the tacks 2 pair for $1 / 4$ of a day.

To lay twice lay'd Ropes upon the wheel warped 135 fathom; 12 a day, the same length for strands upon the wheel; Ropes upon the hooks from $2 \frac{1}{2}$ to 5 in 4 a day \& upwards, 3 a day the same length.

Head Ropes not to exceed 60 or 70 fathoms when lay'd 5 men 8 a day both ropes ye same length from $2^{1 / 4}$ to $31 / 45$ men; and all upward 6 men 4 a day.

For $1 / 2$ ropes white or tar'd from 3 In to 5 In one thread extra above ${ }^{1 / 2}$ the allowance of the whole rope from 5 in \& all upward 2 threads.

The yarn for short lay'd ropes to be warped 180 Fathom: for cable lay'd ropes 200 fathom, \& short lay'd ropes from $21 / 4$ to 3 inch handed upon the wheel.

Allowances for cords and cables

| Allowance for Hauser lay'd cordage |  |  |  | Allowance for cable strands |  |  |  | Allowance for Cables |  |  |  | Allowance for Strands \& Stays |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \ddot{N} \\ & \text { कै } \end{aligned}$ |  | $\begin{aligned} & \infty \\ & 0 \\ & 0 \\ & 0 \\ & \text { Ho } \\ & 0 \\ & 0 \end{aligned}$ |  | $\begin{aligned} & \stackrel{N}{N} \\ & \dot{\sim} \end{aligned}$ |  | $\begin{aligned} & n \\ & 0 \\ & 0 \\ & 0 \\ & \text { 山o } \\ & 0 \\ & 0 \end{aligned}$ |  | $\stackrel{\sim}{N}$ |  | $\begin{aligned} & \infty \\ & 0 \\ & 0 \\ & 0 \\ & \text { U } \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { d } \\ & 0 \\ & \dot{む} \\ & 0 \\ & 0 \\ & \text { o } \\ & 0 \\ & 0 \end{aligned}$ | $\stackrel{\ddot{N}}{\dot{\sim}}$ |  | $\begin{aligned} & \stackrel{\sim}{N} \\ & \dot{\sim} \end{aligned}$ |  |
| 7 | 24 | 0 | 3 | 18 | 35 | 0 | 3 | 18 | 70 | 0 | 2 | 15 | 2 | 9 | 3 |
| $6^{1 / 2}$ | 23 | 0 | 3 | 17 | 31 | 0 | 3 | 17 | 62 | 0 | 2 | $14^{1 / 2}$ | 2 | $81 / 2$ | 4 |
| 6 | 21 | 0 | 3 | 16 | 258 | 0 | 3 | 16 | 54 | 0 | 2 | 14 | 2 | 8 | 4 |
| $51 / 2$ | 16 | 0 | 3 | 15 | 26 | 0 | 3 | 15 | 50 | 0 | 2 | $13^{1 / 2}$ | 2 | 7112 | 4 |
| 5 | 14 | 0 | 3 | 14 | 23 | 0 | 3 | 14 | 44 | 0 | 2 | 13 | 2 | 7 | 4 |
| $41 / 2$ | 12 | 0 | 4 | 13 | 21 | 0 | 3 | 13 | 40 | 0 | 2 | $12^{1 / 2}$ | 2 | $61 / 2$ | 4 |
| 4 | 12 | 0 | 4 | 12 | 17 | 0 | 4 | 12 | 36 | 0 | 6 | 12 | 2 | 6 | 4 |
| 3112 | 10 | 0 | 4 | 11 | 15 | 0 | 4 | 11 | 34 | 0 | 3 | $11^{1 / 2}$ | 3 | 5112 | 4 |
| $31 / 4$ | 9 | 0 | 4 | 10 | 14 | 0 | 4 | 10 | 29 | 0 | 3 | 11 | 3 | 5 | 4 |
| 3 | 8 | 0 | 4 | 9 | 11 | 0 | 4 | 9 | 27 | 0 | 3 | $10^{1 / 2}$ | 3 | $4^{1 / 2}$ | 4 |
| $23 / 4$ | 7 | 0 | 4 | 8 | 9 | 0 | 4 | 8 | 24 | 0 | 4 | 10 | 3 | 4 | 4 |
| $21 / 2$ | 5 | 0 | 4 | 7 | 8 | 0 | 4 | 7 | 17 | 3 | 4 | 9 | 3 | 3 | 3 |
| $21 / 4$ | 4 | 1 | 4 | 6 | 7 | 0 | 4 | 6 | 15 | 0 | 4 |  |  |  |  |
| 2 | 8 | 2 | 12 | 5 | 5 | 1 | 4 | 5 | 12 | 1 | 4 |  |  |  |  |
| $13 / 4$ | 8 | 2 | 12 | $4^{1 / 2}$ | 8 | 1 | 12 | $4^{112}$ | 11 | 1 | 4 |  |  |  |  |
| $11 / 2$ | 7 | 1 | 12 | 4 | 7 | 1 | 12 | 4 | 1 | 0 | 4 |  |  |  |  |
| $11 / 4$ | 7 | 1 | 12 | $31 / 2$ | 6 | 1 | 12 | $31 / 2$ | 8 | 0 | 4 |  |  |  |  |
| 1 | 5 | 2 | 12 | 3 | 5 | 1 | 12 | 3 | 7 | 0 | 4 |  |  |  |  |
| $3 / 4$ | 5 | 2 | 12 |  |  |  |  |  |  |  |  |  |  |  |  |


| Allowance for White Shrouds |  |  |  | A table from 12 thread a hook for 3 inch to 16 for 3 inch hauser lay'd |  |  |  |  |  |  | A table from 12 thread a hook for 3 inch to 20-3 inch hauser lay'd |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| \% | $\begin{aligned} & \text { 영 } \\ & \text { d } \end{aligned}$ |  |  | $\begin{aligned} & \dot{む} \\ & \stackrel{0}{0} \\ & \end{aligned}$ | Inch | 12 | 13 | 14 | 15 | 16 | Inch | 17 | 18 | 19 | 20 |
|  | Z | O. .ٌ | $\stackrel{\circ}{\square}$ | $\stackrel{\square}{9}$ | 9 | 108 | 117 | 126 | 135 | 144 | 9 | 153 | 162 | 111 | 180 |
| 8 | 14 | 6 | 42 | 2 | $81 / 2$ | 95 | 107 | 112 | 120 | 128 | $81 / 2$ | 136 | 144 | 152 | 160 |
| $71 / 2$ | 16 | 6 | 37 | 2 | 8 | 85 | 92 | 99 | 106 | 113 | 8 | 120 | 123 | 135 | 147 |
| 7 | 14 | 6 | 32 | 2 | $711 / 2$ | 75 | 81 | 87 | 93 | 100 | $71 / 2$ | 106 | 112 | 118 | 125 |
| $61 / 2$ | 14 | 4 | 28 | 10 | 7 | 65 | 70 | 76 | 81 | 87 | 7 | 92 | 93 | 103 | 108 |
| 6 | 12 | 4 | 25 | 10 | $61 / 2$ | 56 | 61 | 65 | 70 | 75 | $61 / 2$ | 97 | 84 | 896 | 95 |
| $51 / 2$ | 12 | 3 | 21 | 9 | 6 | 48 | 52 | 56 | 60 | 64 | 6 | 68 | 72 | 76 | 80 |
| 5 | 11 | 3 | 19 | 9 | $5^{11 / 2}$ | 40 | 43 | 47 | 50 | 53 | $51 / 2$ | 57 | 60 | 63 | 67 |
| $41 / 2$ | 9 | 2 | 16 | 4 | 5 | 33 | 36 | 38 | 51 | 44 | 5 | 47 | 50 | 52 | 55 |
| 4 | 9 | 2 | 14 | 4 | $41 / 2$ | 27 | 29 | 31 | 33 | 36 | $41 / 2$ | 38 | 40 | 42 | 45 |
| $31 / 2$ | 7 | 2 | 12 | 4 | 4 | 21 | 23 | 24 | 26 | 28 | 4 | 30 | 32 | 33 | 35 |
| 3 | 7 | 2 | 11 | 4 | $31 / 2$ | 16 | 17 | 19 | 20 | 21 | $31 / 2$ | 23 | 24 | 25 | 27 |
|  |  |  |  |  | 3 | 12 | 13 | 14 | 15 | 16 | 3 | 17 | 18 | 19 | 20 |
|  |  |  |  |  | $2^{1 / 2}$ | 8 | 9 | 9 | 10 | 11 | $21 / 2$ | 11 | 12 | 13 | 19 |


| A Table from 21 thread a hook for 3 inch to 24 for 3 inch Hauser Lay'd |  |  |  |  | A Table from 25 thread a hook for 3 inch to 28 for 3 inch Hauser Lay'd |  |  |  |  | A Table from 29 thread a hook for 3 inch to 32 for 3 inch Hauser Lay'd |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inch | 21 | 22 | 23 | 24 | Inch | 25 | 26 | 27 | 28 | Inch | 29 | 30 | 31 | 32 |
| 9 | 189 | 198 | 207 | 216 | 9 | 225 | 234 | 243 | 252 | 9 | 261 | 270 | 279 | 288 |
| $81 / 2$ | 168 | 176 | 184 | 192 | $81 / 2$ | 200 | 208 | 216 | 224 | $81 / 2$ | 232 | 240 | 248 | 256 |
| 8 | 149 | 156 | 163 | 170 | 8 | 177 | 184 | 192 | 199 | 8 | 206 | 213 | 220 | 227 |
| 7112 | 131 | 137 | 143 | 150 | $71 / 2$ | 156 | 162 | 168 | 175 | $71 / 2$ | 181 | 187 | 193 | 200 |
| 7 | 114 | 119 | 124 | 130 | 7 | 136 | 141 | 147 | 152 | 7 | 157 | 163 | 168 | 174 |
| $61 / 2$ | 99 | 103 | 107 | 112 | $61 / 2$ | 117 | 121 | 126 | 131 | $61 / 2$ | 136 | 140 | 145 | 150 |
| 6 | 84 | 88 | 92 | 96 | 6 | 100 | 104 | 108 | 112 | 6 | 116 | 120 | 124 | 128 |
| 5112 | 70 | 73 | 77 | 80 | $51 / 2$ | 84 | 87 | 90 | 94 | $51 / 2$ | 97 | 100 | 104 | 107 |
| 5 | 58 | 61 | 63 | 66 | 5 | 69 | 72 | 75 | 77 | 5 | 80 | 83 | 86 | 88 |
| $4^{1 / 2}$ | 47 | 49 | 51 | 54 | $4^{1 / 2}$ | 56 | 58 | 60 | 63 | $4^{11 / 2}$ | 65 | 67 | 70 | 72 |
| 4 | 37 | 39 | 40 | 42 | 4 | 44 | 46 | 48 | 49 | 4 | 51 | 53 | 55 | 45 |
| 3112 | 28 | 29 | 31 | 32 | 3112 | 34 | 35 | 36 | 38 | $31 / 2$ | 39 | 40 | 42 | 43 |
| 3 | 21 | 22 | 23 | 24 | 3 | 25 | 26 | 27 | 28 | 3 | 29 | 30 | 31 | 32 |
| $2^{1 / 2}$ | 14 | 15 | 15 | 16 | $21 / 2$ | 17 | 18 | 18 | 19 | $21 / 2$ | 20 | 20 | 21 | 22 |


| A Table from 33 thread a hook for 3 inch to 34 for 3 inch Hauser Lay'd |  |  | A Table from 15 thread a hook for six inch to 19 for 6 in cable Lay'd |  |  |  |  |  | A Table from 15 thread a hook for 6 inch to 19 for 6 inch Cable Lay'd |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inch | 33 | 34 | Inch | 15 | 16 | 17 | 18 | 19 | Inch | 15 | 16 | 17 |
| 9 | 297 | 306 | 18 | 135 | 144 | 153 | 162 | 171 | $10^{1 / 2}$ | 45 | 49 | 52 |
| $81 / 2$ | 264 | 272 | $171 / 2$ | 127 | 136 | 144 | 153 | 161 | 10 | 51 | 44 | 47 |
| 8 | 234 | 241 | 17 | 120 | 128 | 136 | 144 | 152 | $91 / 2$ | 37 | 40 | 42 |
| $71 / 2$ | 206 | 212 | $16^{1 / 2}$ | 113 | 121 | 128 | 136 | 143 | 9 | 33 | 36 | 38 |
| 7 | 179 | 185 | 16 | 106 | 113 | 220 | 128 | 135 | $81 / 2$ | 30 | 32 | 34 |
| $6^{1 / 2}$ | 154 | 159 | $15^{1 / 2}$ | 100 | 106 | 113 | 120 | 126 | 8 | 26 | 28 | 30 |
| 6 | 132 | 136 | 16 | 93 | 100 | 106 | 112 | 118 | $71 / 2$ | 23 | 25 | 26 |
| $51 / 2$ | 110 | 114 | $14^{1 / 2}$ | 87 | 93 | 99 | 105 | 110 | 7 | 20 | 21 | 23 |
| 5 | 194 | 97 | 14 | 81 | 87 | 92 | 98 | 103 | $61 / 2$ | 17 | 18 | 19 |
| $4^{1 / 2}$ | 74 | 76 | $131 / 2$ | 75 | 81 | 86 | 91 | 96 | 6 | 15 | 16 | 17 |
| 4 | 58 | 60 | 13 | 70 | 75 | 79 | 84 | 89 | $51 / 2$ | 12 | 13 | 14 |
| $31 / 2$ | 44 | 46 | $12^{1 / 2}$ | 65 | 69 | 73 | 78 | 82 | 5 | 10 | 11 | 11 |
| 3 | 33 | 34 | 12 | 60 | 64 | 68 | 72 | 76 | $4^{1 / 2}$ | 8 | 9 | 9 |
| $2^{1 / 2}$ | 22 | 23 | $11^{1 / 2}$ | 55 | 58 | 62 | 66 | 69 | 4 | 6 | 7 | 7 |
|  |  |  | 11 | 50 | 53 | 57 | 60 | 63 | $31 / 2$ | 5 | 5 | 5 |
|  |  |  |  |  |  |  |  |  | 3 | 4 | 4 | 4 |


| A Table from 20 threads a hook for 6 inch to 24 for 6 in cable lay'd |  |  |  |  |  | A Table for 20 thread a hook for 6 inch to 24 for 6 in cable Lay'd |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Inches | 20 | 21 | 22 | 23 | 24 | Inches | 20 | 21 | 22 | 23 | 24 |
| 18 | 180 | 189 | 198 | 207 | 216 | $10^{1 / 2}$ | 61 | 64 | 67 | 70 | 73 |
| $17^{1 / 2}$ | 170 | 179 | 187 | 198 | 206 | 10 | 55 | 58 | 61 | 63 | 66 |
| 17 | 160 | 168 | 176 | 184 | 192 | $91 / 2$ | 50 | 52 | 55 | 57 | 60 |
| $16^{1 / 2}$ | 151 | 157 | 166 | 173 | 181 | 9 | 45 | 47 | 49 | 51 | 54 |
| 16 | 142 | 149 | 156 | 163 | 170 | $81 / 2$ | 40 | 42 | 44 | 46 | 48 |
| $15^{1 / 2}$ | 133 | 140 | 146 | 153 | 160 | 8 | 35 | 37 | 39 | 40 | 42 |
| 15 | 125 | 131 | 137 | 143 | 179 | 7112 | 31 | 32 | 32 | 35 | 37 |
| $141 / 2$ | 116 | 122 | 128 | 134 | 140 | 7 | 27 | 28 | 29 | 31 | 32 |
| 14 | 108 | 114 | 119 | 125 | 130 | $61 / 2$ | 23 | 24 | 25 | 26 | 28 |
| $131 / 2$ | 101 | 106 | 111 | 116 | 121 | 6 | 20 | 21 | 22 | 23 | 24 |
| 13 | 93 | 98 | 103 | 107 | 112 | $51 / 2$ | 16 | 17 | 18 | 19 | 20 |
| 12 | 86 | 91 | 95 | 99 | 104 | 5 | 13 | 14 | 15 | 15 | 15 |
| $11^{1 / 2}$ | 73 | 77 | 80 | 84 | 88 | $4^{11 / 2}$ | 11 | 11 | 12 | 12 | 13 |
| 11 | 67 | 70 | 73 | 77 | 80 | 4 | 8 | 9 | 9 | 10 | 10 |
|  |  |  |  |  |  | $31 / 2$ | 6 | 7 | 7 | 7 | 8 |
|  |  |  |  |  |  | 3 | 5 | 5 | 5 | 6 | 6 |

A Table to Shew the weight of cable lay'd cordage from 1 fathom to 120 at every 5 fathom

| The Weight of 18 in cable |  |  |  |  | The weight of $171 / 2$ inch cable |  |  |  |  | The weight of 17 inch cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qt | Lb | Oz | Fath | Ct | Qt | Lb | Oz | Fath | Ct | Qt | Lb | Oz |
| 1 | 0 | 2 | 19 | 9 | 1 | 0 | 2 | 15 | 7 | 1 | 0 | 2 | 11 | 9 |
| 5 | 3 | 1 | 14 | 0 | 5 | 3 | 0 | 21 | 5 | 5 | 3 | 0 | 1 | 3 |
| 10 | 6 | 3 | 0 | 0 | 10 | 6 | 1 | 14 | 10 | 10 | 6 | 0 | 2 | 6 |
| 15 | 10 | 0 | 14 | 0 | 15 | 9 | 3 | 7 | 14 | 15 | 9 | 0 | 3 | 8 |
| 20 | 13 | 2 | 0 | 0 | 20 | 12 | 2 | 1 | 3 | 20 | 12 | 0 | 4 | 11 |
| 25 | 16 | 3 | 14 | 0 | 25 | 15 | 3 | 22 | 8 | 25 | 15 | 0 | 5 | 14 |
| 30 | 20 | 1 | 0 | 0 | 30 | 19 | 0 | 15 | 12 | 30 | 18 | 0 | 7 | 0 |
| 35 | 23 | 2 | 14 | 0 | 35 | 22 | 1 | 9 | 1 | 35 | 21 | 0 | 8 | 3 |
| 40 | 27 | 0 | 0 | 0 | 40 | 25 | 2 | 2 | 6 | 40 | 24 | 0 | 9 | 6 |
| 45 | 30 | 1 | 14 | 0 | 45 | 28 | 2 | 23 | 10 | 45 | 27 | 0 | 10 | 8 |
| 50 | 33 | 3 | 0 | 0 | 50 | 31 | 3 | 16 | 15 | 50 | 30 | 0 | 11 | 11 |
| 55 | 37 | 0 | 14 | 0 | 55 | 35 | 0 | 10 | 4 | 55 | 33 | 0 | 12 | 14 |
| 60 | 40 | 2 | 0 | 0 | 60 | 38 | 1 | 3 | 8 | 60 | 36 | 0 | 14 | 3 |
| 65 | 43 | 3 | 14 | 0 | 65 | 41 | 1 | 24 | 3 | 65 | 39 | 0 | 15 | 3 |
| 70 | 47 | 1 | 0 | 0 | 70 | 44 | 2 | 18 | 2 | 70 | 42 | 0 | 16 | 6 |
| 75 | 50 | 2 | 14 | 0 | 75 | 47 | 3 | 11 | 6 | 75 | 45 | 0 | 17 | 8 |
| 80 | 54 | 0 | 0 | 0 | 80 | 51 | 0 | 4 | 11 | 80 | 48 | 0 | 18 | 11 |
| 85 | 57 | 1 | 14 | 0 | 85 | 54 | 0 | 26 | 0 | 85 | 51 | 0 | 19 | 14 |
| 90 | 60 | 3 | 0 | 0 | 90 | 57 | 1 | 19 | 4 | 90 | 54 | 0 | 21 | 0 |
| 95 | 64 | 0 | 14 | 0 | 95 | 60 | 2 | 12 | 9 | 95 | 57 | 0 | 22 | 3 |
| 100 | 67 | 2 | 0 | 0 | 100 | 63 | 3 | 5 | 14 | 100 | 60 | 0 | 23 | 6 |
| 105 | 70 | 3 | 14 | 0 | 105 | 66 | 3 | 27 | 2 | 105 | 63 | 0 | 24 | 8 |
| 110 | 71 | 1 | 0 | 0 | 110 | 70 | 0 | 20 | 7 | 110 | 66 | 0 | 25 | 11 |
| 120 | 81 | 0 | 0 | 0 | 120 | 76 | 2 | 7 | 0 | 115 | 69 | 0 | 26 | 14 |
|  |  |  |  |  |  |  |  |  |  | 120 | 72 | 1 | 0 | 0 |

A table to show the weight of Cable Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of $16^{1 / 2}$ inch cable |  |  |  |  | The weight of 16 in cable |  |  |  |  | The weight of $15^{1 / 2}$ in cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | $\mathrm{Q}^{\text {r }}$ | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 2 | 7 | 6 | 1 | 0 | 2 | 3 | 11 | 1 | 0 | 2 | 0 | 1 |
| 5 | 2 | 3 | 9 | 10 | 5 | 2 | 2 | 18 | 11 | 5 | 2 | 2 | 0 | 5 |
| 10 | 5 | 2 | 19 | 4 | 10 | 5 | 1 | 9 | 6 | 10 | 5 | 0 | 0 | 11 |
| 15 | 8 | 2 | 0 | 14 | 15 | 8 | 0 | 0 | 0 | 15 | 7 | 2 | 0 | 14 |
| 20 | 11 | 1 | 10 | 8 | 20 | 10 | 2 | 18 | 11 | 20 | 10 | 0 | 1 | 3 |
| 25 | 14 | 0 | 22 | 2 | 25 | 13 | 1 | 9 | 6 | 25 | 12 | 2 | 1 | 8 |
| 30 | 17 | 0 | 1 | 12 | 30 | 16 | 0 | 0 | 0 | 30 | 15 | 0 | 1 | 2 |
| 35 | 19 | 3 | 11 | 6 | 35 | 18 | 2 | 18 | 11 | 35 | 17 | 2 | 2 | 1 |
| 40 | 22 | 2 | 21 | 0 | 40 | 21 | 1 | 9 | 6 | 40 | 20 | 0 | 2 | 6 |
| 45 | 25 | 2 | 2 | 10 | 45 | 24 | 0 | 0 | 0 | 45 | 22 | 2 | 2 | 10 |
| 50 | 28 | 1 | 12 | 4 | 50 | 26 | 2 | 18 | 11 | 50 | 25 | 0 | 2 | 15 |
| 55 | 31 | 0 | 21 | 14 | 55 | 29 | 1 | 9 | 6 | 55 | 27 | 2 | 3 | 4 |
| 60 | 34 | 0 | 3 | 8 | 60 | 32 | 0 | 0 | 0 | 60 | 30 | 0 | 3 | 8 |
| 65 | 36 | 3 | 13 | 2 | 65 | 34 | 2 | 18 | 11 | 65 | 32 | 2 | 3 | 12 |
| 70 | 39 | 2 | 22 | 12 | 70 | 37 | 1 | 9 | 6 | 70 | 35 | 0 | 4 | 1 |
| 75 | 42 | 2 | 4 | 6 | 75 | 40 | 0 | 0 | 0 | 75 | 37 | 2 | 4 | 6 |
| 80 | 45 | 1 | 14 | 0 | 80 | 42 | 2 | 18 | 11 | 80 | 40 | 2 | 4 | 15 |
| 85 | 48 | 0 | 23 | 10 | 85 | 45 | 1 | 9 | 6 | 85 | 42 | 2 | 4 | 15 |
| 90 | 51 | 0 | 5 | 9 | 90 | 48 | 0 | 0 | 0 | 90 | 45 | 0 | 5 | 4 |
| 95 | 43 | 3 | 14 | 14 | 95 | 50 | 2 | 18 | 11 | 95 | 47 | 2 | 5 | 9 |
| 100 | 46 | 2 | 24 | 8 | 100 | 53 | 1 | 9 | 6 | 100 | 50 | 0 | 5 | 14 |
| 105 | 59 | 2 | 6 | 2 | 105 | 56 | 0 | 0 | 0 | 105 | 52 | 2 | 6 | 2 |
| 110 | 62 | 1 | 15 | 12 | 110 | 58 | 2 | 18 | 11 | 110 | 55 | 0 | 6 | 7 |
| 115 | 65 | 0 | 25 | 6 | 115 | 61 | 1 | 9 | 6 | 115 | 57 | 2 | 6 | 12 |
| 120 | 68 | 0 | 7 | 0 | 120 | 64 | 0 | 0 | 0 | 120 | 60 | 0 | 7 | 0 |


| The weight of 15 inch cable |  |  |  |  | The weight of $14^{1} / 2$ inch cable |  |  |  |  | The weight of 14 inch cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 1 | 24 | 8 | 1 | 0 | 1 | 21 | 1 | 1 | 0 | 1 | 17 | 10 |
| 5 | 2 | 1 | 10 | 8 | 5 | 2 | 0 | 21 | 5 | 5 | 2 | 8 | 4 |  |
| 10 | 4 | 2 | 21 | 0 | 10 | 4 | 1 | 14 | 10 | 10 | 4 | 0 | 9 | 5 |
| 15 | 7 | 0 | 3 | 8 | 15 | 6 | 2 | 7 | 14 | 15 | 6 | 0 | 14 | 0 |
| 20 | 9 | 1 | 14 | 0 | 20 | 8 | 3 | 1 | 3 | 20 | 8 | 0 | 18 | 10 |
| 25 | 11 | 2 | 24 | 8 | 25 | 10 | 3 | 22 | 8 | 25 | 10 | 0 | 23 | 5 |
| 30 | 14 | 0 | 7 | 0 | 30 | 13 | 0 | 15 | 12 | 30 | 12 | 1 | 3 | 0 |
| 35 | 16 | 1 | 17 | 8 | 35 | 15 | 1 | 9 | 1 | 35 | 14 | 1 | 4 | 10 |
| 40 | 18 | 3 | 0 | 0 | 40 | 17 | 2 | 2 | 6 | 40 | 16 | 1 | 9 | 5 |
| 45 | 21 | 0 | 10 | 8 | 45 | 19 | 2 | 23 | 10 | 45 | 18 | 1 | 14 | 0 |
| 50 | 23 | 1 | 21 | 0 | 50 | 21 | 3 | 16 | 15 | 50 | 20 | 1 | 18 | 1 |
| 55 | 25 | 3 | 3 | 8 | 55 | 24 | 0 | 10 | 4 | 55 | 22 | 1 | 23 | 5 |
| 60 | 28 | 0 | 14 | 0 | 60 | 26 | 1 | 3 | 8 | 60 | 24 | 2 | 0 | 0 |
| 65 | 30 | 1 | 24 | 8 | 65 | 28 | 1 | 24 | 13 | 65 | 26 | 2 | 4 | 10 |
| 70 | 32 | 3 | 7 | 0 | 70 | 30 | 2 | 18 | 2 | 70 | 28 | 2 | 9 | 5 |
| 75 | 35 | 0 | 17 | 8 | 75 | 32 | 3 | 11 | 6 | 75 | 30 | 2 | 14 | 0 |
| 80 | 37 | 2 | 0 | 0 | 80 | 35 | 0 | 4 | 11 | 80 | 32 | 2 | 18 | 10 |
| 85 | 40 | 0 | 10 | 8 | 85 | 37 | 0 | 26 | 0 | 85 | 34 | 2 | 23 | 5 |
| 90 | 42 | 1 | 21 | 0 | 90 | 39 | 1 | 19 | 4 | 90 | 36 | 3 | 0 | 0 |
| 95 | 44 | 2 | 3 | 8 | 95 | 41 | 2 | 10 | 12 | 95 | 38 | 3 | 4 | 10 |
| 100 | 46 | 3 | 14 | 0 | 100 | 43 | 3 | 5 | 15 | 100 | 40 | 3 | 9 | 5 |
| 105 | 49 | 0 | 24 | 8 | 105 | 45 | 3 | 27 | 2 | 105 | 42 | 3 | 14 | 0 |
| 110 | 50 | 2 | 7 | 0 | 110 | 48 | 0 | 20 | 7 | 110 | 44 | 3 | 18 | 10 |
| 115 | 53 | 3 | 17 | 8 | 115 | 50 | 1 | 15 | 12 | 115 | 46 | 3 | 23 | 5 |
| 120 | 56 | 1 | 0 | 0 | 120 | 52 | 2 | 7 | 0 | 120 | 48 | 0 | 0 | 0 |

A table to show the weight of Cable Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of $131 / 2$ inch cable |  |  |  |  | The weight of 13 in cable |  |  |  |  | The weight of $12^{1 / 2}$ in cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 1 | 14 | 8 | 1 | 0 | 1 | 11 | 7 | 1 | 0 | 1 | 8 | 7 |
| 5 | 1 | 3 | 16 | 10 | 5 | 1 | 3 | 1 | 2 | 5 | 1 | 2 | 14 | 5 |
| 10 | 3 | 3 | 5 | 4 | 10 | 3 | 2 | 2 | 5 | 10 | 3 | 1 | 0 | 10 |
| 15 | 5 | 2 | 21 | 14 | 15 | 5 | 1 | 3 | 8 | 15 | 4 | 3 | 14 | 14 |
| 20 | 7 | 2 | 10 | 8 | 20 | 7 | 0 | 4 | 10 | 20 | 6 | 2 | 1 | 3 |
| 25 | 9 | 1 | 27 | 2 | 25 | 8 | 3 | 5 | 13 | 25 | 8 | 0 | 15 | 8 |
| 30 | 11 | 1 | 15 | 12 | 30 | 10 | 2 | 7 | 0 | 30 | 9 | 3 | 1 | 2 |
| 35 | 13 | 1 | 4 | 6 | 35 | 12 | 1 | 8 | 2 | 35 | 11 | 1 | 16 | 1 |
| 40 | 15 | 1 | 21 | 0 | 40 | 14 | 0 | 9 | 5 | 40 | 13 | 0 | 2 | 6 |
| 45 | 17 | 0 | 9 | 10 | 45 | 15 | 3 | 10 | 8 | 45 | 14 | 2 | 16 | 10 |
| 50 | 18 | 3 | 26 | 4 | 50 | 17 | 2 | 11 | 10 | 50 | 16 | 1 | 2 | 14 |
| 55 | 20 | 3 | 14 | 14 | 55 | 19 | 1 | 12 | 8 | 55 | 17 | 3 | 17 | 3 |
| 60 | 22 | 3 | 3 | 8 | 60 | 21 | 0 | 14 | 0 | 60 | 19 | 2 | 3 | 8 |
| 65 | 24 | 2 | 20 | 2 | 65 | 22 | 3 | 15 | 2 | 65 | 21 | 0 | 17 | 12 |
| 70 | 26 | 2 | 8 | 12 | 70 | 24 | 2 | 16 | 25 | 70 | 22 | 3 | 4 | 1 |
| 75 | 28 | 1 | 25 | 6 | 75 | 26 | 1 | 17 | 8 | 75 | 24 | 1 | 18 | 6 |
| 80 | 30 | 1 | 14 | 0 | 80 | 28 | 0 | 18 | 10 | 80 | 26 | 0 | 4 | 10 |
| 85 | 32 | 1 | 2 | 10 | 85 | 29 | 3 | 19 | 13 | 85 | 27 | 2 | 18 | 15 |
| 90 | 34 | 0 | 19 | 4 | 90 | 31 | 2 | 21 | 0 | 90 | 29 | 1 | 5 | 4 |
| 95 | 36 | 0 | 7 | 14 | 95 | 33 | 1 | 22 | 2 | 95 | 30 | 3 | 19 | 9 |
| 100 | 37 | 3 | 24 | 8 | 100 | 35 | 0 | 23 | 5 | 100 | 32 | 2 | 5 | 4 |
| 105 | 39 | 3 | 13 | 2 | 105 | 36 | 3 | 24 | 8 | 105 | 34 | 0 | 20 | 2 |
| 110 | 41 | 3 | 1 | 12 | 110 | 38 | 2 | 25 | 10 | 110 | 35 | 3 | 6 | 6 |
| 115 | 43 | 2 | 18 | 6 | 115 | 40 | 1 | 26 | 13 | 115 | 37 | 1 | 20 | 11 |
| 120 | 45 | 2 | 7 | 0 | 120 | 42 | 1 | 0 | 0 | 120 | 39 | 0 | 0 | 7 |

A table to show the weight of Cable Lay'd
Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of 12 inch cable |  |  |  |  | The weight of $11 \frac{1}{2}$ inch cable |  |  |  |  | The weight of 11 inch cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 1 | 5 | 9 | 1 | 0 | 1 | 2 | 13 | 1 | 0 | 1 | 0 | 4 |
| 5 | 1 | 2 | 0 | 0 | 5 | 1 | 1 | 14 | 5 | 5 | 1 | 1 | 1 | 3 |
| 10 | 3 | 0 | 0 | 0 | 10 | 2 | 3 | 0 | 10 | 10 | 2 | 2 | 2 | 6 |
| 15 | 4 | 2 | 0 | 0 | 15 | 4 | 0 | 14 | 14 | 15 | 3 | 3 | 3 | 8 |
| 20 | 6 | 0 | 0 | 0 | 20 | 5 | 2 | 1 | 3 | 20 | 5 | 0 | 4 | 11 |
| 25 | 7 | 2 | 0 | 0 | 25 | 6 | 3 | 15 | 8 | 25 | 6 | 1 | 5 | 14 |
| 30 | 9 | 0 | 0 | 0 | 30 | 8 | 1 | 1 | 12 | 30 | 7 | 2 | 7 | 0 |
| 35 | 10 | 2 | 0 | 0 | 35 | 9 | 2 | 16 | 1 | 35 | 8 | 3 | 8 | 3 |
| 40 | 12 | 0 | 0 | 0 | 40 | 11 | 0 | 2 | 6 | 40 | 10 | 0 | 9 | 6 |
| 45 | 13 | 2 | 0 | 0 | 45 | 12 | 1 | 16 | 11 | 45 | 11 | 1 | 10 | 8 |
| 50 | 15 | 0 | 0 | 0 | 50 | 13 | 3 | 2 | 15 | 50 | 12 | 2 | 11 | 11 |
| 55 | 16 | 2 | 0 | 0 | 55 | 15 | 0 | 17 | 3 | 55 | 13 | 3 | 12 | 14 |
| 60 | 18 | 0 | 0 | 0 | 60 | 16 | 2 | 3 | 8 | 60 | 15 | 0 | 14 | 0 |
| 65 | 19 | 2 | 0 | 0 | 65 | 17 | 3 | 17 | 13 | 65 | 16 | 1 | 15 | 3 |
| 70 | 21 | 0 | 0 | 0 | 70 | 19 | 1 | 4 | 2 | 70 | 17 | 2 | 16 | 6 |
| 75 | 22 | 2 | 0 | 0 | 75 | 20 | 2 | 18 | 6 | 75 | 18 | 3 | 17 | 8 |
| 80 | 24 | 0 | 0 | 0 | 80 | 22 | 0 | 4 | 11 | 80 | 20 | 0 | 18 | 11 |
| 85 | 25 | 2 | 0 | 0 | 85 | 23 | 1 | 19 | 0 | 85 | 21 | 1 | 19 | 14 |
| 90 | 27 | 0 | 0 | 0 | 90 | 24 | 3 | 5 | 4 | 90 | 22 | 2 | 21 | 0 |
| 95 | 28 | 2 | 0 | 0 | 95 | 26 | 0 | 19 | 9 | 95 | 23 | 3 | 22 | 3 |
| 100 | 30 | 0 | 0 | 0 | 100 | 27 | 2 | 5 | 14 | 100 | 25 | 0 | 23 | 6 |
| 105 | 31 | 2 | 0 | 0 | 105 | 28 | 3 | 20 | 2 | 105 | 26 | 1 | 24 | 8 |
| 110 | 33 | 0 | 0 | 0 | 110 | 30 | 1 | 6 | 7 | 110 | 27 | 2 | 25 | 11 |
| 115 | 34 | 2 | 0 | 0 | 115 | 31 | 2 | 20 | 12 | 115 | 28 | 3 | 26 | 14 |
| 120 | 36 | 0 | 0 | 0 | 120 | 33 | 0 | 7 | 0 | 120 | 30 | 1 | 0 | 0 |

A table to show the weight of Cable Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of $101 / 2$ inch cable |  |  |  |  | The weight of 10 in cable |  |  |  |  | The weight of $91 / 2$ in cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 25 | 11 | 1 | 0 | 0 | 23 | 6 | 1 | 0 | 0 | 21 | 0 |
| 5 | 1 | 0 | 16 | 10 | 5 | 1 | 0 | 4 | 11 | 5 | 0 | 3 | 21 | 5 |
| 10 | 2 | 1 | 5 | 4 | 10 | 2 | 0 | 9 | 6 | 10 | 1 | 3 | 14 | 10 |
| 15 | 3 | 1 | 21 | 14 | 15 | 3 | 0 | 14 | 0 | 15 | 2 | 3 | 7 | 14 |
| 20 | 4 | 1 | 10 | 8 | 20 | 4 | 0 | 18 | 11 | 20 | 3 | 3 | 1 | 3 |
| 25 | 5 | 2 | 27 | 2 | 25 | 5 | 0 | 23 | 6 | 25 | 4 | 2 | 22 | 8 |
| 30 | 6 | 3 | 15 | 12 | 30 | 6 | 1 | 0 | 0 | 30 | 5 | 2 | 15 | 12 |
| 35 | 8 | 0 | 4 | 6 | 35 | 7 | 1 | 4 | 11 | 35 | 6 | 2 | 9 | 1 |
| 40 | 9 | 0 | 21 | 0 | 40 | 8 | 1 | 9 | 6 | 40 | 7 | 2 | 2 | 6 |
| 45 | 10 | 1 | 9 | 10 | 45 | 9 | 1 | 14 | 0 | 45 | 8 | 1 | 23 | 10 |
| 50 | 11 | 1 | 26 | 4 | 50 | 10 | 1 | 18 | 11 | 50 | 9 | 1 | 16 | 15 |
| 55 | 12 | 2 | 14 | 12 | 55 | 11 | 1 | 23 | 6 | 55 | 10 | 1 | 10 | 4 |
| 60 | 13 | 3 | 3 | 8 | 60 | 12 | 2 | 0 | 0 | 60 | 11 | 1 | 3 | 8 |
| 65 | 14 | 3 | 20 | 2 | 65 | 13 | 2 | 4 | 11 | 65 | 12 | 0 | 21 | 3 |
| 70 | 16 | 0 | 8 | 12 | 70 | 14 | 2 | 9 | 6 | 70 | 13 | 0 | 18 | 2 |
| 75 | 17 | 0 | 25 | 6 | 75 | 15 | 2 | 14 | 0 | 75 | 14 | 0 | 11 | 6 |
| 80 | 18 | 1 | 19 | 0 | 80 | 16 | 2 | 18 | 11 | 80 | 15 | 0 | 4 | 11 |
| 85 | 19 | 2 | 2 | 10 | 85 | 17 | 2 | 23 | 6 | 85 | 15 | 3 | 26 | 0 |
| 90 | 20 | 2 | 19 | 4 | 90 | 18 | 3 | 0 | 0 | 90 | 16 | 3 | 19 | 4 |
| 95 | 21 | 3 | 7 | 14 | 95 | 19 | 3 | 4 | 11 | 95 | 17 | 3 | 12 | 9 |
| 100 | 22 | 3 | 24 | 8 | 100 | 20 | 3 | 9 | 6 | 100 | 18 | 3 | 5 | 14 |
| 105 | 24 | 0 | 13 | 2 | 105 | 21 | 3 | 14 | 0 | 105 | 19 | 2 | 27 | 2 |
| 110 | 25 | 1 | 1 | 12 | 110 | 22 | 3 | 3 | 11 | 110 | 20 | 2 | 20 | 7 |
| 115 | 26 | 1 | 18 | 6 | 115 | 23 | 3 | 23 | 6 | 115 | 21 | 2 | 13 | 12 |
| 120 | 27 | 2 | 7 | 0 | 120 | 25 | 0 | 0 | 0 | 120 | 22 | 2 | 27 | 0 |

A table to show the weight of Cable Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of 9 inch cable |  |  |  |  | The weight of $81 / 2$ inch cable |  |  |  |  | The weight of 8 inch cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 18 | 4 | 1 | 0 | 0 | 16 | 13 | 1 | 0 | 0 | 14 | 14 |
| 5 | 0 | 3 | 16 | 8 | 5 | 0 | 3 | 0 | 5 | 5 | 0 | 2 | 18 | 11 |
| 10 | 1 | 2 | 21 | 0 | 10 | 1 | 2 | 0 | 10 | 10 | 1 | 1 | 9 | 6 |
| 15 | 2 | 2 | 3 | 8 | 15 | 2 | 1 | 0 | 14 | 15 | 2 | 0 | 0 | 0 |
| 20 | 3 | 1 | 14 | 0 | 20 | 3 | 0 | 1 | 3 | 20 | 2 | 2 | 18 | 11 |
| 25 | 4 | 0 | 24 | 8 | 25 | 3 | 3 | 1 | 8 | 25 | 3 | 1 | 9 | 6 |
| 30 | 5 | 0 | 7 | 0 | 30 | 4 | 2 | 1 | 12 | 30 | 4 | 0 | 0 | 0 |
| 35 | 5 | 3 | 17 | 8 | 35 | 5 | 1 | 2 | 1 | 35 | 4 | 2 | 18 | 11 |
| 40 | 6 | 3 | 0 | 0 | 40 | 6 | 0 | 2 | 6 | 40 | 5 | 1 | 9 | 6 |
| 45 | 7 | 2 | 10 | 8 | 45 | 6 | 3 | 2 | 10 | 45 | 6 | 0 | 0 | 0 |
| 50 | 8 | 1 | 21 | 0 | 50 | 7 | 2 | 2 | 15 | 50 | 6 | 2 | 18 | 11 |
| 55 | 9 | 1 | 7 | 8 | 55 | 8 | 1 | 3 | 4 | 55 | 7 | 1 | 9 | 6 |
| 60 | 10 | 0 | 14 | 0 | 60 | 9 | 0 | 3 | 8 | 60 | 8 | 0 | 0 | 0 |
| 65 | 10 | 3 | 21 | 8 | 65 | 9 | 3 | 3 | 13 | 65 | 8 | 2 | 18 | 11 |
| 70 | 11 | 3 | 7 | 0 | 70 | 10 | 2 | 4 | 2 | 70 | 9 | 1 | 9 | 6 |
| 75 | 12 | 2 | 17 | 8 | 75 | 11 | 1 | 4 | 6 | 75 | 10 | 0 | 0 | 0 |
| 80 | 13 | 2 | 0 | 0 | 80 | 12 | 0 | 4 | 11 | 80 | 10 | 2 | 18 | 11 |
| 85 | 14 | 1 | 10 | 8 | 85 | 12 | 3 | 5 | 0 | 85 | 11 | 1 | 9 | 6 |
| 90 | 15 | 0 | 21 | 0 | 90 | 13 | 2 | 5 | 4 | 90 | 12 | 0 | 0 | 0 |
| 95 | 16 | 0 | 3 | 8 | 95 | 14 | 1 | 5 | 0 | 95 | 12 | 2 | 18 | 11 |
| 100 | 16 | 3 | 14 | 0 | 100 | 15 | 0 | 5 | 14 | 100 | 13 | 1 | 9 | 6 |
| 105 | 17 | 2 | 24 | 8 | 105 | 15 | 3 | 6 | 2 | 105 | 14 | 0 | 0 | 0 |
| 110 | 18 | 2 | 7 | 0 | 110 | 16 | 2 | 6 | 7 | 110 | 14 | 2 | 18 | 11 |
| 115 | 19 | 1 | 17 | 8 | 115 | 17 | 1 | 6 | 12 | 115 | 15 | 1 | 9 | 6 |
| 120 | 20 | 1 | 0 | 0 | 120 | 18 | 0 | 7 | 0 | 120 | 16 | 0 | 0 | 0 |

A table to show the weight of Cable Lay'd
Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of $71 / 2$ inch cable |  |  |  |  | The weight of 7 in cable |  |  |  |  | The weight of $61 / 2$ in cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 13 | 2 | 1 | 0 | 0 | 11 | 7 | 1 | 0 | 0 | 9 | 14 |
| 5 | 0 | 2 | 9 | 10 | 5 | 0 | 2 | 1 | 3 | 5 | 0 | 1 | 21 | 5 |
| 10 | 1 | 0 | 19 | 4 | 10 | 1 | 0 | 2 | 6 | 10 | 0 | 3 | 14 | 10 |
| 15 | 1 | 3 | 0 | 14 | 15 | 1 | 2 | 3 | 8 | 15 | 1 | 1 | 7 | 14 |
| 20 | 2 | 1 | 10 | 8 | 20 | 2 | 0 | 4 | 11 | 20 | 1 | 3 | 1 | 3 |
| 25 | 2 | 3 | 20 | 2 | 25 | 2 | 2 | 5 | 14 | 25 | 2 | 0 | 22 | 8 |
| 30 | 3 | 2 | 1 | 12 | 30 | 3 | 0 | 7 | 0 | 30 | 2 | 2 | 15 | 12 |
| 35 | 4 | 0 | 11 | 6 | 35 | 3 | 2 | 8 | 3 | 35 | 3 | 0 | 9 | 1 |
| 40 | 4 | 2 | 21 | 0 | 40 | 4 | 0 | 9 | 6 | 40 | 3 | 2 | 2 | 6 |
| 45 | 5 | 1 | 2 | 10 | 45 | 4 | 2 | 10 | 8 | 45 | 3 | 3 | 2 | 10 |
| 50 | 5 | 3 | 12 | 4 | 50 | 5 | 0 | 11 | 11 | 50 | 4 | 1 | 16 | 5 |
| 55 | 6 | 1 | 21 | 14 | 55 | 5 | 2 | 12 | 14 | 55 | 4 | 3 | 10 | 4 |
| 60 | 7 | 0 | 3 | 8 | 60 | 6 | 0 | 14 | 0 | 60 | 5 | 1 | 8 | 8 |
| 65 | 7 | 2 | 13 | 2 | 65 | 6 | 2 | 15 | 3 | 65 | 5 | 2 | 24 | 18 |
| 70 | 8 | 0 | 22 | 12 | 70 | 7 | 0 | 16 | 16 | 70 | 6 | 8 | 18 | 2 |
| 75 | 8 | 3 | 4 | 6 | 75 | 7 | 2 | 17 | 8 | 75 | 6 | 2 | 11 | 7 |
| 80 | 9 | 1 | 14 | 0 | 80 | 8 | 0 | 18 | 11 | 80 | 7 | 0 | 4 | 11 |
| 85 | 9 | 3 | 23 | 10 | 85 | 8 | 2 | 11 | 14 | 85 | 7 | 1 | 25 | 15 |
| 90 | 10 | 2 | 5 | 4 | 90 | 9 | 0 | 21 | 0 | 90 | 7 | 3 | 19 | 4 |
| 95 | 11 | 0 | 14 | 14 | 95 | 9 | 2 | 22 | 3 | 95 | 8 | 1 | 12 | 9 |
| 100 | 11 | 2 | 24 | 8 | 100 | 10 | 0 | 23 | 16 | 100 | 8 | 3 | 5 | 14 |
| 105 | 12 | 1 | 6 | 2 | 105 | 10 | 2 | 24 | 8 | 105 | 9 | 0 | 27 | 2 |
| 110 | 12 | 3 | 15 | 12 | 110 | 11 | 0 | 0 | 11 | 110 | 9 | 2 | 20 | 7 |
| 115 | 13 | 1 | 25 | 6 | 115 | 11 | 2 | 26 | 14 | 115 | 10 | 0 | 13 | 12 |
| 120 | 14 | 0 | 7 | 0 | 120 | 12 | 1 | 0 | 0 | 120 | 10 | 2 | 7 | 0 |

A table to show the weight of Cable Lay'd
Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of 6 inch cable |  |  |  |  | The weight of $51 / 2$ inch cable |  |  |  |  | The weight of 5 inch cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 8 | 6 | 1 | 0 | 0 | 7 | 1 | 1 | 0 | 0 | 5 | 13 |
| 5 | 0 | 1 | 14 | 0 | 5 | 0 | 1 | 7 | 5 | 5 | 0 | 1 | 1 | 3 |
| 10 | 0 | 3 | 0 | 0 | 10 | 0 | 2 | 14 | 10 | 10 | 0 | 2 | 2 | 6 |
| 15 | 1 | 0 | 14 | 0 | 15 | 0 | 3 | 21 | 14 | 15 | 0 | 3 | 3 | 8 |
| 20 | 1 | 2 | 0 | 0 | 20 | 1 | 1 | 1 | 3 | 20 | 1 | 0 | 4 | 11 |
| 25 | 1 | 3 | 14 | 0 | 25 | 1 | 2 | 8 | 8 | 25 | 1 | 1 | 5 | 14 |
| 30 | 2 | 1 | 0 | 0 | 30 | 1 | 3 | 15 | 12 | 30 | 1 | 2 | 7 | 0 |
| 35 | 2 | 2 | 14 | 0 | 35 | 2 | 0 | 23 | 0 | 35 | 1 | 3 | 8 | 3 |
| 40 | 3 | 0 | 0 | 0 | 40 | 2 | 2 | 2 | 5 | 40 | 2 | 0 | 9 | 6 |
| 45 | 3 | 1 | 14 | 0 | 45 | 2 | 3 | 9 | 10 | 45 | 2 | 1 | 10 | 8 |
| 50 | 3 | 3 | 0 | 0 | 50 | 3 | 0 | 16 | 5 | 50 | 2 | 2 | 11 | 11 |
| 55 | 4 | 0 | 14 | 0 | 55 | 3 | 1 | 23 | 8 | 55 | 2 | 3 | 12 | 14 |
| 60 | 4 | 2 | 0 | 0 | 60 | 3 | 3 | 2 | 8 | 60 | 3 | 0 | 14 | 0 |
| 65 | 4 | 3 | 14 | 0 | 65 | 4 | 0 | 10 | 13 | 65 | 3 | 1 | 15 | 3 |
| 70 | 5 | 1 | 0 | 0 | 70 | 4 | 1 | 18 | 2 | 70 | 3 | 2 | 16 | 6 |
| 75 | 5 | 2 | 14 | 0 | 75 | 4 | 2 | 25 | 0 | 75 | 3 | 3 | 17 | 8 |
| 80 | 6 | 0 | 0 | 0 | 80 | 5 | 0 | 4 | 11 | 80 | 4 | 0 | 18 | 11 |
| 85 | 6 | 1 | 14 | 0 | 85 | 5 | 1 | 12 | 0 | 85 | 4 | 1 | 19 | 14 |
| 90 | 6 | 3 | 0 | 0 | 90 | 5 | 2 | 19 | 5 | 90 | 4 | 2 | 21 | 0 |
| 95 | 7 | 0 | 14 | 0 | 95 | 5 | 3 | 26 | 10 | 95 | 4 | 3 | 22 | 3 |
| 100 | 7 | 2 | 0 | 0 | 100 | 6 | 1 | 5 | 14 | 100 | 5 | 0 | 23 | 6 |
| 105 | 7 | 3 | 14 | 0 | 105 | 6 | 2 | 13 | 3 | 105 | 5 | 1 | 24 | 8 |
| 110 | 8 | 1 | 0 | 0 | 110 | 6 | 3 | 20 | 8 | 110 | 5 | 2 | 25 | 11 |
| 115 | 8 | 2 | 14 | 0 | 115 | 7 | 0 | 27 | 12 | 115 | 5 | 3 | 26 | 14 |
| 120 | 9 | 0 | 0 | 0 | 120 | 7 | 2 | 7 | 0 | 120 | 6 | 1 | 0 | 0 |

A table to show the weight of Cable Lay'd
Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of $41 / 2$ inch cable |  |  |  |  | The weight of 4 in cable |  |  |  |  | The weight of $31 / 2$ in cable |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 4 | 11 | 1 | 0 | 0 | 3 | 11 | 1 | 0 | 0 | 2 | 15 |
| 5 | 0 | 0 | 23 | 10 | 5 | 0 | 0 | 18 | 11 | 5 | 0 | 0 | 14 | 5 |
| 10 | 0 | 1 | 19 | 4 | 10 | 0 | 1 | 9 | 6 | 10 | 0 | 1 | 0 | 10 |
| 15 | 0 | 2 | 14 | 14 | 15 | 0 | 2 | 0 | 0 | 15 | 0 | 1 | 14 | 14 |
| 20 | 0 | 3 | 10 | 8 | 20 | 0 | 2 | 18 | 11 | 20 | 0 | 2 | 1 | 3 |
| 25 | 1 | 0 | 6 | 2 | 25 | 0 | 3 | 9 | 6 | 25 | 0 | 2 | 15 | 8 |
| 30 | 1 | 1 | 1 | 12 | 30 | 1 | 0 | 0 | 0 | 30 | 0 | 3 | 1 | 12 |
| 35 | 1 | 1 | 25 | 6 | 35 | 1 | 0 | 18 | 11 | 35 | 0 | 3 | 16 | 1 |
| 40 | 1 | 2 | 21 | 0 | 40 | 1 | 1 | 9 | 6 | 40 | 1 | 0 | 2 | 6 |
| 45 | 1 | 3 | 16 | 10 | 45 | 1 | 2 | 0 | 0 | 45 | 1 | 0 | 16 | 10 |
| 50 | 2 | 0 | 12 | 4 | 50 | 1 | 2 | 18 | 11 | 50 | 1 | 1 | 2 | 14 |
| 55 | 2 | 1 | 7 | 14 | 55 | 1 | 3 | 9 | 6 | 55 | 1 | 1 | 17 | 3 |
| 60 | 2 | 2 | 3 | 8 | 60 | 2 | 0 | 0 | 0 | 60 | 1 | 2 | 8 | 8 |
| 65 | 2 | 2 | 27 | 2 | 65 | 2 | 0 | 18 | 11 | 65 | 1 | 2 | 17 | 12 |
| 70 | 2 | 3 | 22 | 12 | 70 | 2 | 1 | 9 | 6 | 70 | 1 | 3 | 4 | 1 |
| 75 | 3 | 0 | 18 | 6 | 75 | 2 | 2 | 0 | 0 | 75 | 1 | 3 | 18 | 6 |
| 80 | 3 | 1 | 14 | 0 | 80 | 2 | 2 | 18 | 11 | 80 | 2 | 0 | 5 | 10 |
| 85 | 3 | 2 | 9 | 10 | 85 | 2 | 3 | 9 | 6 | 85 | 2 | 0 | 18 | 15 |
| 90 | 3 | 3 | 5 | 4 | 90 | 3 | 0 | 0 | 0 | 90 | 2 | 1 | 5 | 4 |
| 95 | 4 | 0 | 0 | 14 | 95 | 3 | 0 | 18 | 11 | 95 | 2 | 1 | 19 | 9 |
| 100 | 4 | 0 | 24 | 8 | 100 | 3 | 1 | 9 | 6 | 100 | 2 | 2 | 6 | 4 |
| 105 | 4 | 1 | 20 | 2 | 105 | 3 | 2 | 0 | 0 | 105 | 2 | 2 | 20 | 3 |
| 110 | 4 | 2 | 15 | 12 | 110 | 3 | 2 | 18 | 11 | 110 | 2 | 3 | 6 | 8 |
| 115 | 4 | 3 | 11 | 6 | 115 | 3 | 3 | 9 | 6 | 115 | 2 | 3 | 20 | 12 |
| 120 | 5 | 0 | 7 | 0 | 120 | 4 | 0 | 0 | 0 | 120 | 3 | 0 | 7 | 0 |


| A table to show the weight of Cable Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| The weight of 4 inch cable |  |  |  |  |
| Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 2 | 2 |
| 5 | 0 | 0 | 10 | 5 |
| 10 | 0 | 0 | 21 | 0 |
| 15 | 0 | 1 | 3 | 8 |
| 20 | 0 | 1 | 14 | 0 |
| 25 | 0 | 1 | 24 | 8 |
| 30 | 0 | 2 | 7 | 0 |
| 35 | 0 | 2 | 17 | 8 |
| 40 | 0 | 3 | 0 | 0 |
| 45 | 0 | 3 | 10 | 8 |
| 50 | 0 | 3 | 21 | 0 |
| 55 | 1 | 0 | 3 | 8 |
| 60 | 1 | 0 | 14 | 0 |
| 65 | 1 | 0 | 24 | 8 |
| 70 | 1 | 1 | 7 | 0 |
| 75 | 1 | 1 | 17 | 8 |
| 80 | 1 | 2 | 0 | 0 |
| 85 | 1 | 2 | 10 | 8 |
| 90 | 1 | 2 | 21 | 0 |
| 95 | 1 | 3 | 3 | 8 |
| 100 | 1 | 3 | 14 | 0 |
| 105 | 1 | 3 | 24 | 8 |
| 110 | 2 | 0 | 7 | 0 |
| 115 | 2 | 0 | 17 | 8 |
| 120 | 2 | 1 | 0 | 0 |


| A table to show the weight of Hauser Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| The weight of 9 inch hauser layd rope |  |  |  |  | The weight of $81 / 2$ in Hauser Layd Rope |  |  |  |  | The weight of 8 inch hauser layd rope |  |  |  |  |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 20 | 4 | 1 | 0 | 0 | 17 | 15 | 1 | 0 | 0 | 15 | 14 |
| 5 | 0 | 3 | 17 | 4 | 5 | 0 | 3 | 5 | 14 | 5 | 0 | 0 | 23 | 10 |
| 10 | 1 | 3 | 6 | 8 | 10 | 1 | 2 | 11 | 13 | 10 | 1 | 1 | 19 | 5 |
| 15 | 2 | 2 | 23 | 12 | 15 | 2 | 1 | 17 | 12 | 15 | 2 | 2 | 15 | 0 |
| 20 | 3 | 2 | 13 | 0 | 20 | 3 | 0 | 23 | 11 | 20 | 2 | 2 | 10 | 10 |
| 25 | 4 | 2 | 2 | 41 | 25 | 4 | 0 | 1 | 10 | 25 | 3 | 3 | 6 | 5 |
| 30 | 5 | 1 | 19 | 8 | 30 | 4 | 3 | 7 | 8 | 30 | 4 | 4 | 2 | 0 |
| 35 | 6 | 1 | 8 | 12 | 35 | 5 | 2 | 13 | 7 | 35 | 4 | 4 | 25 | 10 |
| 40 | 7 | 0 | 26 | 0 | 40 | 6 | 1 | 19 | 6 | 40 | 5 | 5 | 21 | 5 |
| 45 | 8 | 0 | 15 | 4 | 45 | 7 | 0 | 25 | 4 | 45 | 6 | 6 | 17 | 0 |
| 50 | 9 | 0 | 4 | 8 | 50 | 8 | 0 | 3 | 2 | 50 | 7 | 7 | 12 | 10 |
| 55 | 9 | 3 | 21 | 12 | 55 | 8 | 3 | 9 | 2 | 55 | 7 | 7 | 8 | 5 |
| 60 | 10 | 3 | 11 | 0 | 60 | 9 | 2 | 25 | 0 | 60 | 8 | 8 | 4 | 0 |
| 65 | 11 | 3 | 0 | 4 | 65 | 1 | 1 | 20 | 15 | 65 | 9 | 9 | 27 | 10 |
| 70 | 12 | 2 | 17 | 8 | 70 | 11 | 0 | 26 | 14 | 70 | 9 | 9 | 23 | 5 |
| 75 | 13 | 2 | 6 | 12 | 75 | 12 | 0 | 4 | 13 | 75 | 10 | 10 | 19 | 0 |
| 80 | 14 | 1 | 24 | 0 | 80 | 12 | 3 | 10 | 12 | 80 | 11 | 11 | 14 | 10 |
| 85 | 15 | 1 | 13 | 4 | 85 | 13 | 2 | 16 | 11 | 85 | 12 | 12 | 10 | 5 |
| 90 | 16 | 1 | 2 | 8 | 90 | 14 | 1 | 22 | 10 | 90 | 12 | 12 | 6 | 0 |
| 95 | 17 | 0 | 19 | 12 | 95 | 15 | 1 | 0 | 8 | 95 | 13 | 13 | 1 | 10 |
| 100 | 18 | 0 | 9 | 0 | 100 | 16 | 0 | 6 | 7 | 100 | 14 | 14 | 25 | 5 |
| 105 | 18 | 3 | 26 | 4 | 105 | 16 | 3 | 12 | 8 | 105 | 14 | 14 | 21 | 0 |
| 110 | 19 | 3 | 15 | 8 | 110 | 17 | 2 | 18 | 4 | 110 | 15 | 15 | 16 | 10 |
| 115 | 20 | 3 | 4 | 12 | 115 | 18 | 1 | 24 | 2 | 115 | 16 | 16 | 12 | 5 |
| 120 | 21 | 2 | 22 | 0 | 120 | 19 | 1 | 2 | 0 | 120 | 17 | 17 | 8 | 0 |


| A table to show the weight of Hauser Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| The weight of $71 / 2$ in Hauser Layd Rope |  |  |  |  | The weight of 7 inch hauser Layd rope |  |  |  |  | The weight of $61 / 2$ in Hauser Layd Rope |  |  |  |  |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 13 | 12 | 1 | 0 | 0 | 12 | 3 | 1 | 0 | 0 | 10 | 6 |
| 5 | 0 | 2 | 13 | 0 | 5 | 0 | 2 | 5 | 0 | 5 | 0 | 1 | 23 | 14 |
| 10 | 1 | 0 | 26 | 0 | 10 | 1 | 0 | 10 | 1 | 10 | 0 | 3 | 19 | 12 |
| 15 | 1 | 3 | 11 | 0 | 15 | 1 | 2 | 15 | 2 | 15 | 1 | 1 | 15 | 10 |
| 20 | 2 | 4 | 24 | 0 | 20 | 2 | 0 | 20 | 2 | 20 | 1 | 3 | 14 | 8 |
| 25 | 3 | 0 | 9 | 0 | 25 | 2 | 2 | 25 | 3 | 25 | 2 | 1 | 7 | 6 |
| 30 | 3 | 2 | 22 | 0 | 30 | 3 | 1 | 2 | 4 | 30 | 2 | 3 | 3 | 4 |
| 35 | 4 | 1 | 7 | 0 | 35 | 3 | 3 | 7 | 4 | 35 | 3 | 0 | 27 | 2 |
| 40 | 4 | 3 | 20 | 0 | 40 | 4 | 1 | 12 | 5 | 40 | 3 | 2 | 23 | 0 |
| 45 | 5 | 2 | 5 | 0 | 45 | 4 | 3 | 17 | 6 | 45 | 4 | 0 | 18 | 14 |
| 50 | 6 | 0 | 18 | 0 | 50 | 5 | 1 | 22 | 6 | 50 | 4 | 2 | 14 | 12 |
| 55 | 6 | 3 | 3 | 0 | 55 | 5 | 3 | 27 | 7 | 55 | 5 | 0 | 10 | 10 |
| 60 | 7 | 1 | 16 | 0 | 60 | 6 | 2 | 4 | 8 | 60 | 5 | 2 | 6 | 8 |
| 65 | 8 | 0 | 1 | 0 | 65 | 7 | 0 | 9 | 9 | 65 | 6 | 0 | 2 | 6 |
| 70 | 8 | 2 | 14 | 0 | 70 | 7 | 2 | 14 | 10 | 70 | 6 | 1 | 26 | 4 |
| 75 | 9 | 0 | 27 | 0 | 75 | 8 | 0 | 19 | 10 | 75 | 6 | 3 | 22 | 2 |
| 80 | 9 | 3 | 12 | 0 | 80 | 8 | 2 | 24 | 11 | 80 | 7 | 1 | 18 | 0 |
| 85 | 10 | 1 | 25 | 0 | 85 | 9 | 1 | 1 | 2 | 85 | 7 | 3 | 13 | 14 |
| 90 | 11 | 1 | 10 | 0 | 90 | 9 | 3 | 6 | 13 | 90 | 8 | 1 | 9 | 12 |
| 95 | 11 | 3 | 23 | 0 | 95 | 10 | 1 | 11 | 13 | 95 | 8 | 3 | 5 | 10 |
| 100 | 12 | 2 | 8 | 0 | 100 | 10 | 3 | 16 | 14 | 100 | 9 | 1 | 1 | 8 |
| 105 | 13 | 0 | 21 | 0 | 105 | 11 | 1 | 21 | 15 | 105 | 9 | 2 | 25 | 6 |
| 110 | 13 | 3 | 6 | 0 | 110 | 11 | 3 | 26 | 15 | 110 | 10 | 0 | 21 | 4 |
| 115 | 14 | 1 | 19 | 0 | 115 | 12 | 2 | 3 | 0 | 115 | 10 | 2 | 17 | 2 |
| 120 | 15 | 0 | 4 | 0 | 120 | 13 | 0 | 9 | 0 | 120 | 11 | 0 | 13 | 0 |

A table to show the weight of Cable Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of 6 inch Rope |  |  |  |  | The weight of $51 / 2$ in Rope |  |  |  |  | The weight of 5 in Rope |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 8 | 14 | 1 | 0 | 0 | 7 | 7 | 1 | 0 | 0 | 6 | 3 |
| 5 | 0 | 1 | 16 | 11 | 5 | 0 | 1 | 9 | 12 | 5 | 0 | 1 | 2 | 3 |
| 10 | 0 | 3 | 5 | 7 | 10 | 0 | 2 | 11 | 7 | 10 | 0 | 2 | 6 | 4 |
| 15 | 1 | 0 | 22 | 2 | 15 | 1 | 0 | 1 | 2 | 15 | 0 | 3 | 9 | 6 |
| 20 | 1 | 2 | 10 | 13 | 20 | 1 | 1 | 10 | 4 | 20 | 1 | 0 | 12 | 8 |
| 25 | 1 | 3 | 27 | 8 | 25 | 1 | 2 | 20 | 9 | 25 | 1 | 1 | 15 | 10 |
| 30 | 2 | 1 | 16 | 4 | 30 | 2 | 0 | 2 | 4 | 30 | 1 | 2 | 18 | 12 |
| 35 | 2 | 3 | 4 | 15 | 35 | 2 | 1 | 12 | 0 | 35 | 1 | 3 | 21 | 4 |
| 40 | 3 | 0 | 21 | 10 | 40 | 2 | 2 | 21 | 11 | 40 | 2 | 0 | 25 | 0 |
| 45 | 3 | 2 | 10 | 6 | 45 | 3 | 0 | 3 | 6 | 45 | 2 | 2 | 0 | 2 |
| 50 | 3 | 3 | 27 | 2 | 50 | 3 | 1 | 13 | 2 | 50 | 2 | 3 | 3 | 4 |
| 55 | 4 | 1 | 15 | 13 | 55 | 3 | 2 | 22 | 13 | 55 | 3 | 0 | 6 | 6 |
| 60 | 4 | 3 | 4 | 8 | 60 | 4 | 0 | 4 | 8 | 60 | 3 | 1 | 9 | 8 |
| 65 | 5 | 0 | 21 | 3 | 65 | 4 | 1 | 14 | 4 | 65 | 3 | 2 | 12 | 10 |
| 70 | 5 | 2 | 9 | 14 | 70 | 4 | 2 | 23 | 15 | 70 | 3 | 3 | 15 | 12 |
| 75 | 5 | 3 | 26 | 10 | 75 | 5 | 0 | 5 | 10 | 75 | 4 | 0 | 18 | 14 |
| 80 | 6 | 1 | 15 | 5 | 80 | 5 | 1 | 15 | 6 | 80 | 4 | 1 | 22 | 0 |
| 85 | 6 | 3 | 4 | 0 | 85 | 5 | 2 | 25 | 1 | 85 | 4 | 2 | 25 | 2 |
| 90 | 7 | 0 | 20 | 12 | 90 | 6 | 0 | 6 | 12 | 90 | 5 | 0 | 0 | 4 |
| 95 | 7 | 2 | 9 | 7 | 95 | 6 | 1 | 16 | 8 | 95 | 5 | 1 | 3 | 6 |
| 100 | 7 | 3 | 26 | 2 | 100 | 6 | 2 | 26 | 3 | 100 | 5 | 2 | 6 | 8 |
| 105 | 8 | 1 | 14 | 14 | 105 | 7 | 0 | 7 | 14 | 105 | 5 | 3 | 9 | 10 |
| 110 | 8 | 3 | 3 | 9 | 110 | 7 | 1 | 17 | 10 | 110 | 6 | 0 | 12 | 12 |
| 115 | 9 | 0 | 20 | 4 | 115 | 7 | 2 | 27 | 5 | 115 | 6 | 1 | 15 | 14 |
| 120 | 9 | 2 | 9 | 0 | 120 | 8 | 0 | 9 | 0 | 120 | 6 | 2 | 19 | 0 |

A table to show the weight of Cable Lay'd
Cordage from 1 to 120 fathoms at every 5 fathoms

| The weight of $41 / 2$ inch Rope |  |  |  |  | The weight of 4 inch Rope |  |  |  |  | The weight of $31 / 2$ inch Rope |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 5 | 1 | 1 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 3 | 1 |
| 5 | 0 | 0 | 25 | 5 | 5 | 0 | 0 | 19 | 15 | 5 | 0 | 0 | 15 | 4 |
| 10 | 0 | 1 | 22 | 10 | 10 | 0 | 1 | 11 | 14 | 10 | 0 | 1 | 2 | 8 |
| 15 | 0 | 2 | 19 | 14 | 15 | 0 | 2 | 3 | 12 | 15 | 0 | 1 | 17 | 12 |
| 20 | 0 | 3 | 17 | 3 | 20 | 0 | 2 | 23 | 11 | 20 | 0 | 2 | 5 | 0 |
| 25 | 1 | 0 | 14 | 8 | 25 | 0 | 3 | 15 | 10 | 25 | 0 | 2 | 20 | 4 |
| 30 | 1 | 1 | 11 | 12 | 30 | 1 | 0 | 7 | 8 | 30 | 0 | 3 | 7 | 8 |
| 35 | 1 | 2 | 9 | 1 | 35 | 1 | 0 | 27 | 7 | 35 | 0 | 3 | 22 | 12 |
| 40 | 1 | 3 | 6 | 6 | 40 | 1 | 1 | 9 | 6 | 40 | 1 | 0 | 10 | 0 |
| 45 | 2 | 0 | 3 | 10 | 45 | 1 | 2 | 11 | 4 | 45 | 1 | 0 | 25 | 4 |
| 50 | 2 | 1 | 0 | 14 | 50 | 1 | 3 | 3 | 3 | 50 | 1 | 1 | 12 | 8 |
| 55 | 2 | 1 | 26 | 3 | 55 | 1 | 3 | 23 | 2 | 55 | 1 | 1 | 25 | 12 |
| 60 | 2 | 2 | 23 | 8 | 60 | 2 | 0 | 15 | 0 | 60 | 1 | 2 | 15 | 0 |
| 65 | 2 | 3 | 20 | 12 | 65 | 2 | 1 | 6 | 15 | 65 | 1 | 3 | 2 | 4 |
| 70 | 3 | 0 | 18 | 1 | 70 | 2 | 1 | 26 | 14 | 70 | 1 | 3 | 17 | 8 |
| 75 | 3 | 1 | 15 | 96 | 75 | 2 | 1 | 18 | 12 | 75 | 2 | 0 | 4 | 12 |
| 80 | 3 | 2 | 12 | 10 | 80 | 2 | 3 | 10 | 11 | 80 | 2 | 0 | 20 | 0 |
| 85 | 3 | 3 | 10 | 14 | 85 | 3 | 0 | 2 | 10 | 85 | 2 | 1 | 7 | 4 |
| 90 | 4 | 0 | 7 | 11 | 90 | 3 | 0 | 22 | 8 | 90 | 2 | 1 | 22 | 8 |
| 95 | 4 | 1 | 4 | 9 | 95 | 3 | 1 | 14 | 7 | 95 | 2 | 2 | 9 | 12 |
| 100 | 4 | 2 | 1 | 14 | 100 | 3 | 2 | 6 | 6 | 100 | 2 | 2 | 25 | 0 |
| 105 | 4 | 2 | 27 | 3 | 105 | 3 | 2 | 26 | 4 | 105 | 2 | 3 | 12 | 4 |
| 110 | 4 | 3 | 24 | 7 | 110 | 3 | 3 | 18 | 3 | 110 | 2 | 3 | 27 | 8 |
| 115 | 5 | 0 | 21 | 12 | 115 | 4 | 0 | 10 | 2 | 115 | 3 | 0 | 14 | 12 |
| 120 | 5 | 1 | 19 | 0 | 120 | 4 | 1 | 2 | 0 | 120 | 3 | 1 | 2 | 0 |


| A table to show the weight of Hauser Lay'd Cordage from 1 to 120 fathoms at every 5 fathoms |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| The weight of 3 inch hauser layd rope |  |  |  |  | The weight of $2^{1} / 2$ in hauser layd rope |  |  |  |  | The weight of $21 / 4$ in hauser layd rope |  |  |  |  |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 2 | 4 | 1 | 0 | 0 | 1 | 9 | 1 | 0 | 0 | 1 | 4 |
| 5 | 0 | 0 | 11 | 3 | 5 | 0 | 0 | 7 | 13 | 5 | 0 | 0 | 6 | 5 |
| 10 | 0 | 0 | 22 | 6 | 10 | 0 | 0 | 15 | 10 | 10 | 0 | 0 | 12 | 10 |
| 15 | 0 | 1 | 5 | 8 | 15 | 0 | 0 | 23 | 6 | 15 | 0 | 0 | 19 | 0 |
| 20 | 0 | 1 | 16 | 11 | 20 | 0 | 1 | 3 | 3 | 20 | 0 | 0 | 25 | 5 |
| 25 | 0 | 1 | 27 | 14 | 25 | 0 | 1 | 11 | 0 | 25 | 0 | 1 | 3 | 10 |
| 30 | 0 | 2 | 11 | 0 | 30 | 0 | 1 | 18 | 12 | 30 | 0 | 1 | 10 | 0 |
| 35 | 0 | 2 | 22 | 3 | 35 | 0 | 1 | 26 | 9 | 35 | 0 | 1 | 16 | 5 |
| 40 | 0 | 3 | 5 | 6 | 40 | 0 | 2 | 6 | 6 | 40 | 0 | 1 | 22 | 10 |
| 45 | 0 | 3 | 16 | 8 | 45 | 0 | 2 | 14 | 2 | 45 | 0 | 2 | 1 | 0 |
| 50 | 0 | 3 | 27 | 11 | 50 | 0 | 2 | 21 | 5 | 50 | 0 | 2 | 7 | 5 |
| 55 | 1 | 0 | 10 | 14 | 55 | 0 | 3 | 1 | 12 | 55 | 0 | 2 | 13 | 10 |
| 60 | 1 | 0 | 22 | 0 | 60 | 0 | 3 | 9 | 8 | 60 | 0 | 2 | 20 | 0 |
| 65 | 1 | 1 | 5 | 3 | 65 | 0 | 3 | 17 | 5 | 65 | 0 | 2 | 26 | 5 |
| 70 | 1 | 1 | 16 | 6 | 70 | 0 | 3 | 25 | 2 | 70 | 0 | 3 | 4 | 10 |
| 75 | 1 | 1 | 27 | 8 | 75 | 1 | 0 | 4 | 14 | 75 | 0 | 3 | 11 | 0 |
| 80 | 1 | 2 | 10 | 11 | 80 | 1 | 0 | 12 | 11 | 80 | 0 | 3 | 17 | 5 |
| 85 | 1 | 2 | 21 | 14 | 85 | 1 | 0 | 20 | 8 | 85 | 0 | 3 | 23 | 10 |
| 90 | 1 | 3 | 5 | 0 | 90 | 1 | 1 | 0 | 4 | 90 | 1 | 0 | 2 | 0 |
| 95 | 1 | 3 | 16 | 3 | 95 | 1 | 1 | 8 | 1 | 95 | 1 | 0 | 8 | 5 |
| 100 | 1 | 3 | 27 | 6 | 100 | 1 | 1 | 18 | 14 | 100 | 1 | 0 | 14 | 10 |
| 105 | 2 | 0 | 10 | 8 | 105 | 1 | 1 | 23 | 10 | 105 | 1 | 0 | 21 | 0 |
| 110 | 2 | 0 | 21 | 11 | 110 | 1 | 2 | 3 | 9 | 110 | 1 | 0 | 27 | 5 |
| 115 | 2 | 1 | 4 | 14 | 115 | 1 | 2 | 11 | 5 | 115 | 1 | 1 | 5 | 10 |
| 120 | 2 | 1 | 16 | 0 | 120 | 1 | 2 | 19 | 0 | 120 | 1 | 1 | 12 | 0 |


| A table for 8 thread hook hauser lay'd |  |  |  |  | A table for 7 thread hook Hauser lay'd |  |  |  |  | A table for 6 thread hook hauser lay'd |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz | Fath | Ct | Qr | Lb | Oz |
| 1 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 15 | 1 | 0 | 0 | 0 | 13 |
| 5 | 0 | 0 | 5 | 11 | 5 | 0 | 0 | 4 | 15 | 5 | 0 | 0 | 4 | 4 |
| 10 | 0 | 0 | 11 | 6 | 10 | 0 | 0 | 9 | 14 | 10 | 0 | 0 | 8 | 7 |
| 15 | 0 | 0 | 17 | 0 | 15 | 0 | 0 | 14 | 12 | 15 | 0 | 0 | 12 | 10 |
| 20 | 0 | 0 | 22 | 11 | 20 | 0 | 0 | 19 | 11 | 20 | 0 | 0 | 16 | 17 |
| 25 | 0 | 1 | 0 | 6 | 25 | 0 | 0 | 24 | 10 | 25 | 0 | 0 | 21 | 1 |
| 30 | 0 | 1 | 6 | 0 | 30 | 0 | 1 | 1 | 8 | 30 | 0 | 0 | 25 | 4 |
| 35 | 0 | 1 | 11 | 11 | 35 | 0 | 1 | 6 | 7 | 35 | 0 | 1 | 1 | 8 |
| 40 | 0 | 1 | 17 | 6 | 40 | 0 | 1 | 11 | 6 | 40 | 0 | 1 | 5 | 12 |
| 45 | 0 | 1 | 23 | 0 | 45 | 0 | 1 | 16 | 4 | 45 | 0 | 1 | 9 | 15 |
| 50 | 0 | 2 | 1 | 11 | 50 | 0 | 1 | 21 | 3 | 50 | 0 | 1 | 14 | 2 |
| 55 | 0 | 2 | 6 | 6 | 55 | 0 | 1 | 26 | 2 | 55 | 0 | 1 | 18 | 15 |
| 60 | 0 | 2 | 12 | 0 | 60 | 0 | 2 | 3 | 0 | 60 | 0 | 1 | 22 | 8 |
| 65 | 0 | 2 | 17 | 11 | 65 | 0 | 2 | 7 | 15 | 65 | 0 | 1 | 26 | 12 |
| 70 | 0 | 2 | 23 | 6 | 70 | 0 | 2 | 12 | 14 | 70 | 0 | 2 | 2 | 15 |
| 75 | 0 | 3 | 1 | 0 | 75 | 0 | 2 | 17 | 12 | 75 | 0 | 2 | 7 | 2 |
| 80 | 0 | 3 | 6 | 11 | 80 | 0 | 2 | 22 | 11 | 80 | 0 | 2 | 11 | 6 |
| 85 | 0 | 3 | 12 | 6 | 85 | 0 | 2 | 27 | 10 | 85 | 0 | 2 | 15 | 9 |
| 90 | 0 | 3 | 18 | 0 | 90 | 0 | 3 | 4 | 8 | 90 | 0 | 2 | 19 | 12 |
| 95 | 0 | 3 | 23 | 11 | 95 | 0 | 3 | 9 | 7 | 95 | 0 | 2 | 23 | 15 |
| 100 | 1 | 0 | 1 | 6 | 100 | 0 | 3 | 14 | 6 | 100 | 0 | 3 | 2 | 0 |
| 105 | 1 | 0 | 7 | 0 | 105 | 0 | 3 | 19 | 4 | 105 | 0 | 3 | 4 | 6 |
| 110 | 1 | 0 | 12 | 11 | 110 | 0 | 3 | 24 | 3 | 110 | 0 | 3 | 8 | 9 |
| 115 | 1 | 0 | 18 | 6 | 115 | 1 | 0 | 1 | 2 | 115 | 0 | 3 | 12 | 12 |
| 120 | 1 | 0 | 24 | 0 | 120 | 1 | 0 | 6 | 0 | 120 | 0 | 3 | 17 | 0 |


| A Table for 5 Thread a Hook Hauser Lay'd |  |  |  |  | A Table for 4 Thread a Hook Hauser Lay'd |  |  |  |  | A Table for 3 Thread a Hook Hauser Lay'd |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qt | Lb | Oz | Fath | Ct | Qt | Lb | Oz | Fath | Ct | Qt | Lb | Oz |
| 1 | 0 | 0 | 0 | 11 | 1 | 0 | 0 | 0 | 9 | 1 | 0 | 0 | 0 | 6 |
| 5 | 0 | 0 | 3 | 8 | 5 | 0 | 0 | 2 | 13 | 5 | 0 | 0 | 2 | 2 |
| 10 | 0 | 0 | 7 | 0 | 10 | 0 | 0 | 5 | 10 | 10 | 0 | 0 | 4 | 4 |
| 15 | 0 | 0 | 10 | 8 | 15 | 0 | 0 | 8 | 6 | 15 | 0 | 0 | 6 | 6 |
| 20 | 0 | 0 | 14 | 0 | 20 | 0 | 0 | 11 | 3 | 20 | 0 | 0 | 8 | 8 |
| 25 | 0 | 0 | 17 | 8 | 25 | 0 | 0 | 14 | 0 | 25 | 0 | 0 | 10 | 10 |
| 30 | 0 | 0 | 21 | 0 | 30 | 0 | 0 | 16 | 12 | 30 | 0 | 0 | 12 | 12 |
| 35 | 0 | 0 | 24 | 8 | 35 | 0 | 0 | 19 | 9 | 35 | 0 | 0 | 14 | 14 |
| 40 | 0 | 1 | 0 | 0 | 40 | 0 | 0 | 22 | 6 | 40 | 0 | 0 | 17 | 0 |
| 45 | 0 | 1 | 3 | 8 | 45 | 0 | 0 | 25 | 2 | 45 | 0 | 0 | 19 | 2 |
| 50 | 0 | 1 | 7 | 0 | 50 | 0 | 0 | 27 | 15 | 50 | 0 | 0 | 21 | 4 |
| 55 | 0 | 1 | 10 | 8 | 55 | 0 | 1 | 2 | 12 | 55 | 0 | 0 | 23 | 6 |
| 60 | 0 | 1 | 14 | 0 | 60 | 0 | 1 | 5 | 8 | 60 | 0 | 0 | 25 | 8 |
| 65 | 0 | 1 | 17 | 8 | 65 | 0 | 1 | 8 | 5 | 65 | 0 | 0 | 27 | 10 |
| 70 | 0 | 1 | 21 | 0 | 70 | 0 | 1 | 11 | 2 | 70 | 0 | 1 | 1 | 12 |
| 75 | 0 | 1 | 24 | 8 | 75 | 0 | 1 | 13 | 14 | 75 | 0 | 1 | 3 | 14 |
| 80 | 0 | 2 | 0 | 0 | 80 | 0 | 1 | 16 | 11 | 80 | 0 | 1 | 6 | 0 |
| 85 | 0 | 2 | 3 | 8 | 85 | 0 | 1 | 9 | 8 | 85 | 0 | 1 | 8 | 2 |
| 90 | 0 | 2 | 7 | 0 | 90 | 0 | 1 | 22 | 4 | 90 | 0 | 1 | 10 | 4 |
| 95 | 0 | 2 | 10 | 8 | 95 | 0 | 1 | 25 | 1 | 95 | 0 | 1 | 12 | 6 |
| 100 | 0 | 2 | 14 | 0 | 100 | 0 | 1 | 27 | 13 | 100 | 0 | 1 | 14 | 8 |
| 105 | 0 | 2 | 17 | 8 | 105 | 0 | 2 | 2 | 10 | 105 | 0 | 1 | 16 | 10 |
| 110 | 0 | 2 | 21 | 0 | 110 | 0 | 2 | 5 | 6 | 110 | 0 | 1 | 18 | 12 |
| 115 | 0 | 2 | 24 | 8 | 115 | 0 | 2 | 8 | 1 | 115 | 0 | 1 | 20 | 14 |
| 120 | 0 | 3 | 0 | 0 | 120 | 0 | 2 | 11 | 0 | 120 | 0 | 1 | 23 | 0 |


| A Table for 2 Thread a hook hauser lay'd |  |  |  |  | A Table of How many Fathoms \& Feet of Yarn will make Fathoms of cable lay'd Cordage |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Qt | Lb | Oz | Fath | Feet | Fath | Fath | Feet | Fath | Fath | Feet | Fath |
| 1 | 0 | 0 | 0 | 5 | 1 | 4 | 1 | 43 | 2 | 26 | 85 | 0 | 51 |
| 5 | 0 | 0 | 1 | 7 | 3 | 2 | 2 | 45 | 0 | 27 | 86 | 4 | 52 |
| 10 | 0 | 0 | 2 | 14 | 5 | 0 | 3 | 46 | 4 | 28 | 88 | 2 | 53 |
| 15 | 0 | 0 | 4 | 4 | 6 | 4 | 4 | 48 | 2 | 29 | 90 | 0 | 54 |
| 20 | 0 | 0 | 5 | 11 | 8 | 2 | 5 | 50 | 0 | 30 | 91 | 4 | 55 |
| 25 | 0 | 0 | 7 | 2 | 10 | 0 | 6 | 51 | 4 | 31 | 93 | 2 | 56 |
| 30 | 0 | 0 | 8 | 8 | 11 | 4 | 7 | 53 | 2 | 32 | 95 | 0 | 57 |
| 35 | 0 | 0 | 9 | 15 | 13 | 2 | 8 | 55 | 0 | 33 | 96 | 4 | 58 |
| 40 | 0 | 0 | 11 | 6 | 15 | 0 | 9 | 56 | 4 | 34 | 98 | 2 | 59 |
| 45 | 0 | 0 | 12 | 12 | 16 | 4 | 10 | 58 | 2 | 35 | 100 | 0 | 60 |
| 50 | 0 | 0 | 14 | 13 | 18 | 2 | 11 | 60 | 0 | 36 | 101 | 4 | 61 |
| 55 | 0 | 0 | 15 | 10 | 20 | 0 | 12 | 61 | 4 | 37 | 103 | 2 | 62 |
| 60 | 0 | 0 | 17 | 0 | 21 | 4 | 13 | 63 | 2 | 38 | 105 | 0 | 63 |
| 65 | 0 | 0 | 18 | 7 | 23 | 2 | 14 | 65 | 0 | 39 | 106 | 4 | 64 |
| 70 | 0 | 0 | 19 | 14 | 25 | 0 | 15 | 66 | 4 | 40 | 108 | 2 | 65 |
| 75 | 0 | 0 | 21 | 4 | 26 | 4 | 16 | 68 | 2 | 41 | 110 | 0 | 66 |
| 80 | 0 | 0 | 22 | 11 | 28 | 2 | 17 | 70 | 0 | 42 | 111 | 4 | 67 |
| 85 | 0 | 0 | 24 | 2 | 30 | 0 | 18 | 71 | 4 | 43 | 113 | 2 | 68 |
| 90 | 0 | 0 | 25 | 8 | 31 | 4 | 19 | 73 | 2 | 44 | 115 | 0 | 69 |
| 95 | 0 | 0 | 26 | 15 | 32 | 2 | 20 | 75 | 0 | 45 | 116 | 4 | 70 |
| 100 | 0 | 1 | 0 | 6 | 35 | 0 | 21 | 76 | 4 | 46 | 118 | 2 | 71 |
| 105 | 0 | 1 | 2 | 12 | 36 | 4 | 22 | 78 | 2 | 47 | 120 | 0 | 72 |
| 110 | 0 | 1 | 3 | 3 | 38 | 2 | 23 | 80 | 0 | 48 | 121 | 4 | 73 |
| 115 | 0 | 1 | 4 | 10 | 40 | 0 | 24 | 81 | 4 | 49 | 123 | 2 | 74 |
| 120 | 0 | 1 | 6 | 0 | 41 | 4 | 25 | 83 | 2 | 50 | 125 | 0 | 75 |


| A Table of How Many Fathoms \& Feet of Yarn will make fathom of cable Lay'd Rope |  |  |  |  |  | A Table of How Many Fathoms \& Feet of Yarn will make Fathoms of Hauser Lay'd Rope |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Ct | Fath | Fath | Ct | Fath | Fath | Feet | Fath | Fath | Feet | Fath | Fath | Ct | Fath |
| 126 | 4 | 76 | 173 | 2 | 104 | 1 | 3 | 1 | 39 | 0 | 26 | 76 | 3 | 51 |
| 128 | 2 | 77 | 175 | 0 | 105 | 3 | 0 | 2 | 40 | 3 | 27 | 78 | 0 | 52 |
| 130 | 0 | 78 | 176 | 4 | 106 | 4 | 3 | 3 | 42 | 0 | 28 | 79 | 3 | 53 |
| 131 | 4 | 79 | 178 | 2 | 107 | 6 | 0 | 4 | 43 | 3 | 29 | 81 | 0 | 54 |
| 133 | 2 | 83 | 180 | 0 | 108 | 7 | 3 | 5 | 45 | 0 | 30 | 82 | 3 | 55 |
| 140 | 0 | 84 | 181 | 4 | 109 | 9 | 0 | 6 | 46 | 3 | 31 | 84 | 0 | 56 |
| 141 | 4 | 85 | 183 | 2 | 110 | 10 | 3 | 7 | 48 | 0 | 32 | 85 | 3 | 57 |
| 143 | 2 | 86 | 185 | 0 | 111 | 12 | 0 | 8 | 49 | 3 | 33 | 87 | 0 | 58 |
| 145 | 0 | 87 | 186 | 4 | 112 | 13 | 3 | 9 | 51 | 0 | 34 | 88 | 3 | 59 |
| 146 | 4 | 88 | 188 | 2 | 113 | 15 | 0 | 10 | 52 | 3 | 35 | 90 | 0 | 60 |
| 148 | 2 | 89 | 190 | 0 | 114 | 16 | 3 | 11 | 54 | 0 | 36 | 91 | 3 | 61 |
| 150 | 0 | 90 | 191 | 4 | 115 | 18 | 0 | 12 | 55 | 3 | 37 | 93 | 0 | 62 |
| 151 | 4 | 91 | 193 | 2 | 116 | 19 | 3 | 13 | 57 | 0 | 38 | 94 | 3 | 63 |
| 143 | 2 | 92 | 195 | 0 | 117 | 21 | 0 | 14 | 58 | 3 | 39 | 96 | 0 | 64 |
| 155 | 0 | 93 | 196 | 4 | 118 | 22 | 3 | 15 | 60 | 0 | 40 | 97 | 3 | 65 |
| 156 | 4 | 94 | 198 |  | 120 | 24 | 0 | 16 | 61 | 3 | 41 | 99 | 0 | 66 |
| 158 | 2 | 95 | 200 |  |  | 25 | 3 | 17 | 63 | 0 | 42 | 100 | 3 | 67 |
| 160 | 0 | 96 |  |  |  | 27 | 0 | 18 | 64 | 3 | 43 | 102 | 0 | 68 |
| 161 | 4 | 97 |  |  |  | 28 | 3 | 19 | 66 | 0 | 44 | 103 | 3 | 69 |
| 163 | 2 | 98 |  |  |  | 30 | 0 | 20 | 67 | 3 | 45 | 105 | 0 | 70 |
| 165 | 0 | 99 |  |  |  | 31 | 3 | 21 | 69 | 0 | 46 | 106 | 3 | 71 |
| 166 | 4 | 100 |  |  |  | 33 | 0 | 22 | 70 | 3 | 47 | 108 | 0 | 72 |
| 168 | 2 | 101 |  |  |  | 34 | 3 | 23 | 72 | 0 | 48 | 109 | 3 | 73 |
| 170 | 0 | 102 |  |  |  | 36 | 0 | 24 | 73 | 3 | 49 | 111 | 0 | 74 |
| 171 | 4 | 103 |  |  |  | 37 | 3 | 25 | 75 | 0 | 50 | 112 | 3 | 75 |


| A Table of how many Fathoms \& Feet of yarn will make Fathoms of hauser lay'd rope |  |  |  |  |  | A Table of How Many Fathoms Feet of yarn will make Fathoms \& Feet of Stays |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Fath | Feet | Fath | Fath | Feet | Fath | Fath | Feet | Fath | Feet | Fath | Feet | Fath | Feet |
| 114 | 0 | 76 | 151 | 3 | 101 | 7 | 0 | 1 | 0 | 94 | 3 | 13 | 3 |
| 115 | 3 | 77 | 153 | 0 | 102 | 10 | 3 | 1 | 3 | 98 | 0 | 14 | 0 |
| 117 | 0 | 78 | 154 | 3 | 103 | 14 | 0 | 2 | 0 | 101 | 3 | 14 | 3 |
| 118 | 3 | 79 | 156 | 0 | 104 | 17 | 3 | 2 | 3 | 105 | 0 | 15 | 0 |
| 120 | 0 | 80 | 157 | 3 | 105 | 21 | 0 | 3 | 0 | 108 | 3 | 15 | 3 |
| 121 | 3 | 91 | 159 | 0 | 106 | 24 | 3 | 3 | 3 | 112 | 0 | 16 | 0 |
| 123 | 0 | 82 | 160 | 3 | 107 | 28 | 0 | 4 | 0 | 115 | 3 | 16 | 3 |
| 124 | 3 | 83 | 162 | 0 | 108 | 31 | 3 | 4 | 3 | 119 | 0 | 17 | 0 |
| 126 | 0 | 84 | 163 | 3 | 109 | 35 | 0 | 5 | 0 | 122 | 3 | 17 | 3 |
| 127 | 3 | 85 | 165 | 0 | 110 | 38 | 3 | 5 | 3 | 126 | 0 | 18 | 0 |
| 129 | 0 | 86 | 166 | 3 | 111 | 42 | 0 | 6 | 0 | 129 | 3 | 18 | 3 |
| 130 | 3 | 87 | 168 | 0 | 112 | 45 | 3 | 6 | 3 |  |  |  |  |
| 132 | 0 | 88 | 169 | 3 | 113 | 19 | 0 | 7 | 0 |  |  |  |  |
| 133 | 3 | 89 | 171 | 0 | 114 | 52 | 3 | 7 | 3 |  |  |  |  |
| 135 | 0 | 90 | 172 | 3 | 115 | 56 | 0 | 8 | 0 |  |  |  |  |
| 136 | 3 | 91 | 174 | 0 | 116 | 59 | 3 | 8 | 3 |  |  |  |  |
| 138 | 0 | 92 | 175 | 3 | 117 | 63 | 0 | 9 | 0 |  |  |  |  |
| 139 | 3 | 93 | 177 | 0 | 118 | 66 | 3 | 9 | 3 |  |  |  |  |
| 141 | 0 | 94 | 178 | 3 | 119 | 70 | 0 | 10 | 0 |  |  |  |  |
| 142 | 3 | 95 | 180 | 0 | 120 | 73 | 3 | 10 | 3 |  |  |  |  |
| 144 | 0 | 96 | 182 | 3 | 121 | 77 | 0 | 11 | 0 |  |  |  |  |
| 145 | 3 | 97 | 184 | 0 | 122 | 80 | 3 | 11 | 3 |  |  |  |  |
| 147 | 0 | 98 | 185 | 3 | 123 | 84 | 0 | 12 | 0 |  |  |  |  |
| 148 | 3 | 99 | 187 | 0 | 124 | 87 | 3 | 12 | 3 |  |  |  |  |
| 150 | 0 | 100 | 188 | 3 | 125 | 91 | 0 | 13 | 0 |  |  |  |  |



## For Warping Tacks

Taper them ${ }^{2 / 3}$ of the length, as suppose your yarn be 24 fathom begin your taper at 8 fathom from the head of your tacks; and if you have 19 or 25 or any odd thread a hook at the head, take the head half for the shank \& cut your taper of an equal length. Some do put but $1 / 3$ of the yarn in the shanks, for suppose the head to be 24 threads a hook at the head they put 8 in the shank \& so proportion for all others.

For Warping topsail sheets
Begin your taper half way \& half your yarn in the shank but if you be odd threads a hook in the head, take the least half for the shank.

Tables for sizing strands

| A Table for Sizing Strands for cable in inch \& qtr \& the 1 8th part of a $1 / 4$ of an inch |  |  |  |  |  |  |  | A Table for Sizing Strands for stays in inches \& 9 parts of an inch |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Cables | In | Qr | Parts | Cable | In | Qr | Parts | Stay | In | Parts | Stay | Ins | Parts |
| 18 | 9 | 2 | 0 | 10 | 5 | 1 | 61 | 18 | 8 | 0 | $10^{1 / 2}$ | 4 | 6 |
| $17^{1 ⁄ 2}$ | 9 | 0 | 17 | $91 / 2$ | 5 | 0 | 55 | $17^{1 / 2}$ | 7 | 7 | 10 | 4 | 4 |
| 17 | 8 | 3 | 16 | 9 | 4 | 3 | 50 | 17 | 7 | 5 | $91 / 2$ | 4 | 2 |
| $16^{1 ⁄ 2}$ | 8 | 2 | 15 | $8^{1 / 2}$ | 4 | 1 | 45 | $16^{1 / 2}$ | 7 | 3 | 9 | 4 | 0 |
| 16 | 8 | 1 | 14 | 8 | 4 | 0 | 40 | 16 | 7 | 1 | $8^{1 / 2}$ | 3 | 7 |
| $15^{1 ⁄ 2}$ | 8 | 0 | 13 | $71 / 2$ | 3 | 3 | 35 | $15^{1 / 2}$ | 6 | 8 | 8 | 3 | 5 |
| 15 | 7 | 3 | 12 | 7 | 3 | 2 | 31 | 15 | 6 | 6 | 7112 | 3 | 3 |
| $14^{1 / 2}$ | 7 | 2 | 11 | $6^{1 / 2}$ | 3 | 1 | 27 | $14^{1 / 2}$ | 6 | 4 | 7 | 3 | 1 |
| 14 | 7 | 1 | 10 | 6 | 3 | 0 | 23 | 14 | 6 | 2 | $6^{1 / 2}$ | 2 | 8 |
| $13^{1 / 2}$ | 7 | 0 | 9 | $5^{1 ⁄ 2}$ | 2 | 3 | 20 | $13^{1 / 2}$ | 6 | 0 | 6 | 2 | 6 |
| 13 | 6 | 3 | 8 | 5 | 2 | 2 | 16 | 13 | 5 | 7 | $51 / 2$ | 2 | 4 |
| $1211 / 2$ | 6 | 2 | 7 | $4^{112}$ | 2 | 1 | 13 | $12^{1 / 2}$ | 5 | 5 | 5 | 2 | 2 |
| 12 | 6 | 1 | 6 | 4 | 2 | 0 | 11 | 12 | 5 | 3 | $4^{1 / 2}$ | 2 | 0 |
| 11 1⁄2 | 6 | 0 | 5 | $31 / 2$ | 1 | 3 | 8 | $11^{1 / 2}$ | 5 | 1 | 4 | 2 | 7 |
| 11 | 5 | 3 | 4 | 3 | 1 | 2 | 6 | 11 | 4 | 8 |  |  |  |
| $10^{1 / 2}$ | 5 | 2 |  |  |  |  |  |  |  |  |  |  |  |


| This is the Rivell of 24 |  |  | Hauser Lay＇d cordage at the size of 16 thread a hook for 3 in |  |  |  | Hauser Lay＇d Cordage at 20 for 3 in |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size |  |  | Size |  |  | $$ | Siz |  |  |  | $\begin{aligned} & \text { むj} \\ & 0 \\ & 0 \\ & \text { ¿ } \end{aligned}$ | $\begin{aligned} & \text { む̈ } \\ & \text { ®̈ } \\ & \text { む } \end{aligned}$ |
| 0 | 3 | 3 | 0 | 3 | 2 | 6 | 0 | 3 | 2 | 6 | 6 | 12 |
| 1 | 0 | 4 | 1 | 0 | 3 | 9 | 1 | 0 | 3 | 9 | 6 | 12 |
| 1 | 1 | 5 | 1 | 2 | 5 | 15 | 1 | 2 | 6 | 18 | 7 | 10 |
| 1 | 2 | 6 | 2 | 0 | 8 | 24 | 2 | 0 | 9 | 27 | 9 | 10 |
| 1 | 3 | 8 | 2 | 2 | 12 | 36 | 2 | 2 | 14 | 42 | 6 | 4 |
| 2 | 0 | 10 | 3 | 0 | 16 | 48 | 3 | 0 | 20 | 60 | 9 | 4 |
| 2 | 1 | 13 | 3 | 2 | 21 | 63 | 3 | 2 | 26 | 78 | 10 | 4 |
| 2 | 2 | 16 | 4 | 0 | 28 | 48 | 4 | 0 | 35 | 105 | 14 | 4 |
| 2 | 3 | 20 | 4 | 2 | 36 | 108 | 4 | 2 | 44 | 132 | 16 | 4 |
| 3 | 0 | 24 | 5 | 0 | 44 | 132 | 5 | 0 | 54 | 162 | 18 | 3 |
| 3 | 1 | 28 | 5 | 2 | 53 | 159 | 5 | 2 | 65 | 195 | 20 | 3 |
| 3 | 2 | 33 | 6 | 0 | 64 | 192 | 6 | 0 | 77 | 231 | 23 | 3 |
| 3 | 3 | 37 | 6 | 2 | 75 | 225 | 6 | 2 | 91 | 273 | 26 | 3 |
| 4 | 0 | 43 | 7 | 0 | 87 | 261 | 7 | 0 | 105 | 315 | 30 | 3 |
| 4 | 1 | 48 | 7 | 2 | 100 | 300 | 7 | 2 | 122 | 366 | 34 | 3 |
| 4 | 2 | 54 | 8 | 0 | 113 | 339 | 8 | 0 | 138 | 414 | 40 | 3 |
| 4 | 3 | 60 | 8 | 2 | 128 | 384 | 8 | 2 | 156 | 468 | 45 | 3 |
| 5 | 0 | 66 | 9 | 0 | 144 | 432 | 9 | 0 | 175 | 525 | 50 | 2 |
| 5 | 1 | 74 | 9 | 2 | 160 | 480 | 9 | 2 | 195 | 585 | 54 | 2 |
|  |  |  | 10 | 0 | 178 | 534 | 10 | 0 | 216 | 648 | 60 | 2 |


| Size for Ordinary Yarn, the Size of 20 Thread for 3 inch |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| :Nㅜ |  |  |  |  |  |  |  | $\begin{aligned} & \stackrel{N}{\sim} \end{aligned}$ |  |  |  |  |  |  |
| 19 | * | 144 | 432 | 144 | 1872 | 180 |  | 10 | 2 | 44 | 132 | 44 | 572 | 56 |
| 18 | 2 | 136 | 408 | 136 | 1768 | 171 | - | 10 | 0 | 40 | 120 | 40 | 520 | 51 |
| 18 | 0 | 129 | 387 | 129 | 1677 | 162 | 0 | 9 | 2 | 36 | 108 | 36 | 468 | 46 |
| 17 | 2 | 122 | 366 | 122 | 1586 | 153 | $\stackrel{\sim}{0}$ | 9 | 0 | 33 | 99 | 33 | 429 | 41 |
| 17 | 0 | 115 | 345 | 115 | 1495 | 145 | $\stackrel{\circ}{\square}$ | 8 | 2 | 29 | 87 | 29 | 377 | 37 |
| 16 | 2 | 109 | 327 | 109 | 1417 | 136 | 3 | 8 | 0 | 26 | 78 | 26 | 338 | 33 |
| 16 | 0 | 103 | 309 | 103 | 1339 | 128 | O | 7 | 2 | 23 | 69 | 23 | 299 | 29 |
| 15 | 2 | 96 | 288 | 96 | 1248 | 120 | N | 7 | 0 | 20 | 60 | 20 | 260 | 25 |
| 15 | 0 | 90 | 270 | 90 | 1170 | 113 | 鿒 | 6 | 2 | 17 | 57 | 17 | 221 | 22 |
| 14 | 2 | 84 | 252 | 84 | 1092 | 105 | 2 | 6 | 0 | 15 | 45 | 15 | 195 | 19 |
| 14 | 0 | 78 | 224 | 78 | 1014 | 98 | - | 5 | 2 | 13 | 39 | 13 | 169 | 16 |
| 13 | 2 | 73 | 219 | 73 | 949 | 91 | $\frac{0}{2}$ | 5 | 0 | 11 | 33 | 11 | 143 | 13 |
| 13 | 0 | 68 | 204 | 68 | 884 | 85 | $\stackrel{\sim}{\omega}$ | 4 | 2 | 9 | 27 | 9 | 117 | 11 |
| 12 | 2 | 63 | 189 | 63 | 819 | 78 | $\stackrel{\rightharpoonup}{\text { ¢ }}$ | 4 | 0 | 7 | 21 | 7 | 91 | 9 |
| 12 | 0 | 58 | 174 | 58 | 784 | 72 | 2 | 3 | 2 | 5 | 15 | 5 | 65 | 7 |
| 11 | 2 | 53 | 159 | 53 | 689 | 67 | $\checkmark$ | 3 | 0 | 4 | 12 | 4 | 52 | 5 |
| 11 | 0 | 48 | 144 | 48 | 624 | 56 |  |  |  |  |  |  |  |  |

The last column is fine yarn

| With the 1 / 8 inch |  | $\checkmark$ | $\cdots$ | 10 | ^ | $\square$ | $\cdots$ | 10 | ^ | $\checkmark$ | $\cdots$ | $1 \sim$ | ^ | $\bigcirc$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Size of Thread | 10 | 10 | $1 \bigcirc$ | $1 \bigcirc$ | 10 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\wedge$ | ^ | $\wedge$ | ^ | $\infty$ |
| Size of Cable | $\stackrel{7}{7}$ | N $\stackrel{\rightharpoonup}{*}$ | $\stackrel{\text { N }}{ }$ | $\begin{aligned} & \text { N} \\ & \underset{\sim}{N} \end{aligned}$ | $\stackrel{\square}{\square}$ | $\begin{gathered} \text { à } \\ \underset{\sim}{2} \end{gathered}$ | $\stackrel{\text { H }}{\sim}$ | $\stackrel{N}{\sim}$ | $\stackrel{10}{\square}$ | $\begin{aligned} & \text { N} \\ & \stackrel{i}{\square} \end{aligned}$ | $\stackrel{\square}{\square}$ | $\xrightarrow{\sim}$ | $\stackrel{\sim}{-}$ | $\stackrel{-}{\stackrel{N}{\sim}}$ |
| With the $1 / 8$ inch | $\stackrel{\infty}{\sim}$ | 0 | N | $\cdots$ | $\cdots$ | $\wedge$ | $\checkmark$ | ^ | 10 | ^ | $\bigcirc$ | N | + | $\bigcirc$ |
| Size of Thread | $\checkmark$ | $\sim$ | N | $\sim$ | $\sim$ | N | $\cdots$ | $\cdots$ | $\cdots$ | $\cdots$ | + | + | + | + |
| Size of Cable | + | $\stackrel{N}{\underset{\sim}{4}}$ | 10 | $\begin{aligned} & \text { N } \\ & \text { in } \end{aligned}$ | $\bigcirc$ | $\frac{\imath_{0}}{0}$ | $\wedge$ | $\stackrel{\sim}{N}$ | $\infty$ | $\underset{\infty}{\underset{\sim}{N}}$ | の | ã | $\bigcirc$ | $\stackrel{\text { a }}{\substack{--}}$ |

[One line of text along right hand margin is indecipherable]

| Fine Yarn |  |  |  |  | An account of what Man is Allow'd for Strands for stays; and strands \& stay per Day |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\underset{N}{N}}{i}$ |  |  |  |  | $\stackrel{\sim}{N}$ | Man per Strand |  |  |  | $\stackrel{\stackrel{\sim}{N}}{\dot{\omega}}$ |  |  |  |  |
| $11 / 2$ | 7 | 21 | 7 | 10 | 19 | 27 | 4 | 70 | 6 | 11 | 15 | 4 | 36 | 6 |
| 2 | 10 | 30 | 9 | 10 | $18^{1 / 2}$ | 26 | 4 | 65 | 6 | $10^{1 / 2}$ | 14 | 4 | 34 | 6 |
| $21 / 2$ | 16 | 48 | 6 | 4 | 18 | 25 | 4 | 64 | 6 | 10 | 14 | 4 | 32 | 6 |
| $23 / 4$ | 20 | 60 | 7 | 4 | $171 / 2$ | 24 | 4 | 63 | 6 | $911 / 2$ | 12 | 4 | 30 | 6 |
| 3 | 25 | 75 | 10 | 4 | 17 | 23 | 4 | 60 | 6 | 9 | 12 | 4 | 29 | 6 |
| $31 / 2$ | 34 | 102 | 12 | 4 | $16^{1 / 2}$ | 22 | 4 | 58 | 6 | $81 / 2$ | 11 | 4 | 27 | 6 |
| 4 | 44 | 132 | 14 | 4 | 16 | 21 | 4 | 56 | 6 | 8 | 11 | 4 | 26 | 8 |
| $4^{1 / 2}$ | 56 | 168 | 16 | 3 | $15^{1 / 2}$ | 20 | 4 | 54 | 6 | $71 / 2$ | 10 | 4 | 24 | 8 |
| 5 | 68 | 204 | 18 | 3 | 15 | 20 | 4 | 52 | 6 | 7 | 10 | 4 | 23 | 8 |
| $51 / 2$ | 83 | 249 | 20 | 3 | $14^{1 / 2}$ | 19 | 4 | 50 | 6 | $61 / 2$ | 9 | 4 | 21 | 8 |
| 6 | 98 | 294 | 23 | 3 | 14 | 19 | 4 | 48 | 6 | 6 | 9 | 4 | 20 | 8 |
| $61 / 2$ | 115 | 345 | 26 | 3 | $13^{1 / 2}$ | 18 | 4 | 46 | 6 | $51 / 2$ | 9 | 4 | 18 | 8 |
| 7 | 133 | 399 | 30 | 3 | 13 | 16 | 4 | 44 | 6 | 5 | 8 | 8 | 17 | 8 |
| $71 / 2$ | 153 | 459 | 34 | 3 | $121 / 2$ | 16 | 4 | 42 | 6 | $4^{1 / 2}$ | 7 | 8 | 16 | 8 |
| 8 | 174 | 522 | 40 | 3 | 12 | 16 | 4 | 40 | 6 | 4 | 7 | 8 | 14 | 8 |
| $81 / 2$ | 197 | 591 | 43 | 3 | $11^{1 / 2}$ | 15 | 4 | 38 | 6 |  |  |  |  |  |
| 9 | 220 | 660 | 50 | 2 |  |  |  |  |  |  |  |  |  |  |
| $911 / 2$ | 246 | 738 | 54 | 2 |  |  |  |  |  |  |  |  |  |  |
| 10 | 272 | 810 | 60 | 2 |  |  |  |  |  |  |  |  |  |  |

## Cable Lay'd Cordage

| $\stackrel{\sim}{\tilde{\omega}}$ |  |  | $\begin{aligned} & \stackrel{0}{\Xi} \\ & \tilde{ভ} \\ & \pm \\ & \Xi \\ & \Xi \end{aligned}$ |  |  |  | $\begin{aligned} & \text { む} \\ & \text { त } \\ & \tilde{0} \\ & \stackrel{0}{0} \\ & \tilde{0} \end{aligned}$ | $\stackrel{\otimes}{\tilde{N}}$ |  |  | $\begin{aligned} & \stackrel{0}{0} \\ & \tilde{0} \\ & \cong \\ & \Xi \\ & \Xi \end{aligned}$ |  |  |  | $\begin{aligned} & \text { む} \\ & \text { त } \\ & \tilde{0} \\ & \stackrel{0}{0} \\ & \tilde{0} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 6 | 18 | 54 | 7 | 12 | 9 | 5 | $12^{1 / 2}$ | 90 | 270 | 810 | 19 | 4 | 55 | 4 |
| $31 / 2$ | 8 | 24 | 72 | 8 | 12 | 10 | 5 | 13 | 98 | 294 | 882 | 21 | 4 | 59 | 4 |
| 4 | 10 | 30 | 90 | 9 | 12 | 12 | 5 | $13^{1 / 2}$ | 106 | 318 | 954 | 22 | 4 | 64 | 4 |
| $4^{11 / 2}$ | 12 | 36 | 108 | 10 | 12 | 13 | 5 | 14 | 114 | 342 | 1026 | 23 | 4 | 70 | 4 |
| 5 | 15 | 45 | 137 | 7 | 4 | 14 | 4 | $14^{1 / 2}$ | 122 | 366 | 1098 | 24 | 4 | 75 | 4 |
| $5^{1 / 2}$ | 18 | 54 | 162 | 7 | 4 | 15 | 4 | 15 | 130 | 390 | 1170 | 25 | 4 | 80 | 4 |
| 6 | 21 | 63 | 189 | 8 | 4 | 18 | 4 | $15^{1 / 2}$ | 139 | 417 | 1251 | 26 | 4 | 84 | 4 |
| $6^{112}$ | 24 | 72 | 216 | 8 | 4 | 20 | 4 | 16 | 148 | 444 | 1332 | 28 | 4 | 90 | 4 |
| 7 | 28 | 84 | 258 | 10 | 4 | 22 | 4 | $16^{1 / 2}$ | 157 | 471 | 1413 | 29 | 4 | 95 | 4 |
| $71 / 2$ | 32 | 96 | 288 | 10 | 4 | 24 | 4 | 17 | 167 | 501 | 1503 | 31 | 4 | 101 | 3 |
| 8 | 37 | 111 | 333 | 11 | 4 | 26 | 4 | $17^{1 / 2}$ | 177 | 530 | 1593 | 32 | 4 | 106 | 3 |
| $81 / 2$ | 42 | 126 | 378 | 11 | 4 | 27 | 4 | 18 | 187 | 561 | 1683 | 34 | 3 | 113 | 3 |
| 9 | 47 | 141 | 423 | 12 | 4 | 29 | 4 | $18^{1 / 2}$ | 198 | 594 | 1782 | 35 | 3 | 119 | 3 |
| $91 / 2$ | 52 | 156 | 463 | 13 | 4 | 31 | 4 | 19 | 209 | 627 | 1881 | 36 | 3 | 126 | 3 |
| 10 | 58 | 174 | 522 | 14 | 4 | 33 | 4 | $1911 / 2$ | 220 | 660 | 1980 | 38 | 3 | 133 | 3 |
| $10^{1 / 2}$ | 64 | 192 | 576 | 15 | 4 | 37 | 4 | 20 | 231 | 693 | 2709 | 40 | 3 | 140 | 3 |
| 11 | 70 | 210 | 634 | 16 | 4 | 42 | 4 | $20^{1 / 2}$ | 243 | 729 | 2187 | 43 | 3 | 149 | 3 |
| $11^{1 / 2}$ | 76 | 225 | 664 | 17 | 4 | 45 | 4 | 21 | 255 | 765 | 2295 | 46 | 3 | 156 | 2 |
| 12 | 83 | 249 | 717 | 18 | 4 | 50 | 4 | $211 / 2$ | 267 | 801 | 2403 | 49 | 3 | 165 | 2 |
|  |  |  |  |  |  |  |  | 22 | 280 | 849 | 2520 | 52 | 3 | 176 | - |


| Cable Strands Hauser lay＇d being the size of 17：18：19：20 |  |  |  |  | 16 Thread for 6 in Rope 20 thread a hook for 6 in cable lay＇d |  |  |  |  | A Table Shewing the size of strands for a cable |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\stackrel{\sim}{\hat{N}}$ |  |  |  |  | $\stackrel{\sim}{\tilde{\circ}}$ | 17 | 18 | 19 | 20 | $\begin{aligned} & \frac{0}{0} \\ & \stackrel{0}{0} \\ & \tilde{0} \\ & \stackrel{0}{0} \\ & \stackrel{y}{\tilde{n}} \end{aligned}$ |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  | In | 1／8 |  | In | 1／8 |
| 18 | 153 | 162 | 171 | 180 | 10 | 47 | 50 | 52 | 55 | 4 | 2 | 1 | 11 | 5 | 6 |
| $17^{1 / 2}$ | 144 | 153 | 161 | 170 | $91 / 2$ | 42 | 45 | 47 | 50 | $4^{1 / 2}$ | 2 | 3 | $11^{1 / 2}$ | 6 | 0 |
| 17 | 136 | 144 | 153 | 160 | 9 | 38 | 40 | 42 | 45 | 5 | 2 | 5 | 12 | 6 | 3 |
| $16^{1 / 2}$ | 128 | 136 | 143 | 151 | $81 / 2$ | 34 | 36 | 38 | 40 | $51 / 2$ | 2 | 7 | $12^{1 / 2}$ | 6 | 5 |
| 16 | 121 | 128 | 135 | 144 | 8 | 30 | 32 | 34 | 36 | 6 | 3 | 1 | 13 | 6 | 7 |
| $151 / 2$ | 113 | 120 | 128 | 135 | $71 / 2$ | 26 | 25 | 29 | 31 | $61 / 2$ | 3 | 3 | $131 / 2$ | 7 | 1 |
| 15 | 103 | 112 | 118 | 125 | 7 | 23 | 24 | 25 | 27 | 7 | 3 | 5 | 14 | 7 | 3 |
| $141 / 2$ | 99 | 105 | 110 | 116 | $61 / 2$ | 20 | 21 | 22 | 23 | $71 / 2$ | 3 | 7 | $14^{1 / 2}$ | 7 | 5 |
| 14 | 92 | 90 | 105 | 108 | 6 | 17 | 18 | 19 | 20 | 8 | 4 | 2 | 15 | 7 | 7 |
| $131 / 2$ | 85 | 91 | 96 | 102 | $51 / 2$ | 14 | 15 | 16 | 17 | $81 / 2$ | 4 | 4 | $15^{1 / 2}$ | 8 | 1 |
| 13 | 79 | 84 | 90 | 96 | 5 | 11 | 12 | 13 | 14 | 9 | 4 | 6 | 16 | 8 | 4 |
| $12^{1 / 2}$ | 73 | 78 | 83 | 88 | $4^{1 / 2}$ | 9 | 10 | 11 | 12 | 91／2 | 5 | 0 | $16^{1 / 2}$ | 8 | 6 |
| 12 | 68 | 72 | 76 | 80 | 4 | 8 | 8 | 9 | 10 | 10 | 5 | 2 | 17 | 9 | ＊ |
| $11^{1 / 2}$ | 62 | 66 | 70 | 73 | $31 / 2$ | 5 | 6 | 7 | 8 | $10^{1 / 2}$ | 5 | 4 | $17^{1 / 2}$ | 9 | 4 |
| 11 | 57 | 60 | 63 | 67 | 3 | 4 | 2 | 5 | 6 |  |  |  |  |  |  |
| $10^{1 / 2}$ | 52 | 55 | 58 | 61 |  |  |  |  | － |  |  |  |  |  |  |


|  | Cables a day | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ | $\infty$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Men for the cable | N | ন | 산 | $\stackrel{\infty}{\sim}$ | $\stackrel{\infty}{\sim}$ | $\stackrel{\sim}{~}$ | $\stackrel{\square}{\square}$ | $\stackrel{1}{\sim}$ | $\stackrel{\square}{\sim}$ | $\stackrel{9}{7}$ | N | F | $\bigcirc$ | の | $\bigcirc$ |
|  | Strands a day | $\underset{\sim}{\sim}$ | N | $\underset{\sim}{1}$ | $\underset{\sim}{1}$ | $\underset{\sim}{1}$ | $\underset{\sim}{\sim}$ | $\underset{\sim}{\sim}$ | $\underset{\sim}{1}$ | $\underset{\sim}{1}$ | $\underset{\sim}{\sim}$ | N | N | $\underset{\sim}{1}$ | $\underset{\sim}{1}$ | $\underset{\sim}{\sim}$ |
|  | Men for the strand | $\bigcirc$ | の | $\bigcirc$ | $\infty$ | $\infty$ | $\wedge$ | ＾ | $\wedge$ | $\wedge$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |
|  | Thread in y ${ }^{\text {e cable }}$ | 寺 | $\stackrel{\circ}{\circ}$ | 7 | － | $\ni$ | \＆ | ¢ | セ゚ | $\bigcirc$ | 出 | $\stackrel{1}{7}$ | ¢ | ¢ | N | $\stackrel{\infty}{\sim}$ |
|  | Thread in a shank | 간 | $\stackrel{\infty}{\sim}$ | $\stackrel{\sim}{\sim}$ | $\pm$ | $\stackrel{9}{7}$ | F | の | $\infty$ | $\wedge$ | $\bigcirc$ | ๓ | ＋ | ＋ | $\cdots$ | $\sim$ |
|  | Thread a hook | $\stackrel{\circ}{\circ}$ | ก1 | 令 | \％ | ल | ल | ते | $\stackrel{1}{2}$ | ন | $\stackrel{\sim}{\sim}$ | $\stackrel{\square}{\square}$ | N | $\bigcirc$ | $\infty$ | $\bigcirc$ |
|  | Size | $\stackrel{1}{2}$ | $\begin{aligned} & a_{n} \\ & a \end{aligned}$ | の | $\begin{aligned} & \stackrel{\sim}{\infty} \\ & \infty \end{aligned}$ | $\infty$ | $\begin{aligned} & \mathbf{N}^{2} \\ & \hline \end{aligned}$ | $\wedge$ | $\stackrel{3}{6}$ | $\bigcirc$ | $\begin{aligned} & \text { in } \\ & \text { in } \\ & \hline \end{aligned}$ | ๓ | $\stackrel{\text {－}}{\text {－}}$ | ＋ | $\begin{gathered} \stackrel{\sim}{n} \\ \text { m} \end{gathered}$ | m |


| A table to shew the lengths of hauser lay'd cordage by the length of the yarn |  |  |  |  |  | The length of cable by the length of the yarn, the strands to be brought about in 3 parts |  |  |  |  |  | A table to Shew the length of cable lay'd cordage by the length of yarn |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | 2 | 5 | 135 | 0 | 90 | 5 | 1 | 90 | 18 | 175 | 35 | 5 | 3 | 70 | 42 |
| 15 | 0 | 10 | 142 | 2 | 95 | 10 | 2 | 95 | 19 | 180 | 36 | 10 | 6 | 75 | 45 |
| 20 | 2 | 15 | 150 | 0 | 100 | 15 | 3 | 100 | 20 | 185 | 37 | 15 | 9 | 80 | 48 |
| 30 | 0 | 20 | 157 | 2 | 105 | 20 | 4 | 105 | 21 | 190 | 38 | 20 | 12 | 85 | 51 |
| 37 | 2 | 25 | 165 | 0 | 110 | 25 | 5 | 110 | 22 | 195 | 39 | 25 | 15 | 90 | 54 |
| 45 | 0 | 30 | 172 | 2 | 115 | 30 | 6 | 115 | 23 | 200 | 40 | 30 | 18 | 95 | 57 |
| 52 | 2 | 35 | 180 | 0 | 120 | 35 | 7 | 120 | 24 | 205 | 41 | 35 | 21 | 100 | 60 |
| 60 | 0 | 40 | 187 | 2 | 125 | 40 | 8 | 125 | 25 | 210 | 42 | 40 | 24 | 105 | 63 |
| 67 | 2 | 45 | 195 | 0 | 130 | 45 | 9 | 130 | 26 | 215 | 43 | 45 | 27 | 110 | 66 |
| 75 | 0 | 50 | 202 | 2 | 135 | 50 | 10 | 135 | 27 | 220 | 44 | 50 | 30 | 115 | 69 |
| 82 | 2 | 55 | 210 | 0 | 140 | 55 | 11 | 140 | 28 | 225 | 45 | 55 | 33 | 120 | 72 |
| 90 | 0 | 60 | 217 | 2 | 145 | 60 | 12 | 145 | 29 | 230 | 46 | 60 | 36 | 125 | 75 |
| 97 | 2 | 65 | 225 | 0 | 150 | 65 | 13 | 150 | 30 | 235 | 47 | 65 | 39 | 130 | 78 |
| 105 | 0 | 70 | 232 | 2 | 155 | 70 | 14 | 155 | 31 | 240 | 48 |  |  |  |  |
| 112 | 2 | 75 | 240 | 0 | 160 | 75 | 15 | 160 | 32 | 245 | 49 |  |  |  | - 3 |
| 120 | 0 | 80 | * |  |  | 80 | 16 | 165 | 33 | 250 | 50 |  |  |  | E |
| 127 | 2 | 85 | * |  |  | 85 | 17 | 170 | 34 |  |  |  |  |  | రీ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Length of cable | $\bar{\infty}$ | あ | - | 8 | ® | ๑๐ | $\stackrel{\square}{\square}$ | $\underset{\sim}{\text { N}}$ | $\stackrel{\square}{\square}$ | $\stackrel{\infty}{\sim}$ | $\exists$ | $\underset{\sim}{\sharp}$ | $\stackrel{\text { A }}{ }$ | 죽 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Length of Yarn | $\stackrel{\leftrightarrow}{\sim}$ | $\stackrel{7}{7}$ | $\stackrel{8}{7}$ | $\stackrel{\circ}{\square}$ | $\stackrel{\sim}{\square}$ | $\stackrel{0}{\square}$ | $\stackrel{\square}{\square}$ | 윽 | $\stackrel{\text { ® }}{\text { N }}$ | $\stackrel{\otimes}{\sim}$ | $\stackrel{\llcorner }{\sim}$ | $\stackrel{\square}{\square}$ | ๕ | - |


| Length of the Stay by the length of yarn the strands to be brought about in 4 parts |  |  |  | The weight of Cable, the yarn to be 200 fathom\& the cable 120 fathom with the weight of one fathom of each |  |  |  |  |  |  | The weight of Cable lay'd cordage the cable to be 100 fathom |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Ct | Qr | Lb | Q ${ }^{\text {r }}$ | Lb | $\begin{aligned} & \mathrm{O} \\ & \mathrm{z} \end{aligned}$ | Size | Ct | Q | Lb | Size | Ct | Q ${ }^{\text {r }}$ | Lb |
| 7 | 1 | 112 | 16 | 4 | 4 | 0 | 0 | - | 3 | 11 | 22 | 102 | 1 | 11 | $12^{1 / 2}$ | 33 | 3 | 11 |
| 14 | 2 | 119 | 17 | $41 / 2$ | 5 | 0 | 14 | - | 4 | 10 | $211 / 2$ | 97 | 2 | 14 | 12 | 30 | 1 | 10 |
| 21 | 3 | 126 | 18 | 5 | 6 | 10 | 0 | - | 5 | 9 | 21 | 92 | 0 | 26 | 111/2 | 27 | 3 | 4 |
| 28 | 4 | 132 | 19 | $51 / 2$ | 7 | 2 | 14 | - | 7 | 0 | $201 / 2$ | 88 | 3 | 11 | 11 | 25 | 2 | 10 |
| 35 | 5 | 140 | 20 | 6 | 9 | 0 | 0 | - | 8 | 6 | 20 | 84 | 1 | 23 | $10^{1 / 2}$ | 23 | 1 | 7 |
| 42 | 6 | 147 | 21 | $61 / 2$ | 10 | 2 | 14 | - | 9 | 12 | $19^{1 / 2}$ | 80 | 1 | 20 | 10 | 21 | 0 | 23 |
| 49 | 7 | 154 | 22 | 7 | 12 | 1 | 0 | - | 11 | 3 | 19 | 76 | 1 | 19 | 91122 | 19 | 0 | 1 |
| 56 | 8 | 161 | 23 | $71 / 2$ | 14 | 0 | 14 | - | 13 | 1 | $18^{1 / 2}$ | 72 | 1 | 16 | 9 | 17 | 0 | 20 |
| 63 | 9 | 168 | 24 | 8 | 16 | 0 | 0 | - | 14 | 14 | 18 | 68 | 1 | 14 | $81 / 2$ | 15 | 1 | 12 |
| 70 | 10 | 175 | 25 | $81 / 2$ | 18 | 0 | 14 | - | 16 | 12 | $171 / 2$ | 64 | 1 | 11 | 8 | 13 | 2 | 12 |
| 77 | 11 | 182 | 26 | 9 | 20 | 1 | 0 | - | 18 | 14 | 17 | 61 | 3 | 7 | $71 / 2$ | 11 | 2 | 22 |
| 84 | 12 | 189 | 27 | $91 / 2$ | 22 | 0 | 14 | - | 23 | 5 | $16^{1 / 2}$ | 57 | 1 | 16 | 7 | 10 | 0 | 27 |
| 91 | 13 | 196 | 28 | 10 | 25 | 0 | 0 | - | - | * | 16 | 54 | 0 | 13 | $61 / 2$ | 8 | 3 | 1 |
| 98 | 14 | 203 | 29 | 11 | 30 | 1 | 0 | - | 5 | 9 | 15 1/2 | 50 | 3 | 17 | 6 | 7 | 2 | 19 |
| 105 | 15 | 210 | 30 | 12 | 36 | 0 | 0 | - | 11 | 3 | 15 | 47 | 2 | 3 | 51/2 | 6 | 2 | 9 |
|  |  |  |  | 13 | 42 | 0 | 0 | - | 17 | 11 | $14^{1 / 2}$ | 44 | 2 | 12 | 5 | 5 | 1 | 26 |
|  |  |  |  | 14 | 49 | 0 | 0 |  | * | * | 14 | 41 | 2 | 20 | $4^{1 / 2}$ | 4 | 1 | 15 |
|  |  |  |  |  |  |  |  |  |  |  | $131 / 2$ | 38 | 3 | 1 | 4 | 3 | 2 | 1 |
|  |  |  |  |  |  |  |  |  |  |  | 13 | 35 | 3 | 9 | $31 / 2$ | 2 | 3 | 17 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 3 | 2 | 0 | 21 |



## Dimensons of the Frigate South Carolina

Length of keel for tonnage 143 ft 8 in . Length of gundeck from one foot before the rabbit of the stern to the rabbit of the port 172 ft 6 t in. Extreem breadth as follows Viz:

| At |  | Ft | In |  | Ft | In |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dis | 19 | 5 | from rabbit of port is | 35 | $91 / 2$ | broad |
| 2 | D ${ }^{\text {o }}$ | 20 |  | forward |  | 40 | 0 |
| 3 | $\mathrm{D}^{\circ}$ | 20 |  | $\mathrm{D}^{\text {o }}$ | 41 | $10^{3 / 4}$ |  |
| 4 | Do | 21 |  | D ${ }^{\text {o }}$ | 42 | 6 |  |
| 5 | Do | 20 |  | D ${ }^{\text {o }}$ | 42 | $81 / 2$ | extream breadth |
| 6 | $\mathrm{D}^{\text {o }}$ | 20 |  | $\mathrm{D}^{\text {o }}$ | 41 | 9 |  |
| 7 | $\mathrm{D}^{\text {o }}$ | 20 |  | $\mathrm{D}^{\circ}$ | 37 | 9 |  |
| 8 | Do | 11 | 10 | D ${ }^{\text {o }}$ | 33 | $11 / 2$ |  |
| 9 | Do | 10 | 2 | D ${ }^{\text {o }}$ | 26 | $61 / 2$ |  |
| 10 | $\mathrm{D}^{\text {o }}$ | 7 | 7 | $\mathrm{D}^{\circ}$ to the after part of |  |  |  |
| 11 | $\mathrm{D}^{\circ}$ | 6 |  | $\mathrm{D}^{\circ}$ to the rabbit of the |  |  |  |
| 12 | D ${ }^{\text {o }}$ |  | 1 | $\mathrm{D}^{\circ}$ to the foreside of |  |  |  |

Feet 172-6 length of gundeck.
Stem tumbles home 6 in above wales.

Extream Breadth at the top of the plankshear

|  | Ft In | Ft In |  |
| :--- | ---: | :--- | :--- |
| 1 distance | 6 | 1 | abaft the rabbit of the stern |
| 2 distance | 20 |  | 26 wide |
| 3 distance | 20 | 33 | 6 |
| 4 distance | 20 |  | 37 |
| 5 distance | 20 | 0 | 38 |
| 6 distance | 26 | 0 | 38 |
| 7 distance | 20 | 0 | 37 |
| 8 distance | 16 |  | 35 |
| 9 distance | 20 |  | 31 |
| 10 distance | 6 | 8 | 24 |

The last distance is to the after part of the stern \& 4 ft 2 in from that is the after part of the Balcony.
All the Breadths are taken from Outside to Outside of the timber.
The flat of the stern rakes 9 in in 4 feet \& the after part of the Balcony rakes 12 in in 4 feet; Poopdeck takes in the Mizzen Mast. After port 9 ft 6 in from the Rabbit of the Post, foremost post 22 feet from the side of the stern round the outside of Beam 7 Ft 10 In distance between the ports \& 14 ports, height of port sills 2 feet 5 In, ports fore and aft 3 ft 4 In , up \& down 3 ft 1 In

Center of the Fore Mast 18 ft 6 In abaft the Rabbit of the stern on the gundeck, Center of the Main Mast abaft the center of the foremast 70 feet \& the center of the Mizzen Mast 53 ft 3 in abaft the center of the Main Mast.

Height of the Crossbeam above the lower edge of the rabbit of the Keel 24 ft 7 In , height of the lower edge of the lower wale, at the fore end at the lower edge of the Rabbitt 20 ft 11 In. Length of the Transom (or the
length from the outside of the upper edge of lower wale where the Cross seam lays) 28 ft 2 In ; Rudder at the lower end 4 ft 6 In Wide, \& 7 pair of Rudder Irons, Sternpost at the lower end clear of the rabbit 23 In \& at the cross $10^{1 / 2}$ In, Keel thwarthsips 16 In. Projection of the Counter abaft the rabbit of the port on a Square 3 ft 10 In \& the lower edge of the Arch board at the upper edge the black streak, 3 Wales \& the black streak are 15 In each in lower moulding on the Arch board 6 inches \& the upper moulding $71 / 2$ in $\mathrm{w}^{\mathrm{d}} \& 16$ In between the mouldings, lower rim of the galery 11 feet long \& $31 / 2$ feet from the wide cathead outside of the nuckle 6 feet 18 In fore \& aft by 15 In .

Gangways 9 feet 9 in wide clear of the inside waste plank. 8 shrouds to the foremast \& the channel 2 ft 3 in wide, $271 / 2$ feet long, 9 shrouds for the main mast \& the channel 2 ft 6 in wide $351 / 2$ feet long; 6 shrouds to the mizzen mast \& the channel $181 / 2$ wide by 15 ft long. Channell wales $131 / 4$ in wide by 6 in thick, clamps 6 in

From the top of the deadwood to the top of the floor timber in the throat 21 in \& sided to $12 \& 1 / 2$ inches timber at the upper edge of the middle wale 12 in \& at the upper end 10 in . Keelson 12 in deep 20 in broad. Depth of the hold from the top of the floor timber to the top of the beam is 15 feet 9 inches; stern post at the head fore \& aft 22 in by 16 in; transom 18 in fore \& aft before the port \& jogled for the port [indecipherable] which makes it 28 in by 19 in counter timber at the keel 12 by 9 hold of beams 9 by 12 not kneed, 7 feet apart with 5 ledges of 4 in square between them, cable bitts 16 by $18 \&$ the cross piece 29 by 16 height of the fore castle from plank to plank 6 ft 10 in \& the beams 12 in square. Main hatch 7 ft 8 in fore \& aft by $71 / 4$ feet.

Diameter of double capstand 3 ft 10 in the spindle 23 in in the partners, water 7 in thick \& the running plank in the bottom is $41 / 4$ inches.

Lower deck beams 13 in sided 12 moulded, quarter deck beam 12 in square gundeck beams 15 in moulded \& 14 in sided, Hollop deck 6 feet below the lower deck from plank to plank, height between decks 6 feet 5 in. Height under the Qtr deck 6 ft 10 in hanging knees for the gundeck sided to 11 in \& lodging knees $91 / 2$.

The stem rakes as near as could be measured 15 feet.

[Labels added by transcriptionist for clarity]

1. $4^{\text {th }}$ or $\otimes$ Frame
2. $5^{\text {th }}$ frame
3. 3rd frame
4. $6^{\text {th }}$ frame
5. $2^{\text {nd }}$ frame
6. $3^{\text {rd }}$ or fore frame
7. $7^{\text {th }}$ frame
8. Fashion Pieces

Ft In

| Fore Frame | 13 | 11 | from the fore side of the stem |
| :--- | :--- | :--- | :--- |
| $2^{\text {nd }}$ | 16 |  |  |
| $3^{\text {rd }}$ | 25 |  |  |
| $4^{\text {th }} \otimes$ | 26 |  |  |
| $6^{\text {th }}$ | 23 | 5 |  |
| $7^{\text {th }}$ | 26 | 6 |  |

The South Carolina has 3 feet too much shear for a ship of war \& is too sharp at both ends \& too full in the middle which makes her strain \& hog accordingly.


Plan of the Bellesarius built in New England and reckoned one of the fastest sailing ships that swam the seas. 93 feet \& keel for tonnage 30 feet 6 in beam \& 15 ft 6 inches hold to her gundeck.

Height of the cross beam 15 ft 10 inches. Height of the lower edge of the lower wale at the stem 15 ft 4 inch stem rakes 15 ft 4 inches Stern post rakes $21 / 2$ feet. Length of the crossbeam 20 ft 4 inches.


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[Labels added by transcriptionist for clarity]

1. $2^{\text {nd }}$ frame or $\otimes 20$ feet abaft the fore frame
2. $3^{\text {rd }}$ frame 20 feet abaft $\otimes$ or $2^{\text {nd }}$ frame
3. 4 frame 20 feet abaft $3{ }^{\text {rd }}$ frame
4. 5 frame 20 feet abaft $4^{\text {th }}$ frame \& 9 feet 10 in before the port
5. Fore frame 21 feet abaft the rabbit of the stem

Drawings of a new constructed wheel for stearing vessels




The description of a new constructed wheel for stearing vessels

Fig 1 represents a fore and aft view of the wheel frame \&c
$A A A A$ stand for the wheel, $B B B B$ the wheel, $C C$ the barrel of the wheel, $D$ the lower cross box for the axletree to work in $E$ upper crossbox to confine the axletree down, $F$ the axletree, $G$ an iron barr that goes over the head of the iron plates, $\boldsymbol{H} \boldsymbol{H}$ and is for locked closed down to prevent the upper box from raising. $\boldsymbol{H} H$ iron plates to strengthen the frame as well as to secure the axletree from raising. $\boldsymbol{H} \boldsymbol{H}$ four forelock bolts to secure the frame of the wheel to the deck, fitted in the sill, that in case any accident should happen the wheel a tiller may be fixed immediately.

Fig $2^{\text {nd }}$ represents a horizontal view of the behind $B B$ the wheel, $C$ the barrel of the wheel, D the axletree
$E$ the neck of the axletree that works in the stand or frame for the wheel, $\boldsymbol{E}$ the nuts or cogs of the axletree (five in number) that work in the cogs of the iron segment of the circle GG containing 18 cogs on the face or upper edge as represented in Fig $3^{r d}$. D the nuts or cogs on the axletree which when turned moves the iron segment $G G$ from side to side. $H$ a brass friction wheel to support \& keep the iron segment from pressing below the cogs of the axletree $\boldsymbol{D}$. Fig $2^{\text {nd }}$ Iron arms $\boldsymbol{H}$ which goes round the rudder head and supports the iron segment which communicates the motion to the rudder head. Those arms are kept together by an iron hoop $K K$ as represented by dotted lines, before the rudder and is put on afterwards wedged very tight the other section of this hoop is seen in Fig 4th. $L$ the rudder head $M M$ an iron strap that receives an iron swivel through and in which the after end of the spindle is fixed and works. The fore and view of winch is seen by Fig 5 th and $N$ is the hole in the swivel in which the end of the spindle works.

Fig $\boldsymbol{6}^{\text {th }}$ shews a side view of the machine $\boldsymbol{A}$ the stand or frame for the wheel, $\boldsymbol{B B}$ the wheel, $\boldsymbol{C}$ the barrel, $\boldsymbol{D}$ the axletree, $\boldsymbol{E}$ the nuts or cogs of the axletree, $\boldsymbol{F}$ the iron arm that communicates the motion to the rudder head. $L$ the rudder head $M$ the iron strap through which the swivel $N$ passes, $N$ an iron swivel to receive the end of the spindle. $\boldsymbol{O}$ two staples to secure the arms on the rudderhead on each side and to keep them steady.

This machine may be inverted to the aft side of the rudder to answer the same purpose, when there is sufficient projection at the stern of the ship and will take up much less room.

If any objection should be made to the junking of the wheel it may be fixed without cogs by making a barrel of the same size as the cogs of the axletree on which fix your tiller ropes letting one end of each rope pass through an eye at the end of each arm and to sett up with a lanyard, to find the size of your tiller rope you must say, as the common length of your tiller is to the common size of your rope, so is the length of the iron arm from the center of the rudder to the size of the rope required. If a tiller of 12 feet in length requires a 3 inch rope then a tiller of 4 feet will require three times as much strain on the rope consequently it must contain three times the quantity of hemp or flax.

The Frigate Delaware had $1 / 4 \& 1 / 16$ hang of the shear to 1 foot in length round the half breadth from the stem to the transom.

Proportion for mainmast - To find the length of the main mast of a ship multiply the moulded breadth by 24 and divide by 10 for its length *This makes the mast too long. Again $13 / 4$ of the beam added to $1 / 5$ of the keel fors ${ }^{1}$ rabit will give the length of main mast.

Dimensions for the Masts, yards \& spars of a Frigate of 44 guns, whose length of keel is 147 feet. Straight rabbet, extream breadth of beam 43 feet, depth of hold 14 feet, depth of waist, between decks 13 feet.

As the extream breadth of beam of a ship is proportional to the Length of her keel, so is the length of the masts \& yards calculated according that that breadth but as the formation of all Vessels bodies differ according to the purpose for which they are intended, it is absolutely necessary to vary in the mode of calculating the dimensions of the Spars, according to the Construction of the Body. The Diameter of all Spars here under the denomination of Masts are intended to be one inch in the partners to three feet in Length, \& that of the yards are one inch in the Slings to four \& three quarters feet in Length. The Mizzen Mast excepted that is calculated one inch to four feet \& the Bow Sprit is the same size of the fore mast.

As the main mast, main yard and Extream breadth of Beam are here given, as the basis from which all the proportions are found - to find the Length of the main mast, I take twice the breadth of beam \& $1 / 6$ of the same \& add them together thus Breadth of beam

43 feet
$\times 2$
6) 86
14.4
the whole length of main mast
100.4
and to find the length of the main yard, I take twice the breadth of the beam thus

The whole length of main yard

43 feet
$\times 2$
86 feet

The studding sail booms \& small spars, not inserted here, must be regulated by the mast \& yards, according to the plain \& general rule.

NB to find the diameter of the mizzen top mast, or the top gallant masts, deduct off the partners and divide the length of the mast, from hound to heel, by 3.

The same principles of masting will answer in proportion for the thirty six gun frigates

|  | Ft | In |  | Foot |
| :---: | :---: | :---: | :---: | :---: |
| Main mast whole length as calculated | 100 | 4 | head | 13 |
| 1/13 deduct from main mast \& the remainder |  |  |  |  |
| gives the whole length of foremast | 92 | 8 | head | 13 |
| Mizenmast the length of foremast | 92 | 8 | head | 10 |
| Main yard whole length as calculated | 86 | 0 | arms | 4 |
| 1/20 deduct from mizzen yard \& the remaining |  |  |  |  |
| Crossjack yard $1 / 4$ shorter than foreyard | 61 | 4 | arm | 3 |
| Bowsprit $1 / 3$ shorter than foremast | 61 | 10 |  |  |
| Gibboom $1 / 4$ shorter than bowsprit | 46 | 5 |  |  |
| $3 / 5$ of main mast is the main topmast | 60 |  | head | 8 |
| $1 / 20$ deduct from main topmast \& the |  |  |  |  |
| remainder is the whole length of foretopmast | 57 |  | head | 8 |
| $2 / 3$ of mizzen mast is pole mizzen topmast | 61 | 9 | head | 19-9 |
| $4 / 5$ of main topmast is the main top gallant | 48 | 0 | head | 16 in |
| $4 / 5$ of foretop g mast is the foretop gallant | 45 | 7 | head | 15 in |
| Difference between $1 / 3 \& 1 / 4$ taken from the main yard gives the length of main topsail yd | 60 | 11 | arms | 5 |
| Difference between $1 / 3 \& 1 / 4$ of taken from the main |  |  |  |  |
| $1 / 4$ taken from main top gallant gives the main top gallant royal yard | 32 | 6 | arms | 1/2 |
| Diffns between $1 / 3 \& 1 / 4$ taken from foreyard gives the length of fore topsail yard | 51 | 11 | arm | 5 feet |
| Diff ${ }^{\text {ns }}$ between $1 / 3 \& 1 / 4$ taken from foretop |  |  |  |  |
| $1 / 4$ taken from fore top gallant yard gives the fore top gallant royal yard | 30 | 10 | arms | $11 / 2$ |
| Diffns between $1 / 3 \& 1 / 4$ taken from the crossjack yd gives the length of the mizzen topsail yard | 43 | 5 | arms | $2^{1 / 2}$ |
| Diff ${ }^{n s}$ between $1 / 3 \& 1 / 4$ taken from mizen topsail yard gives the length of mizen topsail yard | 115 | 5 |  |  |
| Spanker or mizzen boom one \& one third the length of gaff | 57 | 11 |  |  |
| Ensign staff $1 / 4$ shorter than mizzen topsail yard | 32 | 7 |  |  |
| Jack Staff half the length of ensign staff | 16 | 3 |  |  |
| $1 / 2$ the breadth of beam \& 1/20 of the beam is the |  |  |  |  |
| Width of main top | 23 | 7 |  |  |
| $1 / 2$ of the beam is the width of fore top | 21 | 6 |  |  |
| $2 / 3$ of main top is the width of mizzen top | 15 | 8 |  |  |

NB In ships of the line you add the depth between the additional deck to the lower masts, the sprit sail yard is the same as the fore top sail yard, the sprit sail top sail yard the same as the fore top gallant yard


Signed Thomas Truxton
Letter to T. Truxton disputing calculations

## Cap ${ }^{n}$ Thomas Truxton

## Dear Sir

I have considered the principles by which you have calculated the masts \& yards for the frigates \& of the opinion they are just as to the length but the bigness vary. Mizen masts should not exceed an inch to 4 feet, top gallant masts 1 inch to 4 feet. Bowsprits 2 inch to 1 foot in length, but when I examine the principles respecting the yards I cannot help differing from you for the following reasons. That it is evident a longer ship (supposing her breadth and depth the same) than a shorter one will require longer yards, though the masts would be the same. Therefore in order to find the main yard, multiply the length of the gun deck by .525 which will find the length of the main yard.

Instance the gun deck 173
.525
865
366
865
90.825
12
99.00

8
7200
These proportions may do for the main yard of a frigate but will not anywise for a double decked ship
Then I find the main yard should be 90.825 feet, or 90 feet 9 inches $7 / 8 \& 200$ parts of $1 / 8$ of an inch. I think when you examine this rule you will be convinced of its propriety, to find the length of the main top gallant yard multiply the length of the main yard by 48 will produce 43, , 686 feet or 43 feet 8 inches $1 / 8 \& 836$ parts of an eight. When these are found the other spars may be produced by your rule ascertain truly \& systematically the length of yard arms which are the principles you must take the depth of the lower reef which I believe to be about one third of which would be the distance the lower reef will hall out \& allow no more than sufficient outside the sheave to contain the eye bold in the yard arm. It is found necessary from the size \& weight of canvas to vary the size of the yards lower yards should be 1 inch to 5 feet.

One general rule has been observed with respect to bowsprits to take the length of the beam for its length outboard but when a vessel is very sharp forward. I think they should be something shorter, in finding the length of the main mast I would suggest the idea of describing the method by saying double the beam added to $1 / 3$ of its length will give its height.
[Transcriptionist Note: the above letter seems to be from Joshua Humphreys, the Memorandum below is apparently from Thomas Truxton (note the signature) explaining why there was a difference.]

Memorandum
The omissions to which you refer was omitted by copying. I have however interlined them \& of course you only differ with me as to the yards in which I am convinced you think improperly on that subject, for nothing can be more detrimental to a ships sailing than over square yards for the reasons I have verbally given you.


Joshua Humphreys Notebook

Proportions for Masts \& Yards
$4 / 5$ of the extream breadth is the length of main mast in yards
Main yard $7 / 8$ of main mast

Do top mast $3 / 5$ of main mast
Do yard $5 / 7$ of main yard
$\mathrm{D}^{\circ}$ Top gallant mast $\quad 1 / 2$ main top mast These are bad
Foremast
Do top mast
Do Top gallant mast
8/9 of main mast proportions

Fore Yard
$\mathrm{D}^{\circ}$ Top sail yard
Do Top gallant
$3 / 5$ of fore mast
$1 / 2$ of fore top mast
$7 / 8$ of main yard
$5 / 7$ of fore yard

Mizen Mast
3/5 fore top sail yard
$4 / 5$ of main mast
Do Top mast
Cross Jack yard
$5 / 7$ of main top mast

Gaff
$3 / 8$ of main yard
Bowsprit
$1 / 2$ mize mast
3/5 of main mast
Jibboom

Diameter of masts \&c
All masts to be $7 / 8$ of an inch to every yard in length, except mizzen mast

| Yards | $5 / 8$ of an inch to $\mathrm{D}^{\circ}$ which is $3 / 4$ |
| :--- | :--- |
| Bowsprit | $13 / 8 \mathrm{D}^{\mathrm{o}}$ |

Twice the beam \& $1 / 9$ of the keel straight rabbit added together for the length of ships main mast

## Dimentions of Mould Lofts

Mr. Perrys mould loft at Blackwell is in length
Mr. Clewleys at Gravesend $\mathrm{D}^{\circ}$
Mr. Masters Rotherdale

120 feet by 50 feet
100 by 50
80 by 40

This latter gentleman could not get his mould loft built larger as he was confined for room
Particular Dimentions of Schooner [indecipherable name]
Centers of the mast 15 feet 10 inches abaft the aft side of the apron and center of the main mast 28 feet 3 inches abaft. The center foremast dead rising 22 inches to 10 feet from transom, $91 / 2$ feet tuck from the upper part of the wale 3 feet the lower part of the tucks 8 feet 4 inches from the bottom of the keel, agreeable to the draught of water marks.

Dimentions of Ship Stern

|  | Feet | Inches |
| :--- | :--- | :--- |
| Length of gun deck from apron of stern | 120 | 6 |
| Keel for Tonnage | 95 | 6 |
| Extream Breadth | 32 |  |
| Depth in the hold | 10 | 6 |
| Height of wing transom | 17 | 1 |
| Do Lower wale to upper edge forward $_{\text {Midships }}^{14}$ | 1 |  |
| Abaft | 12 | 2 |
| Built by Thomas \& James | 16 | 9 |
| Breadth of Wing Transom |  |  |
| Rising Midships Flat including Hollow Floor | 18 |  |
| Half Breadth of Floor | 1 | 7 |
| Tumbling Home of Top Timber | 1 | 3 |
| Hanging of Gun Decks | 2 | 9 |
| Ditto at Middle | 1 | 10 |
| Height between Decks | 1 | 6 |
| Waist at Midships | 4 | 6 |
| Port Sills from the Deck | 3 |  |
| Up \& Down in the Clear | 1 | 10 |
| Width fore \& aft | 2 | 2 |
| Disance berm Pors | 2 | 4 |

Distance between Ports
Number of Bits on Gun Deck 12 Exclusive Beak head

Proportions of the French Frigate of Danae Masts of 32 gun

| English Measure | length <br> Ft:in:line | diameter |
| :---: | :---: | :---: |
| Main Mast | 90:6:4 | 2:6:1 |
| Mizzen Mast | 67:-:- | 1:8:3 |
| Main Top Mast | 36:1:3 | 1:4:1¹/2 |
| Fore Top Mast | 36:1:3 | 1:4:11/2 |
| Main Gallant Mast | 43:2:9½ :8: $7^{1 / 2}$ |  |
| Fore Gallant Mast | 43:2:9½ :7:91⁄2 |  |
| Main Yard | 84:2:71/2 1:8:3 |  |
| Main top yard | 59:3:81/2 | 1:6:11 |
| Fore top yard | 59:3:81/2 | 1:6:11 |
| Cross Jack yard | 36:1:3 | :11:101/2 |
| Mizzen top yard | 38:1:3 | $1: 6: 11^{1 / 2}$ |
| Main gallant yard | 38:1:3 | :6:11¹⁄2 |
| Fore gallant yard | 38:1:3 | :6:11¹⁄2 |
| Mizzen Gallant yard | 21:6 | :5:41/2 |
| Main Royal yard | 23:9 | :4:10 |
| Fore Royal yard | 23:9 | :4:10 |

## Ship London Packett

75 feet keel 27 feet Beam $111 / 2$ feet hold \& $51 / 2$ feet between Decks Main Mast 62 feet Main Yard 50 feet

Proportions of Masts \& Yards
Double the Beam \& $1 / 9$ of the Rail is the length of the main mast.
Main top mast $3 / 5$ of the Main Mast
Main top gallant mast $1 / 7$ of the top mast
Fore mast 9/10 of the main mast (too short say 12/18)
Fore top mast $3 / 5$ of the fore mast
Fore top gallant mast 6/7 of the top mast
pole Mizzen mast same length as the fore mast
pole Mizzen top mast 2/3 of the mizzen mast
if no pole take half the length of main mast
Main Yard one \& 6/7 of the [below]
Main topsail yard $3 / 4$ of the main yd
Main top gall t y $7 / 11$ of the topsail yd
Foreyard 12/13 of the main yard
Foretop sail yard 5/7 of the fore yard
$5 / 7$ fore top gall ${ }^{t}$ yd $5 / 7$ of the topsail yd
Cross jack yard $3 / 4$ of the main yd
Mizen topsail $\mathrm{yd}^{3} / 4$ of the main topsail yd
Mizen top gallant $y^{3} / 4$ of the main top gall ${ }^{t}$
Royal yd $3 / 4$ of their respective top gall ${ }^{\mathrm{t}}$
Bowsprit (outboard) the length of the beam
Main top ${ }^{11 / 2}$ the breadth of beam
Foretop 7/8 of the main top

| Mizzen topmast $1 ⁄ 2$ <br> of the |
| :--- |
| mizzen mast |

Main top $3 / 4$ of the main top
Sprit sail yard same length as the fore topsail yard
Sprit sail topsail yard the same as the fore topgallant yard
Gibboom one and $1 / 6$ of the beam
Main \& foremast heads $3 / 4$ of their respective topmasts
Main mast head $6 / 4$ of their respective top gallant
masts first deducting the poles. This proportion gives the top mast head $6 / 3$ of the top gallant masts is the pole of the same

United States Ship Delaware $721 / 2$ keel 28 feet beam. Main mast 64 \& main yard 56 feet
United States Brig Scammel 57 feet keel 20 feet 6 beam

## Weights of cubic foot of different woods

Weight of a cubic foot of live ash when cut three months eighty one pounds being kept in a counting house one year it weighs 70 lbs weight
$\begin{array}{ll}\text { Weighed in March } 1795 & 81 \mathrm{lbs} \\ \text { D }^{\circ} \quad \text { in February } 1796 & 70\end{array}$
Weight of a cubic foot of white pine taken green $40 \mathrm{lb}^{1 / 2} 2$
Weight of a cubic foot of white oak dry 54 lb

Principal Dimentions of his Britannic Majesty's ship Squirrel, mounting 22 twelve Pounders on her gun deck \& 10 ---- Pounders on her quarterdeck \& forecastle, In all thirty two guns

|  | Ft | In |
| :--- | :--- | :--- |
| Length of gun deck | 119 feet |  |
| D $^{\circ} \quad$ keel for tonnage | 98 | $91 / 4$ |
| Breadth extream | 32 | 9 |
| Doulded $^{\circ}$ mould | 32 | 3 |
| Depth of hold | 10 | 3 |
| Burthen in tons | 563 | $46 / 94$ |

This ship is said to sail remarkably fast

## Dimensions of ships of war calculated to carry 44, 36 \& 38 guns

Number of guns on main gun deck
Weight of metal
Length of gundeck between perpendicula Length of keel for tonnage
Moulded breadth of beam
Depth in hold
Height between decks
Height from gun to upper deck
Carpenters tonnage by the olde mode 1178 90/95

The above for a ship of 44 guns
SH

Dimensions of a Ship to carry 38 guns
Number of Guns on gun deck
Weight of Metal
Length between the perpendicular
Length of keel for tonnage
Moulded breadth of beam
Depth in the hold
Height between decks
Height from gun to upper deck
Carpenters tonnage by the olde mode
Dimensions of a Ship to carry 36 guns
Number of guns on gun deck
Weight of metal
Length between the perpendicular
Moulded breadth of beam
Depth of Hold
Height between decks
Do from gun to upper deck
Carpenters tonnage by the olde mode
120 feet keel

## 30

18
1676
$6 \quad 9$
too little beam 1822 S Humphreys


Dimensions of Masts \& Spars of Brig Venus of 60 feet, keel 22 feet, beam 12 ft 5 in to upper deck.

|  | Feet | In |  | Feet | In |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Main Mast | 56 |  | head | 7 |  |
| Top mast | 27 |  | head | 3 | 9 |
| Main top gallant mast | 23 |  | head | 8 |  |
| Fore mast | 46 |  | head | 6 | 6 |
| Topmast | 29 |  | head | 4 | 0 |
| Top gallant mast | 25 |  | head | 9 |  |
| Cross jack yard | 38 |  | arms | 1 | 6 |
| Main topsail yard | 30 |  | arms | 1 | 6 |
| Top gallant yard | 18 |  | arms | 1 |  |
| Royal yard | 12 |  |  |  |  |
| Fore yard | 42 | 6 | arms | 2 |  |
| Topsail yard | 32 | 6 | arms | 1 | 3 |
| Royal yard | 16 |  |  |  |  |
| Bowsprit outboard | 20 |  |  |  |  |
| Jibboom | 24 |  |  |  |  |
| Main Gaff | 22 |  |  |  |  |
| Boom | 50 |  |  |  |  |

[Scan of signature]
Dimensions of Schooner Gosport
$541 / 2$ feet keel
Twenty one feet 9 inch beam
Ten feet hold

Principal Dimensions of the Frigate Philadelphia built by S. Humphreys

|  | Feet | Inches |
| :--- | :--- | :--- |
| Length of gun deck | 157 |  |
| Keel for tonnage | 136 |  |
| Beam moulded | 39 |  |
| Depth of hold | 13 | 6 |
| Height between decks | 6 | 0 |
| Height between gun \& upper deck | 6 | 9 |

Measuring 1040 tons

To find the strength of new rope:
Square the circumference \& divide that product by five, which will give the weight in tons a rope will bear. Suppose a five inch rope, the square of which is 25 , that divided by five will give 5 tons.

Note: It appears to me this notion will not hold good, I think a rope of five inches will not carry 5 tonnes.

J Humphreys Nov. 4, 1804
Capt Wm Jones Proportions for Masting Frigates
Twice the beam \& depth of hold for the length of main mast
Main yard $8 / 9$ of the main mast
Main topsail yard 5/7 of main yard
Main topgallant yard 2/3 of main topsail yard
Main Royal yard $1 / 2$ of main topsails yard
Main topmast $3 / 5$ of main mast
Main top gallant mast $4 / 5$ of main topmast
Pole of the top gallant mast $2 / 5$ of the whole length
The foremasts \& yards are $9 / 10$ of the mainmast \& yard
Mizenmast $8 / 9$ of the main mast
Mizen top mast $3 / 4$ of main topmast
Mizen top g_mast $4 / 5$ of mizzen topmasts
The fore \& main mast heads $1 / 7$ of the whole length
Main fore \& mizzen topmast heads $1 / 8$ of their respective length
Mizenmast head 1/9 of whole length
Diameter of the masts $9 / 10$ of an inch to every yard in length which is the British Rule for all ships from 50 to 32 guns inclusive.
Diameter of the yard 7/10 of an inch for every yard in length.

Cost of a pilot boat the Joseph Sims built down the River by Flanigan \& Sons 31 93/95 tons
33 feet 9 inches. Keel 15 feet 2 inches Beam 5 ft 1 in Hold

| Carpenter bill 600 | Joyner 70 | Cordage 211 yards | 881.28 |
| :--- | :--- | :--- | ---: |
| Canvas sail maker 29289 | Blacksmith 130 |  | 422.89 |
| Anchor 40 | Mast maker 46 | Boat builder 52 | 138.00 |
| Runs for launching 10 | Fitting 5 | Rigging \& leather 3 | 18.00 |
| Paint \& putty 12 | Hoops \& Hanks 1356 | Serapor 5 | 30.56 |
| Plumber 1467 | Cambrose 8 | Water casks 12 | 34.67 |
| Spyglass 15 12 | Blockmaker 20 | Stove 12 ${ }^{82}$ | 37.94 |
| Cabin Furniture 11 | [burger] 6 | Painter 8 | 25.00 |
| Compass 7 | Oakum 4 | Ballast board 4 | $\underline{17.00}$ |
|  |  |  | 1605.34 |

This boat was built - say in the early part of 1807

## Dimensions \& Cost of Sloop Diana built by Joseph Grice for a New Castle Packet 1807

Keel St Rabbit Beam Hold

| Joseph Grice his bill | 1800.00 Doll |
| :--- | ---: |
| P Brown Blacksmith | 707.18 |
| P Brown Sons for lumber | 10.30 |
| John [indecipherable] (Mast maker) | 142.77 |
| Lewis [indecipherable] (Ship joyner) | 435.00 |
| [indecipherable] Wilson (Boat builder) | 61.30 |
| [indecipherable] Shreeve (Rigger) | 42.34 |
| Ludlam \& Voight (Plumber) | 70.40 |
| D King (Brass foundry) | 12.75 |
| Rush (Carver) | 3.00 |
| Fling (Painter) | 120.00 |
| Reynolds (Cooper) | 6.25 |
| Fish (Ironmonger) | 69.28 |
| Atherton \& Boker Do 8 24/100 | 8.24 |
| Crockery Ware | 26.40 |
| Davenport (instrument maker) | 2.25 |
| Wainwright (Blocks maker) | 83.06 |
| Gaw (Chair maker) | 50.44 |
| Looking glass | 14.00 |
| 143 $1 / 2$ bushels of salt | 127.60 |
| Cordage \& Ships Chandling | 711.13 |
| Cordage at this time was 16 dollar per CWT |  |
| 12 piece Holland Duck at 24 dollar | 288.00 |
| 10½ D Linen Duck at 15 | 157.50 |
| 1 piece Holland duck | 25.00 |
| Sail Maker | 107.56 |
| [Can Boom] | 33.25 |
| 2 ton pig iron | 72.00 |
| Cabinet maker | 143.50 |

The whole cost of this packet was (exclusive of the cost of coppering) 6470 dollars. The coppering was say 1000 Dolls coppered to a sailing trim mark. There is a number of other charges against the packet such as mattress, blankets, sheets \&c. which it was not considered necessary to put down here.
\(\left.\begin{array}{ll}Dimension of Schooner Stag \& <br>
Her spars \&c. Pilot boat built \& 72 feet keel 23 feet beam <br>

Mainmast 73 feet \& Topmast 30 feet Pole 13\end{array}\right]\)| Foremast 70 feet | Topmast 40 feet Pole 16 feet |
| :--- | :--- |
| Fore gaft $261 / 2$ feet | main gaft 23 feet |
| Bowsprit (outboard) 12 feet - too short <br> Gibboom 30 feet | Flying gibboom 12 feet |
| Main Boom 58 feet |  |
| Foreyard 46 feet | foretopsail yard 32 feet |
| This vessel was built by John Wilson for John Allen in the early part of 1808. |  |

Dimensions of the Schooner Chance
Belonging to Nixon \& Walker
$471 / 2$ feet \& keel 20 feet 3 inches, beam 8 feet 4 inches, hold full built- - -
Main mast 58 feet head 7 feet Topmast 18 Pole 5
Foremast 55 feet head 7 feet Topmast 24 feet head 7 feet
Foreyard 30 feet arm 15 inches Topsail yard 20 feet arm 15 inches
Main boom 44 feet Gafts 22 feet each Gibboom 27 feet
Bowsprit (outboard) 15 feet
This schooner was built down the river
Cost of Schooner Humble built by J Humphrey \& Sons
For Cap' Quinn \& Strandridge
Joshua P Humphrey \& Sons bill for hull \& frame ..... 1127.25
Adam [indecipherable] for iron work \& anchors ..... 367.52
Joiner complete ..... 130
Plumber ..... 77
Boar builder ..... 63.08
Painter ..... 32
Scraper ..... 8
Rope maker \& ship chandler ..... 420.17
Block maker ..... 72.40
Sail maker ..... 117.21
Canvas ..... 491
Rigging 2120/ ${ }_{100}$ Compass 8 naval stores $11^{15}$ / 100 ..... 40.35
Wharfage 20, Launching expense 50, colors 20, portage 10 ..... 100Ballast \& pig iron$\underline{200.00}$3185.98
The above was the Schooner Humble
Ready to take in @ cargo Built in the summer of 1800

## Dimension of the Queen Charlotte

$\left.\begin{array}{lll}\begin{array}{l}\text { Length on the range of the lower gundeck from the } \\ \text { rabbit of the stern to rabbit of stern port }\end{array} & & \\ \text { Length from the aft part of the fife rail to the fore } \\ \text { part of the figurehead }\end{array}\right)$

Guns
Upper deck 30 twelve pounders
Middle deck 30 twenty pounders
Lower deck 30 thirty two pounders
Quarter deck 2 twelve pounders
Forecastle 2 twelve pounders
Round House 6 eighteen pounders
Burthen 2270 tons

Dimension of Brig US Nautilus captured by The British in 1812
64 feet keel straight rabbit 23 feet beam
11 feet hold 87 feet between perpendiculars

| Main mast | 55 feet | head 9 feet | diameter 18 inches |  |
| :---: | :---: | :---: | :---: | :---: |
| Foremast | 50 feet | head 9 feet | $\mathrm{D}^{\text {o }}$ | $171 / 2$ |
| Main \& fore topmasts $301 / 2$ feet head 5 feet |  |  | $\mathrm{D}^{\text {o }}$ | 91/2 |
| Main \& fore | $\mathrm{g}^{t}$ mast | pole 12 ft | D ${ }^{\text {o}}$ | 51/2 |
| Main top ya | 48 feet | arms 2 feet | $\mathrm{D}^{\circ}$ | 10 |
| $\mathrm{D}^{\circ}$ top | 36 feet |  |  |  |
| $\mathrm{D}^{\text {o }}$ top | d 24 ft | D ${ }^{\circ} 12$ inches | $\mathrm{D}^{\text {o }}$ | $51 / 4$ |
| $\mathrm{D}^{\circ}$ roy | d 16 | $\mathrm{D}^{\text {o }}$ | $\mathrm{D}^{\text {o }}$ | $31 / 4$ |

Bowsprit whole length 32 ft outer end 21 ft bed 17 inches
Gibboom 26 feet diam $81 / 2$ flying gibboom 28 diam 6
Main boom 48 ft diam 10 gaft 31 ft diam 10 inches

Navy yard Washington June $2^{\text {nd }} 1809$
Signed
A Sinclair

Rules for masting Frigates 1809

For placing masts

Foremast $1 / 7$ of spar deck from forward
Main mast $2 / 7$ and $6 / 7$ of $1 / 7$ of spar decks rom the foremast
Mizenmast $1 / 7$ and $2 / 3$ of $1 / 7$ of spar deck from mizenmast

Length of Masts

Main mast $281 / 3$ the extreme breadth of the ship
Foremast 10/11 of the main mast
Mizen mast $7 / 8$ of main mast
Main top mast 11/18 of main mast
Foretop mast 15/16 of main top mast
Mizen top mast 7/8 of foretop mast
Top gallant mast 9/17 of their respective topmasts exclusive of Pole -
Royal mast from topmost cap 1/10 hounds of top gt mast -
Skyscraper masts $3 / 9$ of their royal masts above royal mast head when lowered down to step on top mast caps

Length of Yards
Main yard 10/11 of main mast
Foreyard 7/8 of main yard
Crossjack yard 9/10 of fore yard
Topsail yard $3 / 4$ of their respective lower yards
Royal $\mathrm{D}^{\circ} 2 / 3$ of their topgallant yards
Sky scraper $2 / 3$ of their royal yards
The steering sail yard $4 / 7$ of their boom
Spanker boom same as bowsprit
Gaft same as main topsail yards
Bowsprit $11 / 2$ the breadth of beam
Gibboom 4/5 of bowsprit
Flying gibboom to go outboard 2/3 of what the
Gibboom is outboard the heel to come to bowsprit cap
a nonsteering swinging boom 6/9 of main yards
$D^{\circ} \quad D^{\circ} \quad D^{\circ} \quad$ yards same as main top mast
Steering sail yards
Steering sail boom $1 / 2$ of their respective yards to which add $1 / 20$ of their length for length of steering
sail boom yard
Ringtail boom same as main top $\mathrm{g}^{\mathrm{t}}$ yard
Length of Mast Heads
Main \& foremast $1 / 6$ of their length
Main heads \& topmast $51 / 2$ inches for every yard in length
Length of yard Arms
Main \& Foreyards $1 / 20$ of their length
Crossjack yd sail yards $1 / 12$ top gallant $1 / 17$

Royal yards $2 \& 1 / 2$ their diameter in sling
Top sail yards the same All steering s ${ }^{1} \&$ yds twice their diameter
Main \& fore masts $\quad 15 / 16$ of an inch to every year in length
Main mast $\quad 3 / 4 \mathrm{D}^{\circ} \quad \mathrm{D}^{o} \quad \mathrm{D}^{\circ}$
Main \& main topmast $\quad 15 / 16 \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$
Foretop mast same as main top mast
Main \& mizzen top $g^{t}$ masts 1 inch to every yard in length
Foretop gallant mast same as main top gallant mast
Royal masts $3 / 4$ of their top gallant mast
Skyscraper mast 4/5 of the royal

## Diameter of yards

Main \& foreyards $\quad 7 / 10$ of an inch for every yard in length
Crossjack yard same as main top s ${ }^{1}$ yard
Topsail yard $\quad 2 / 3$ of an inch to every yard in length
Top $G^{t}$ Royal \& sky sail yards $5 / 8$ of an inch $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$
Sprit sails yd spanker boom same as foretops' yd
Gaft same as main topsail yard
Bowsprit same as main mast
Gibboom 7/8 of an inch to every yard in length
Flying gibboom $13 / 8$ of an inch to every yard outboard
Steering sail boom 1 inch to 5 feet
Ringtail boom 1 1/8 inch to 4 feet
Do yard
Swinging boom 1 inch to 6 feet
Martingale $1 / 2$ the length of gibboom outboard
Below the bowsprit cap to be made double
Dimensions of spars of US Frigate President

## Main Mast

Fore Mast
Main Mast This mast must have [slope] on the Orlope
Main topmast (exclusive of heel block)
Fore topmast $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Mizen topmast $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Main topgallant mast exclusive of pole
Fore $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Main $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Main Royal Mast
Fore $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Mizen $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Main skyscraper mast
Fore $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$

| Whole |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Length | Pole |  | Head |  |
| Ft In | Ft | In | Ft | In |
| 1000 | 2 | $73 / 4$ | 16 | 11 |
| 914 | 2 | $41 / 4$ | 15 | 3 |
| 86 | 1 | 10 | 13 | 6 |
| 62 | 1 | 7 | 9 | 6 |
| 58 | 1 | 7 | 8 | 6 |
| 50 | 1 | 3 | 7 | $71 / 2$ |
| 33 | 1 | 1 |  |  |
| 306 | 1 | 1 |  |  |
| 26 |  | $51 / 2$ |  |  |
| 22 |  | $71 / 4$ |  |  |
| 204 |  | $71 / 4$ |  |  |
| 174 |  | 6 |  |  |
| 166 |  | $51 / 4$ |  |  |
| 153 |  | $53 / 4$ |  |  |
| 13 |  | $4^{3 / 4}$ |  |  |
| 921 | 1 | 0 | 3 | 10 |
| 80 | 1 | $63 / 4$ | 3 | 4 |
| 72 | 1 | $11 / 4$ | 6 |  |
| 69 | 1 | 3 | 5 | 9 |


| Foretop sail yard | 45 |  | 10 | 3 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Main top galltyard | 44 | 6 |  | $91 / 2$ | 2 |
| Fore $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$ | 40 |  |  | $71 / 2$ | 2 |
| Mizen Do ${ }^{\circ}{ }^{\circ} \mathrm{D}^{\circ}$ | 30 |  |  | $6^{1 / 4}$ | 1 |
| Main royal yard | 30 |  |  | $6^{1 / 4}$ | 1 |
| Fore Royal D ${ }^{\text {o }}$ | 26 | 6 |  | $5^{1 / 2}$ | 1 |
| Mizzen Royal Yard | 30 |  | $4^{1 / 4}$ |  |  |
| Main Skysail yard | 20 |  | $4^{1 / 4}$ |  | 9 |
| Fore Skysail yard | 18 |  | $4{ }^{1 / 4}$ |  | 8 |
| Mizzen skysail yard | 13 | 4 | $31 / 2$ |  | 7 |
| Sprit sail yard | 60 |  |  | $11 / 4$ | 5 |
| Bowsprit | 65 | 3 |  | $73 / 4$ |  |
| Jibboom | 48 |  |  | 2 |  |
| Flying Jibboom | 53 |  | $91 / 2$ |  |  |
| Spanker boom | 69 |  | $13^{1 / 1}$ |  |  |
| Gaff | 45 |  | 10 |  |  |
| Ring tail boom | 30 |  | $63 / 4$ |  |  |
| Ring tail yard | 15 |  | 4 |  |  |
| Lower Steering sail swinging boom | 50 | 2 | 10 |  |  |
| Lower steering sail swinging yard | 26 | 3 | $51 / 4$ |  |  |
| Main top mast steering sail boom | 47 | 6 | $93 / 4$ |  |  |
| Main topmast steering sail booms | 26 | 3 | $5^{1 / 4}$ |  |  |
| Fore topmast steering sail booms | 41 | 6 | $81 / 4$ |  |  |
| Fore topmast steering sail yards | 22 | 10 | 7 |  |  |
| Main top gt steering sail boom | 35 | 6 | 7 |  |  |
| Main top gt steering sail yards | 19 | 8 | 4 |  |  |
| Fore top gt steering sail boom | 31 |  | $61 / 4$ |  |  |
| Fore top gt steering sail yard | 17 | 1 | $33 / 4$ |  |  |
| Mizzen top gallant steering sail boom | 23 |  | $43 / 4$ |  |  |
| Mizzen top gallant steering sail yards | 13 |  | $23 / 4$ |  |  |
| Main royal steering sail boom | 23 |  | $4{ }^{3 / 4}$ |  |  |
| Main royal steering sail booms | 13 |  | $23 / 4$ |  |  |
| Fore royal steering sail booms | 20 | 9 | 4 |  |  |
| Fore royal steering sail yards | 12 |  |  |  |  |
| Mizzzen royal booms |  | 6 |  |  |  |
| Mizzen royal steering sail yards |  | m | ards |  |  |



Dimensions of Ship Madison Corvette
Built-Launched at Sacketts Harbour on the Lakes November 1812

| 112 Feet Keel | $321 ⁄ 2$ feet Beam $\quad 111 / 2$ feet Hold |
| :--- | :--- | :---: |
| 580 Tons | Mounts 24 thirty two pound Carronades |

1834 June 19 ${ }^{\text {th }}$ - Alter the rule for Schooners Masts so that the head of the main Topmast shall be as high as the main topmast Trestletrees if rigged as a Brig and half the topmast head.

This rule gives a maximum Main Mast. If half the topmast head be not added the length of the mast will be quite moderate.

## Proportions of Schooners

Main Mast
Take $1 / 3$ of the Keel at Rabbet
$1 / 3$ of the depth of Hold
Twice the Beam

Sept 1814 A Better Rule
\{Twice the Beam in moulded Breadth, one half the Keel at Rabbet from which Deduct/half the depth of Holdmakes a good Main mast.\}


## [TRANSCRIPTIONIST NOTE: The above lines were $x^{\prime} d$ out in the original journal pages but were clearly legible and so included here]

The Length of a Schooners Mast should depend on the depth. Shoal vessels should carry longer masts than deep ones \& hence by deducting the depth from any given proportion you make a better proportioned mast.

## The US Ship Franklin

On the $17^{\text {th }}$ of April 1813 Charles Penrose \& Samuel Humphreys were appointed by William Jones, Secretary of the Navy to make improvements in the Navy yard \& to build a 74 gun ship called the Franklin of the following dimensions VIZ
$155.0^{3} / 8$ Streight Rabbit 50 feet moulded beam 19 feet 6 inches. Hold 7 feet 2 inches between lower gundeck \& middle gun deck \& 7 feet between middle gundeck \& upper deck. No Round House.

The dimensions of this ship were altered from a draft drawn by Joshua Humphrey in 1799 \& the draft of this ship altered a little forward \& aft from the original draft. Her sheer was dropped at the upper wale 9 inches at each end-

This ships keel was in 5 pieces \& was sided 20 inches \& 23 inches deep, the top of rabbit was cut 1 inch below the top of the keel a deadwood of 7 inches was placed on the top of the keel. The throats of the floor timbers intended at first to be 22 inches were reduced to 20 inches on account of widening the ship this increased the depth of hold to 20 feet as the main hatch. The gundeck was raised at $\otimes 3$ inches from the old draft. This ships outside bilge Strake were 2 of 6 inches thick 2 of $51 / 2$ in $\& 2$ of 8 in $\& 1$ of 7 inches. The foot waling of 4 $\& 41 / 2$ inches. Her inside bilge strakes were 2 strakes of $81 / 22$ of 7 inches and 2 of 6 inches.

Her orlope deck clamps were 1 strake of $81 / 2$ and 1 of 7 inches thick - thick strake at $1^{\text {st }}$ futtock heads. Insides 1 strake of 7 inches \& 2 of 6 inches thick - Wale 5 strakes of 11 inches wide strake under the wale 7 inches thick Her frame principally of live oak The floor of timber live oak The $1^{\text {st }}$ futtocks excepting 3 on each side near P Q \& R were of mahogany 2 futtocks, $3^{\text {d }}$ futtock of live oak. $4^{\text {th }}$ futtock is of live oak top timber live oak.

This ship was called The Franklin
Main transom of mahogany in two pieces of mahogany
The improvement of the Navy Yard occupied a considerable time - a wharf was built, a blacksmith shop - a mould loft, a saw shed - a counting house, a mart yard \& the ground leveled, a large quantity of live oak near 100 pieces was brought from New York overland from Brunswick all of which did not arrive in the Navy Yard until the middle of Jan 1814.

The keel was laid Aug 7th 1813
The stem was raised on the $12^{\text {th }}$ day of August $1813 \&$ the stern raised on the $16^{\text {th }}$ day of August within the same year. The stern was raised without the main transom and weigh [---] tons [---] hundred to raise it one fall of white rope 9 inches with a pair of shears [---] feet long \& [---] feet \& 20 inches diam ${ }^{\mathrm{r}}$ at 4 feet \& [---] inches from butt end.

## TRANSCRIPTIONIST NOTE: [---] in the above and following paragraphs indicate a blank space in the original journal.

Another sett of carling blocks \& a fall of 6 inches was also used to assist in the raising of the stern.

Lower gun deck clamps 3 strakes 8 inches thick at top \& $6 \frac{1}{2}$ inches at bottom. Middle gun deck clamps 7 inches. Upper deck clamps 4 inches thick 3 strakes of strings \& drift 4 inches thick. Upper gun deck sperketting 4 inches.

On the $29^{\text {th }}$ day of August 1814 with the consent of the Navy Agent we suspended the work on 74 gun ship \& commenced working on gun carriages for Fort Mifflin \& other work for the defense of the port. On the $24^{\text {th }}$ day of September an order was received to discontinue the work on the ship and on the $27^{\text {th }}$ an order was given to recommence the work but on account of the want of funds it was put off until the $18^{\text {th }}$ day of October when the work was resumed.

The upper deck beams were sided 14 \& moulded 11 inches. Knees on this deck sided 8 inches \& bolted with 11/8 iron.

Upper gun deck beams sided 18 moulded 15 with knees sided 10 inches \& bolted with $11 / 4$ inch iron. Lower gun deck beams sided $19 \&$ moulded 16 . Knees sided 11 inches \& bolted with $11 / 4 \mathrm{inch}$. Orlope deck beams sided 16 \& moulded 14 bolted with 1 1/8 copper. Knees sided $9 \& 10$ inches.

On the $11^{\text {th }}$ day of December 1814 the upper deck being laid \& caulked. Plank sheats on \& the waist planked up. The work was suspended by an order of the Navy Agent. No other decks at this time were laid.

On the $25^{\text {th }}$ day of February, 1815 (Saturday) received an order to finish the ship ready for launching \& on the $21^{\text {st }}$ day of August at 10 minutes before 3 o'clock the ship was safely launched.
The descent of her keelway $3 / 41 / 16$ of an inch to a foot $\&$ the launching ways lay 1 inch above the bottom of the false keel at the stern port \& were 2 inches below the bottom of false keel

Width of launching ways at the fore block 18 feet
Play in 200 feet $\quad 18-85 / 8$ at $\otimes$. This lessened the descent of the ways \& lifted the ship as she moved. It took half an hour to sett the ship \& take out half her blocks.

There were 4 cross lashings at each end \& 2 lays upright - shores abaft the after blockings to support the ships buttock.

Draft of water when the ship was launched \& with no ballast
Height of the Franklin $4^{\text {th }}$ port from aft

| Aft | $17 . .2$ |
| :--- | :--- |
| Foreward | $13 . .6$ | out of water when launched 11-8 1/2

Height of Franklin $5^{\text {th }}$ port from forward out of water with no ballast 13.. 4

Draft of water of the US Ship Independence built at Boston with 35 tons of ballast on board Aft 19 feet Independence had no bowsprit in forward $14 . .6$

Height of Independence when launched with 35 tons of ballast aboard

| $4^{\text {th }}$ port from aft out of water | 10 feet |
| :--- | :--- |
| $5^{\text {th }}$ port from forward | 12 feet |

## Dimensions of Schooner Rollar Spars

Foremast 73 feet head 8 feet. Main mast 75 head 8 ft .
Bowsprit 17 outboard. Foretopmast 40 feet pole 15 feet.
Main top mast 38 feet pole 14 feet. Gibboom 41 feet outboard 24 feet
Flying gibboom 38 feet outboard 14 feet.
Foreyard 56 feet arms 2 feet top sl yard 38 feet arm 2 ft
Foretop gt yd 28 feet arms 12 inches. Royal yard 20 feet
Main yard 48 feet arms 18 inches. Fore s ${ }^{1}$ yd 30 feet arms 18 inches
Main top gt yd 16 feet. Fore gaft 28 feet main gaft 20
Topmast steering s ${ }^{1}$ booms 28 feet top gt booms 14 feet Fore gunter mast 43 feet main gunter mast 42 ft

Dimensions of Schooner Revenger Spars

Main mast 79 feet 8 feet head. Foremast 77 feet head 8 feet
Foreyard 61 feet arms 2 feet topsail yd 36 feet arms 2 feet
Topgallant yd 26 feet arms 12 inches. Royal yd 18 feet arms 9 inches
Main yard 56 feet arms 2 feet top sl yd 32 ft arms 2 ft
Top gt yd 24 arms 12 inches. Royal yard 16 ft arms 9 inches
Foretopmast 40 feet pole 14 feet gunter mast 37 ft
Maintop mast 36 ft pole 14 feet gibboom 40 ft outboard 24 ft
Flying gibboom 38 ft outboard 14 feet fore gaff 28 feet
Main aft 26 ft ringtail boom 26 ft Ring tail gaff 14 feet
Dimension of Schooner Rollar
Built by Benjamin Phillips
74 feet keel at rabbit
24 feet beam

## Joshua Humphreys Notebook

10 foot hold
Foremast 73 feet head 8 feet
Mainmast 75 feet head 8 feet
Dimensions of Schooner Revenger
98 feet on deck
24 ft 6 beam
11 ft 8 hold
Main Mast 79 feet
Foremast 77 feet

Dimensions of schooner hermaphrodite
built by Mr. Seguin 1814, bought by Savage \& Dryan and sold to the United States and called Prometheus
82 feet Streight rabbit
27 feet beam
11 feet 4 inches hold
Fore mast 62 feet Head 9 feet
Fore top mast 34 feet, head 5 feet
Top gallant mast 28 Pole 12 feet
Main Mast 83 feet head 8 feet
Main top mast 36 feet pole 12
Fore yard 50 feet arms 2 feet
Fore top sail yard 38 feet arm 2 feet
Fore top gallant yard 26 feet arms 7 foot
Fore royal 18 feet arms 9 inches
Main yard 48 feet arms 2 feet
Main top sail yd 26 feet arms 18 inches
Main top gallant yd 22 feet arm 12 inches
Main boom 58 feet Gibboom 38 feet pole 10 ft
Fore \& main gaft 30 feet

Dimensions of schooner built by Mr. Maynard \& bought by T. Reilly 1814
61 feet straight rabbit
20-8 beam
8-4 hold
Main Mast 63 feet
Top mast 25 feet
Gaft 25
Boom 45 feet
Fore mast 59 feet
Top mast 25 feet
Fore year 42 top sail yard 25 feet
Top gallant yd 18 feet gaft 25 feet
Square sale boom 36 feet


## Joshua Humphreys Notebook

Rules for making Gun Carriages
Brackett to be the thickness of the caliber
Axeltree to size of caliber - After axeltree twice the size of calibre in width
Top square of brackett half its whole length.
Half the width of after log
After side of forward axeltree under centre of trunnion
The centre of trunnion Hole to be twice the Diameter of trunnion from the fore end of brackett.
Length of brackett to be from Centre of trunnion to the end of pomillion \& twice the diam of trunnion added Breast Board to be kept fair with the top of port cill
Transom- the upper part to be under the Centre of trunnion \& the fore Part below to be kept fair with the fore part of axletree
Trucks- Thickness to be size of bore \& say 3 times the diameter of trunnion to be the diameter of truck The turned part of axeltree to be the same size as trunnion
For the height of bracketts allow the centre of the gun to be 3 inches below the centre of port and say the top of the bore to be in the centre of port

Commr Rodgin Rules for Mastings Jan 31815

To find the length of the main mast add twice the moulded beam to the length of the keel for tonnage of which product take $5 / 11$ for the length of the mast.
Fore Mast 9/10 of the Main Mast. Mizen Mast 7/8 of Main Mast.
For all Lower Mast Heads take $1 / 6$ of their respective masts.

For the diameter of Fore \& Main Masts in the main deck partners multiply the length of the mast in feet by 6 the product of which divided by 19 will give the Diameter in inches. This ratio is little less than one inch in circumference for every foot the masts are long.

For the Diameter of all Lower Masts at their smallest parts (say under the Hounds) or the neck allow $4 / 5$ of what they are in the main deck partner.

For the Diameter of the Mizen Mast in main deck partners (exclusive of the fish) allow one inch to every four feet in length.

For the diam of all mast heads (in the wake of trestletrees) allow $3 / 4$ of the diam of the sizes on the partners \& topmast in the cap. And for the mast heads in the wake of or under the cap $4 / 5$ of their dimensions of the trestle trees.

By the above rule the square of the trestle trees for the head of the topmasts will be in the clear exactly $3 / 4$ of the size of their respective lower masts in the partners \& at the same time allow sufficient substance at the mast heads to the square of the lower cap being exactly the same diam that the topmast are in the caps as also the top mast cap on their squares, exactly the same size of top gallant mast in the cap. All top mast heads at the upper part of 8 square of Hounds ought to be the same size that the top masts are in the Caps-

Note- The after part of the Mast heads in the Caps ought to stand perpendicular to the after parts of the square or holes in Trestle Trees. The Chocks therefore that form the forepart of the square of Trestle Trees ought to be as thin as the necessary strength will allow so as to admit of as little daylight between the [dowlings] as possible \& to assist which all the extra diameter of the heels of topmast \& top gallant masts fore \& aft in the trestle trees (over what the masts are in the caps ought to be left on the fore part of the masts.

For the length of the fore \& main top masts allow $6 / 10$ of the respective lower masts.
For the diameter of the main top mast (in the cap) allow at the rate $11 / 4$ inches for every four feet for their size in the neck $4 / 5$ of what they are in the cap.

For the length of the Mizzen top Mast allow 5/9 of the length of the mizzen mast provided the mizen mast steps on the keelson. But if it steps on the orlope deck allow $4 / 5$ of the extream length of the main top mast.

The diameter of mizen top mast in the cap allow at the rate of 2 inches for 7 feet. - By the before given dimensions it is calculated that the lower masts \& top masts are to be made of southern yellow pine consequently if northern white pine is used for lower masts a difference of $1 / 20$ more ought to be allowed. For the length of all top mast heads allow $1 / 6$ of their respective mast.
For the length of all top gallant masts from the Heels to the upper part of the shoulders or Hounds allow exactly one half of the length of the respective top masts to which they belong.

For the diameter of top gallant masts in the caps allow at the rate of $1 \& 1 / 10$ Inches for every 3 feet which the masts are long \& for their diameter under the square of hounds $4 / 5$ of their diameter in caps.

Royal Poles $4 / 5$ of the length of their respective top gallant mast \& for their diameter at the largest part of the masts the same as their respective top gallant masts are at the smallest parts under the Hounds.

## Tops Main

Top to be one half the moulded Beam
Fore top
$11 / 12$ of main top, mizzen top $4 / 5$ of Fore top. For the length of all tops \& fore \& aft allow $2 / 3$ of their breadth

## Trestle Trees

All lower trestle trees to be exactly the same length that their respective tops are long. For the length of all top mast trestle trees allow exactly $1 / 3$ of the length of their respective lower trees

## Cross Trees

All lower crosstrees - the same length that their respective tops are broad.
For the length of all top mast crosstrees allow $3 / 5$ of their respective after lower ones.
For the length of middle corsstrees $5 / 6$ of the after crosstrees.
For the fore crosstrees $5 / 6$ of the middle ones.

Yards
For the length of the main yard take twice and $1 / 0$ of the moulded beam
Fore yard 9/10 of main yard
Fore \& main top sail yards 5/7 of their lower yards
Crossjack yard - The same length as main topsail yard. An extra addition however $1 / 16$ of the whole length of the yards will be necessary to add to the yard arms as the crossjack yard arms bear no proportion to any other yardarms on the ship.
Mizen topsail yards $5 / 7$ of the crossjack yard or main topsail yard.
All top gallant yards $2 / 3$ of their topsail yards Royal yards $5 / 7$ of their respective top gallant yards Sprit sail yard - same length as foretop sail yard For yard arms of every description (except crossjack yard) allow $1 / 8$ for the length of their respective yards or $1 / 16$ for each yard arm. For the diameter of Royal \& lower yards in the slings (exclusive of battins) allow one inch to every 5 feet in length.
For the diameter for topsail \& top gallant Yards in the slings (exclusive of battins) Allow one inch for every $41 / 2$ feet

## Bowsprit

For the length of bowsprit take once \& a half of the breadth of beam of which it is to house exactly one third diameter of Bowsprit at Main Gammoning Exactly the same size that the foremast is in the main deck partners.

## Booms

For gibboom take $4 / 5$ of the bowsprit \& for its Diameter allow 3 inches for every 10 feetFlying gibboom same length as gibboom \& for its diameter allow 2/3 the diameter of gibboom Spanker Boom - same length as fore
Topsail yard \& for its diameter allow 1 inch for every 5 feet.
Mizen Gaft 7/10 of the spanker boom.
For the length of top main steering sail boom allow $10 / 19$ of fore $\&$ main yards \& for their diameter $1^{8}$ inch for every 6 feet of their length.
For the length of all top gallant steering sail booms allow exactly one half the length of their respective yards (including booming) \& for their diameter one inch for every 6 feet of their length.

The United States Ship Franklin
Left the port of Philadelphia June 24, 1817 at 8 o'clock A.M. The following information was derived from Leuit. Beltry
The Franklin's best sailing trim is
22 feet 6 inches aft $\quad 21$ feet 6 inches forw ${ }^{\text {d }}$
Height of lower portside 5 feet 7 inches
This ship is considered sufficiently stiff at the draft of water mentioned above
United States Ship Franklin of 74 guns
built at the navy yard in Philadelphia by Charles Penrose \& Samuel Humphreys launched 1815
Launched August 21, 1815


| Black strakes | 1 st <br>  <br> $2^{\text {nd }}$ <br> $D^{\circ}$ | 7 inches |
| :--- | :--- | :--- |
| 6 inches |  |  |

Channel wale 3 strakes $51 / 2$ inches thick
Filling in plank between @ wales \& black strakes $41 / 2$ inches
Planks between channel wale \& fixing $31 / 3$ excepting the two lower ones
Strings \& drifts 4 inches thick
Butt bolts 1 inch
Limber Strake 8 inches thick
Next strake above $61 / 2$ inches
Inside bilge strakes 2 strakes of $81 / 2$ inches
Below them 1 strake of 6 inches
Above them 1 strake of $61 / 2$ \& one of $51 / 2$ inches
Limber boards 3 inches thick
Strakes on first futtock heads 7 inches
One strake above \& one below $51 / 2$ inches thick

Orlope deck clamps

| One strake | 8 inches |
| :--- | :--- |
| One $\mathrm{D}^{\circ}$ | $7 \mathrm{D}^{\circ}$ |
| One $\mathrm{D}^{\circ}$ | $5 \frac{1}{2} \mathrm{D}^{\circ}$ |

Sperketting on orlope deck toggled
3 inches over the beams
2 strakes lower strake 8 inches upper and
$61 / 2$ inches dubbed fair through
Orlope deck beams sided 15 \& moulded 14
At the ends $11 \frac{1}{2}$ inches

Orlope Deck was kneed with one lodging knee and where they could be put in with one standard knee.
This deck had 3 tier of carlings or fore \& aft pieces 8 by 10, ledges 6 inches square.
Stantions to the Beams in the Hold $9_{2}$ sqr. Planks on the orlope 3 inches thick
Breasthooks in the Hold 5 including the Lower Gun Deck Hook.
Lower Gun Deck Clamps in 3 Strakes. The upper edge of the upper strake $81 / 2$ inches $\&$ the lower edge of the lower one $61 / 2$ inches.

Between the lower edge of these clamps \& the upper edge of the orlope deck spirketting there was a list or air strake of 5 inches which was the only one the ship had.

Lower Gun Deck Beams sided $15 \frac{1}{2}$ inch and moulded 16 inch deep at the ends $131 / 2$ inch jogged into the clamps \& sided.
Lodging and hanging knees of this deck sided 11 inches \& bolted with $11 / 4$ copper \& Iron. Coamings and headledges 18 inches above Deck.
Deck Plank $41 / 2$ inches Thick
Waterways Sided 10 inches and moulded 14.
Joggled down $11 / 2$ inches over the beam
An oak plank 6 inches thick was likewise joggled over the beams \& bolted through the waterway \& side \& riveted to the inner edge of this plank

There were 2 strakes of oak 6 inches thick 11 inches wide joggled $1 \frac{1}{2}$ inches down over the beam \& bolted together

Distance at centre of foremost of the of the joint of these strakes from the middle line 5-1 $1 / 2$
Distance at $\otimes$ to joint of $\mathrm{D}^{\circ} \quad 5-4$
Distance at transom 5-2
Spirkettings 2 strakes 6 inches thick
Plank between lower gun deck ports \& between spiketting \& upper gun deck clamps is $41 / 2$ inches
Lower gun deck port hinges 4 inches wide
Centre of the hinge $61 / 2$ inch from side of port
Ring bolts for lashing port in $3 / 4$ iron size of the ring in the clear $31 / 2$
Distance up from Port cill $81 / 2$ Distance from side of port 7 inches
Ring Bolt for Lanyard $101 / 2$ inches from lower edge of port \& 11 from side of port.
Small air port in large port 9 inches fore and aft \& 6 inches up \& down
Lower edge of small port above lower edge of main port
Stops of ports on the sides $21 / 4$ inches
Stops on the lower part of port $23 / 4$ above $11 / 2$
Upper gun deck - Upper gun deck clamp 7 inches thick on The upper edge \& 6 inches thick lower edge Beams sided $171 / 2$ moulded 15 at the ends 12 inches Lodging \& hanging knees sided 10 inches \& bolted with $1 \frac{1}{4}$ iron comings. Head ledge 10 inches above deck A thick strake alongside the waterway \& 2 binding strakes near the hatch directly over the binding strake of the lower gun deck sperkettings $41 / 2$ inches thick. Plank between the ports \& between the sperkettings spar deck clamp $31 / 2$ inches the same outside on this deck as well as the lower gun deck. There were 5 tier of carlings or fore \& aft piece 10 by 11 inches \& 9 by 11 inches one tier in the middle \& 2 tier on either side. The ledge on the lower gun deck were square Stations to support this deck 9 inches square.

Riding Bitts - After pair 20 inches square \& $5-91 / 2$ asunder in the clear
Foremost pair 19 inches square and $4-4$ asunder
The after pair of bitts came to the forestep
Oak cross pieces to bitts up \& down 17
Fore \& aft
17

A pine piece on
the aft side $91 / 2$
inches fore \& aft

Yellow pine on aft side
Bowsprit bitts 17 square
Asunder 2 - 1½
Hause Holes
Center of $1^{\text {st }}$ hausehold from middle line on a square $3-81 / 2$
Diameter of $1^{\text {st }}$ hole sided 18 inches
Distance between hause holes on a square
Diameter of outer hole 16 inches sided $161 / 2$
Spar deck clamps 4 inches thick
Beams sided 14 inches, moulded 11 inches deep at the ends 9 inches
Lodging \& hanging knees sided 8 inches
Mast or port cell 9 inches deep
Comings head ledge 5 inches above deck
Plank of the bulwark inside \& out 3 inches
Carlings \& ledges - same as Orlope Deck
Main step formed by 2 floor riders to reach the main bilge strakes each sided 14 inches \& kept $3-8$ asunder bolts at the ends with 3 bolt of $13 / 8$ copper on the keels

Fore channel has 10 shrouds \& 2 back stays
Main channel 11 shrouds 2 back stays
Mizen 7 shrouds \& 2 back stays with 2 iron bolts of $1 \frac{1}{4}$ inch. The rider stayed close to the ceiling to the lower edge of the bilge strakes \& from there to the ceiling was open enough to admit a man under. They were jogged on the side of the keelson $11 / 4$ inches and 5 inches down \& were 13 inches above the top of the
keelsons. The fore \& aft pieces that formed the side of the step were 13 by 18 inches \& set 2 inches on the rider with a double jog. Beside this jog there was an offset of 3 inches left on the rider to assist in supporting the fore \& aft pieces on the fore \& aft sides of the riders were large cleats sided 14 inches 3 feet long \& 13 inches deep let into the keelson 1 inch to support the rider the fore \& aft way forestep the same as the main excepting that the riders were 4 feet asunder - -
Diagonal Riders - Three pair aft \& 2 pair forwards
Heads lower part of lower cheek 17 inches above upper of wale cheek sided at the stern 11 inches distance between the cheek on a square 3-1 $1 / 2$. Head rail moulded at after end 14 inches at fore end 7 inches.
Middle Rail moulded at after end $\quad 71 / 2$
at fore end
Head timbers number 4
After timbers placed 4 inches before the foreside of the stern
The rabbit of the arm \& sided 8 inches
Foremost timber sided 63/8
Gammoning holes in Number 2
Fore \& aft
Up \& down
$121 / 4$ inches

Counter ports - in Number
Inside of 3 port from middle line
3 inches

Width of port
2 feet

Height of port
Rudder a round head diameter
2-9

Upper brace placed on the 3 d transom
6 braces 5 inches wide
Diameter of Pintles
Channels in Breadth 2-11
Thick at the side $63 / 4$ inches
Thick at the outside 5 inches
Gallery
Lower rim sided $81 / 2$ inches
Upper rim sided $\quad 7 \frac{1}{2}$ inches
Upper stool 61/2 Do
Lower stool $8 \mathrm{D}^{\circ}$
Lower rim outside distance from side 2 - 10
Distance between upper \& lower rim perpendicular in the clear $5-10$
Distance between lower rim and stool perpendicular 1-2
Distance between upper Rim and stool 1-3
Scuppers on Lower Gun Deck
In Number 7
Size after being leaded.
3 by $61 / 2$
Aftermost Scupper 3ft before the fore side of $4^{\text {th }}$ port
Scuppers on Upper Gun Deck
In Number 7
Size after being leaded
3 by $61 / 2$
Aftermost Scupper 15 inches before the fore side of $5^{\text {th }}$ port from galley door wide 3 feet deep
Cill from Deck 19 inches
Distance from after side of door at the height of the lower edge of strip to the aft side of counter timber

6 feet
The other Scuppers were out the same distance
Fore Sheet Block was cut between $10^{\text {th }} \& 11^{\text {th }}$ port from aft - this block was too far forward Main Sheet Block was cut between $3 \& 4^{\text {th }}$ Port from Aft

## Illustration of Franklin Gallery


[Labels added by transcriptionist for clarity]

1. Upper stool sided 6 in head fore end of keel to aft side of [indecipherable] 5 19/32
2. Distance between upper rim \& stool $1-3$ on a square. Upper rim sided $71 / 2$
3. Distance between upper \& lower rims on a square is 5 ft 7 inches
4. After port on upper gun deck
5. Lower rim sided 8 inches
6. Distance between lower rim \& lower stool on a square is 1 foot 3 inches
7. Fore end of rim on fore side of port is $11 \frac{1}{2}$
8. Fore end of stool of the fore end of rim is $191 / 2$ inches
9. [indecipherable]
10. Distance of outer part of lower rim from the plank of side is 2 feet 10 inches

In the lower gun deck hanging knees there were generally 5 bolts in the body beside the throat bolt, which made 6 bolts \& in the arm 4 bolts. However, in the body of some hanging knees there were 6 bolts exclusive of the throat bolt. There ought to have been 6 bolts in the body exclusive of the throat bolt $\& 5$ in the arm.

Franklin left Philadelphia June $24^{\text {th }} 1817$ at 8 o'clock AM. July 17 The Franklin took in 29 long 32 pdrs which weighted 1781 cwt. This weight settled the ship $31 / 2$ inches. Her draught of water after these guns were taken in was Aft $23-1$, forw ${ }^{d} 20-3$. At this depth it required $191 / 2$ tons to settle the ship 1 inch.

Iron Tiller for US Ship Franklin of 74 guns
Whole Length of Tiller


Lignum Vitae Rollers on Sweep 12 inches apart


Iron Tiller for Frigate Guerrier
Whole Length of tiller 13-6 $1 / 4 \quad$ Size at after end 5 by $43 / 4 \quad$ Size at fore end 4 by 4


Lignum Vitae rollers distance asunder from center to center is 12 inches


Iron tiller for US ship Franklin
Whole length of tiller
Capstan for Frigate Guerriere - scan of original drawing


## Joshua Humphreys Notebook

Computer drawn capstan for Frigate Guerriere by Brett Platt - added for clarity, obviously not part of the original journal.


TRANSCRIPTIONIST NOTE: Numbers added by transcriptionist for clarity

12 ft 4 in height from top of pall head to bottom of pumps
$251 / 2$ by 11 inches
3 Lifter Pall-4 in number
4 Neck of barrel 10 in
56 inches
6 Neck of barrel 10 inches
$7 \quad 183 / 4$ inches, 4 palls to this length
84 at top, $51 / 2$ at bottom
914 inches long, 4 palls to this length
10 Neck is [indecipherable]

Rules for the measurement of ships \& vessels to be built in Philadelphia as agreed on by the Shipwright Society January 3rd, 1811
For all plain built ships with two decks - allow $3 / 5$ of the extreme breadth for the rake of the stem beginning to measure twelve inches before the rabbit at the middle of the rale with should determine the point of straight rabbit forward; from that point to the after part of the stern post allowing one twelfth of the extream breadth for its width clear of the rabbit shall determine the length of the keel for tonnage. The breadth for tonnage shall be ascertained from the inside of one rale to the outside of the other in the widest part of the vessel. The depth of hold from the top of ceiling next the keelson (allowing the strake next the keelson the same thickness as the running plank) to the top of after beam amidships \& the height between deck from plank to plank amidships then multiply the length of keel by the extream breadth \& that product by the depth of hold added to half the length between decks which last product divided by 95 shall give the number of tons required.

Single decked vessels on the double deck plan with about 12 inches waist, when depth does not exceed half the extream breadth, measure \& multiply length \& breadth as above \& that product is the depth but when the depth exceeds half the extreme breadth then add that difference to half the extreme breadth for the multiplier for measurement \& divide as aforesaid.

Single deck vessels primed out on the wales measure \& multiply length, breath \& depth \& divide as above.
Frigate built with two flush decks long quarter decks \& forecastle with a tier of ports - multiply the length by breadth \& make product by the height of the gun deck from the ceiling, as aforesaid added to half of the height of the waist amidships which last product divide as above.

Ships with 3 decks \& a tier of ports multiply the length \& breadth as aforesaid \& that product by the height of the middle deck from the ceiling as aforesaid added to half the height between decks which product divide as above.

Single decked vessels with a long quarter deck \& forecastle deep ${ }^{\wedge}$ \& light waist with a tier of ports multiply the length with the extream breadth \& that product by the depth from the ceiling as aforesaid to the top of the beam amidships added to half the height of the wait amidships which last product divide by the common divisor as above.

## Comparison of Independence and Franklin

Comparison between the US Ship Independence launched at Boston in the summer of 1814 and the US Ship Franklin built \& launched at Philadelphia in the Summer of 1815. August $21^{\text {st }} 1815$.

| The Independence when launched drew aft | Ft 19 |
| :---: | :---: |
| The Franklin $\mathrm{D}^{\circ} \mathrm{D}^{\text {o }}$ | 172 |
| Independence drew foreward | 146 |
| Franklin D ${ }^{\text {o }}$ | 136 |
| Independent $4^{\text {th }}$ port from aft above water | 10 |
| Franklin $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ | 118 |
| Independence $5^{\text {th }}$ port from foreward above water | 12 |
| Franklin Do ${ }^{\text {o }}$ ( | 134 |

The Independence had 25 tons of ballast on board which could not have settled her more than 2 inches. Her Bowsprit was not in.

The Franklin had no ballast on board but her Bowsprit was in.
Franklin launched $21^{\text {st }}$ August 1815 at 10 minutes before 3 o' clock
Left Philadelphia June $24^{\text {th }} 1817$ at 8 o'clock
Left the Cape of Delaware October 281817 at 10 o' clock PM
Drawing at Bombay Hook 23-8 water aft with 13 inches of draft of water (differs by as much)


Capstan for 74 Gun Ship Franklin launched at Philadelphia August 211815

Computer graphic of Franklin's capstan
by Brett Platt Added for clarity


3


## TRANSCRIPTIONIST NOTE: Numbers added by transcriptionist for clarity

1. Length from underside of puppy to top of pall head is $2 \mathrm{ft} 4 \frac{1}{2}$ inches
2. $6 \frac{1}{2}$ inches thick
3. Littlest whelps sided $41 / 4$ inside \& $41 / 2$ outside
4. Top of upper gun deck capstand rum head is 4 ft 9 above deck plank that is the running plank
5. Whelps sided $73 / 4$ inches inside \& 10 inches outside
6. Lower side of pallhead is 5 inches above the running deck plank on the upper gun deck

Size of Capstan Spindle for Franklin 74 Gun Ship Franklin


Spindle whole length 19 feet 2 inches


Pall Rim for lower \& Gun decks of US Ship Franklin of 74 Guns<br>The diameter of this rim in the extreme is $4-4 \frac{1}{2}$

There was a Pall fastened to the Pall Head opposite the centre of each Whelp. There were 8 Whelps to each Capstan. The Palls were alternately long \& short. The Band on the Pall Head $1 / 2$ inch thick. Distance from outer part of Whelp to outer Part of Pall Head Bands is $5 \frac{1}{2}$ inches

Puppys 5 inches up \& down. Bar Holes $51 / 2 \times 3$. There was 12 Bar Holes
Outer flat hoop on top \& bottom of drum head $13 / 4$ inches from outer edge. Hoop 3 inches broad \& a bolt between each bar hole. There was also a hoop inside the outer ones. The top of the cast iron pall iron pall ring was $31 / 2$ inches above deck plank. The deck inside th rim was filled up fair to the top of the rim to prevent the water \& dirt from collecting there. The main piece of partners on lower gun deck on which the spindle rested was $11 / 2$ inches above the deck, 17 inches deep. The rest of the partners were 11 inches deep. The whelps were bolted to the barrel with 2 bolts. Lower part of bar holes were 4 feet above the deck plank.

## Upper Gun Deck Capstan

The capstan was the same size as the lower one, it had 8 lifting palls to force up the messanger placed between the whelps about $21 / 8$ inches squared. Outer part of lifting pall from out part of pall head is 3 inches. Bar holes same as lower gun deck capstan.

There were plates of iron set into the top \& bottom of the pall head round the lifting palls $6 \frac{1}{2}$ inches in \& out and $41 / 2$ inches wide.

The outer part of the plate came fair with the outer part of the pall head, partners of the capstan were $11 / 2$ inches above deck and 15 inches deep.


Large scupper cut after the ship was launched to admit the water pass out under deck was cut oval 6 by 9 inches

## Misc. Measurements

A cubic foot of powder weighs 54 pounds
A cubic foot of salt water, say ocean water, weighs $64^{375} / 1000$ pounds
A cubic foot of copper $552687 / 1000$ pounds
A cubic foot if iron 387 pounds
A cubic foot of steel 389 pounds
A cubic foot fresh water $621 / 2$ pounds
231 cubic inches in a gallon
A gallon of fresh water weighs $8355 / 1000 \mathrm{lbs}$
100 gallons fresh water weighs $8351 / 2 \mathrm{lbs}$
Winchester bushel $18 \frac{1}{1} 2$ inches diameter, 8 deep

Dimensioning of ship building at Sacketts Harbour on the Point 1815

Length between perpendiculars
Extreme Breadth (see page 17)
Depth of hold to lower gun deck

Ship Superior built at Sacketts Harbour
Length between perpendiculars
Beam
Hold to lower gun deck

## Ship Mohawk building Sacketts Harbour

Carried 26 long 24 pdrs on gun deck. This ship had a spar deck.
Length between perpendiculars
Beam
Hold

180 ft
43 ft
204 feet
56 feet
21 ft 6 in

17 feet

Ship General Pike - Sacketts Harbour
Length between perpendiculars $\quad 145 \mathrm{ft}$
Beam (corvette built) $\quad 37 \mathrm{ft}$

Hold (this ship had poop \& top gallant forecastle) $\quad 15 \mathrm{ft}$
Waist
5 ft 8 in

| Brig Jones \& Jefferson (Sacketts Harbour) |  |
| :--- | :--- |
| Length between perpendiculars | $1211 / 2 \mathrm{ft}$ |
| Beam | 31 ft 6 in |
| Waist | 5 ft 4 in |

Dimensions of the New Orleans at Sacketts Harbor, in a letter from Sailing Master Ford May 1843

Length of keel
Length lower gun deck
Moulded beam
Beam Extreme
Depth of keel to lower gun deck

183 ft 6 in
200 feet
55 ft 3 in
56 ft 10 in
17 ft 9 in

Cost for Raratan

| Carpenter | 148560 | Dllrs | 21813.74 |
| :--- | ---: | ---: | ---: |
| Laborer | 5230 |  | 4557.97 |
| Sawyer | 3510 |  | 6911.00 |
| Joiners | 1308 |  | 1573.37 |
| Smith | 2868 |  | 3334.00 |
| Caulker | 40 |  | 60.00 |
| Painter | 147 | 207.00 |  |
| Turner |  | 16.00 |  |

Supposed necessary to complete the ship

| Carpenter | 3000 | days |
| :--- | ---: | ---: |
| Caulker | 2304 |  |
| Reamer | 768 |  |
| Joiner | 3720 |  |
| Sawyer | 320 |  |
| Laborers | 1200 |  |
| Painter | 350 |  |

Dimensions of masts \& spars 70 feet

74
72
36
14
52
53

| Keel straight rabbit | $23-5$ | Beams 11 ft |
| :--- | :--- | :--- |
| Main Mast | 73 feet | Head 7 feet |
| Fore mast | $70 \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} 7 \mathrm{D}^{\circ}$ |  |
| Fore top mast | 32 | Pole 12 |
| Bowsprit outboard | 13 feet |  |
| Main boom | $55 \mathrm{D}^{\circ}$ |  |
| Fore yard | $50 \mathrm{D}^{\circ}[\mathrm{mast}] 6$ |  |
| Fore sail yard | $34 \mathrm{D} \quad 1-4$ |  |
| Fore gaff | 20 feet |  |
| Main gaff | 24 feet |  |
| Jibboom | 32 feet | Pole 11 |
| Main top mast | 30 | Pole 10 |

I remain yours most respectfully


Schooner Dolphin
June $23^{\text {rd }} 1820$
James Sexton

TRANSCRIPTIONIST NOTE: This page was very faint, I cannot vouch for the accuracy of the transcription. Also please note that the figures at the left of the page appear to have been added after the original entries were made, and other than the first 6 listed are completely indecipherable.

Dimension of Schooner Bellona
Built in Baltimore in 1812 for Francis Brewer of Phila

| Length | 103 |  |  |
| :---: | :---: | :---: | :---: |
| Beam | 25 |  |  |
| Hold | 11 | 7 | Custom house measurement |
| Dimension of Schooner General Widner |  |  |  |
| Built in 1818 in Talbot County, Maryland |  |  |  |
| Length | 94 | 6 |  |
| Beadth | 22 | 6 |  |
| Depth | 10 | 3 | Custom House measurement |

Dimensions of the Lord Nelson, Caledonia \& Prince Regent - Three Deckers
Length of lower gundecks 205
Keel 170
Beam 53
Depth of Hold 24

| Dimensions of the Commerce de Marseilles | Three decker |  |
| :--- | :---: | :--- |
| Length between the perpendiculars | 208 | 4 |
| Keel | 172 |  |
| Breadth | 54 | $91 / 2$ |
| Depth | 25 |  |
|  |  |  |
| San Joseph |  | Five decker |
| Length between perpendiculars | 194 | 3 |
| Beam | 54 | 3 |
| Hold | 24 | 3 |

Experimental method of finding the tonnage of a ship
Construct an accurate model agreeable to the drawings $f$ the proportioned ship, about one-fourth of an inch to a foot \& let the light load water line be marked on it. Then put the model \& load it until the surface of the water is exactly at the light water line \& let it be suspended until the water drains off \& then weigh now since the weight of similar boats are in the triplicate ratio or as the cubes of the homologous dimensions the weight of the ship when light is therefore equal to the product of the cube of the number of tons the ship exceeds the model by the weight of the model with is to be reduced to tons. Hence if the model is constructed to a quarter of an inch scale, multiply the height of the model by the cube of *48 or 110592 which will give the weight of the ship - - If the multiplier be ounces the product will be ounces, if pounds it will be pounds \& is to be reduced to tons accordingly

Example:
The cube of $48=110592$
$\begin{array}{ll}\text { multiplied by } & 30 \mathrm{lbs} \text { or } 480 \mathrm{oz} \\ 3317760=1481 \mathrm{oz} & 320 \mathrm{lb}\end{array}$
*one fourth of an inch being equal to $1 / 48$ of a foot
Again the model is to be loaded until the surface of the water coincides with the load water line. Now the model being weighed, the weight of the ship is to be found by the preceding rule, then the difference between the weight of the ship when light \& loaded is her tonnage required.

June 27, 1820. Having finished the model of a ship of the line (intended for a three decker) of the following dimensions 210 feet between the perpendiculars, 56 feet 9 inches beam, 23 feet hold. I put it into the water \& loaded it also as to bring the lower port sill 5 feet 6 inches clear of the water, after which the ballast model were weighed at 23 CWT $2 \mathrm{qtr} \& 20 \mathrm{lbs}=$ to 2652 multiplied by the cube of 16 which is the number of three quarters inches in a foot thus:


The above displacement was made in river water. There is 145 tons difference of displacement between fresh water and ocean water.

|  | Tons | Qr | Lbs |
| :--- | :--- | :--- | :--- |
| Freshwater | 4894 | $7-1$ | 20 |
| Add Difference | 145 |  |  |
|  | 4994 | $7-1$ | 20 |

## 74 Gun Ship No 2 North Carolina

Length of main rim of gallery on the side of ship
Length of upper rim on the side of ship 14
Length of lower stool $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$
Length of upper $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$

13
13

> In $10^{1 / 2}$
> $91 / 2$
> 9 3

9 inches
$8 \frac{3}{8}$ inches
$61 / 4$ inches
4 feet 7 inches
1 foot $85 / 8$ inches
1 foot 3 inches
16 inches

Main rim sided to show
Upper rim $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Lower stool $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$
Perpendicular height between rims
Height between main rim \& lower stool
Height between upper rim \& upper stool
Quarter pieces sided

Head
Distance on the bowsprit (underside) from for side
Of rabbit to the sweep of foreside of bust $20^{2}$


## Caliber of guns and weights

42 pdr cannonade weighs 25 CWT 32 pdr weigh 22 CWT
24 pdr weigh 18 cwt
18 pdr cannonade weigh 12 CWT 12 pdr canon weigh 8 CWT
caliber 3.113

Caliber of guns \& pdr

| A 4 pdr | Caliber 3.20 | 6 pdr | Caliber 3.668 |
| :--- | :--- | :--- | :--- |
|  | Shot 3.053 |  | Shot 3.498 |

An 8 in gun weight 3 CWT a 10 inch gun weighs 86 CWT

| 9 pdr | Caliber 4.200 | 12 pdr | Caliber 4.623 |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Shot 4.000 |  | Shot | 4.403 |
| 18 pdr | Caliber 5.292 | 24 pdr | Caliber | 5.524 |
|  | Shot 5.040 |  | Shot | 5.547 |
| 32 pdr | Caliber 6.410 | 42 pdr | Caliber | 7.018 |
|  | Shot 6.105 |  | Shot | 6.684 |

Dimentions for a sloop of war capable of Carrying 30 long 24 pdr corvette
165 feet between perpendiculars
37 feet beam - say for corvette 39 beam
17 feet hold
Distance between the port 7 feet [is a little too short SH]
Ports fore \& aft 3 feet - this for say 3 feet 3 inches
Foreside of foremost port abaft from perpendiculars 12 feet
Afterside of afterport before after perpendicular 10 feet
If to be a frigate built ship, increase the beam to 43 and its length to 175.
The following information was derived from Capt ${ }^{\text {n }}$ John Elton US Navy Hampton Roads April 17, 1820

| Draught of water aft | 25 | $61 / 2$ |
| :--- | :--- | :--- |
| D $^{\circ} \quad \mathrm{D}^{\circ} \quad$ forw $^{\mathrm{d}}$ | 24 | $5^{1 / 2}$ |
| Starboard bow port | 5 | 10 |
| Larboard $\mathrm{D}^{\circ}$ | 5 | 9 |

Stores provisions \& water all in - ninety guns mounted \& 720 men \& offices on board

| Midship port  <br> D starboard <br> $\mathrm{D}^{\circ}$ larboard | 4 | $11^{112}$ | 9 | US Ship Columbus from [Samuel] Hodge |
| :--- | :--- | :--- | :--- | :--- |
| Afterport (mean) | 5 | 11 | 76.174 gallons of water |  |

## North Carolina Capstans

This ship has three capstans - the two lower ones worked together \& the spar deck capstan was calculated to work with the lower one or separate as may be required. There were palls fixed to with whole amount of days work for building them \& fixing compleat say three hundred fourteen 314 days work.

## Dimensions of Frigate Macedonia

Taken from the British
Spar Deck 162

Gun Deck
Beam
Extream Breadth

4

6 from inside to inner
6 from outside outer

Count de Bordas rule for ascertaining the stability of ships of War
Count de Bordas has indicated a method both easy \& simple to ascertain the degree of stability of any ship of war of all rates before going under sail with all stores on board \& the sails bent. That is by placing on starboard side of the ship on the broadest part of the deck close to the bulwark between the main tack \& main sheet such a number of men as the beam measures decimeters, taking care that the remaining part of the crew be equally dispersed throughout the ship so as to be certain of the experiment - the equilibrium through the dispersing of such a number of men being found the rise of water at starboard must accordingly increase. You must then mark exactly to what height of the ship side it terminate \& that being done make them go over to the other side in like manner the number of men which have cooperated in this experiment The change of position will cause a fall of water at starboard side of which you must also be very exact in marking on the ship side the termination of this fall \& if the intervals of the marks were between the rise and fall be twenty centimeters the ship has the desired stability and will prove to be too crank if the distance between the rise \& fall be twenty five centimeters \& too stiff if it be less than fifteen centimeters - French measurement

## English rule for ascertaining the stability of ships

On lower deck guns, run in on one side and not on the other side \& the guns on the other decks to be out on both sides - the men at quarters on all the decks on the side on which the lower deck guns are run out. If the ship heels over 12 inches she is wanting stability.

## Dutch rule for ascertaining the stability of ships

All the crew placed on Main gun deck, close to the side between the main tack \& main sheet. If the ship heels more than 8 inches Dutch measurement, she is considered as wanting stability.

Extract of a memoranda read before the Royal Society at London, November 27, 1817 by Sir Robert [Seppings]

The Nelson, St. Vincent and Howe in form \& dimension are precisely the same as their frame, beam \& external planking of the same scantling. The two former were built according to the old plan \& the latter upon the diagonal system. After the Nelson was launches she was found to have altered nine \& a half inches; the St. Vincent nine \& a quarter inches while the Howe altered only_3 inches \& 5/8. The whole machine in the case of the two former ships were generally disturbed. The Howe exhibited no such symptoms.

The rise of tide where these vessels were launched could not have been less than 18 feet.

## S. Humphreys

Dutch Ship Wassenaar 80 guns
Ballast 353 tons

| Lower gundecks | 28 | 30 pdrs |
| :--- | :--- | :--- |
| Main D | 30 | 18 pdrs |
| Quarter D ${ }^{\circ}$ | 14 | 8 pdrs |
| Forecastle | $\underline{8}$ | 12 pdrs |
|  | $\underline{80}$ guns |  |

Height of the poop

| between the planks |  | 7 | 2 |
| :--- | :--- | :--- | :--- |
| Under the beam | 6 | 6 |  |

Under the beam
$6 \quad 6$

Gundeck

| between the planks | 7 | - |
| :--- | :--- | :--- |
| under |  |  |

under the beam

Between decks
Between the planks $\quad 7 \quad 31 / 2$

Under the beam 6

Cockpit
$\begin{array}{lll}\text { Between the planks } & 7 & 7\end{array}$
Under the beam $6 \quad 21 / 2$

Depth of Hold
$16-9$ under deck 16
under beam $\quad 15 \quad 9$
[Note: The measurements made in Amsterdam post of 11 inches the depth of hold is taken from the top of keelson once one measures]

Draft of water aft
$D^{o}$ forward
Difference of draft

Height of midship lower gundeck port
from the water
Forward Port
After Do
Width of main deck port
Height
Width of lower deck ports
Height
Distance from upper part of lower deck port
to upper part of gun 1
Distance from lower side of gun to lower hull $63 / 4$

Gunpowder
One pound of gun powder measures 32 inches
A cubic foot of gun powder weighs 54 pounds
a cubic inch of gun powder weighs half an ounce

## Dimensions of Ship New Orleans

The following dimensions of the ship of the line New Orleans were taken in the spring of 1842 by the Naval Officer commanding at Sacketts Harbor \& being different from those recorded at page 1 are here recorded

| Length of keel (supposed to be the whole length) | 183 | 6 |
| :--- | :--- | :--- |
| D $^{\circ}$ lower gun deck | 200 |  |
| Beam moulded | 55 | 3 |
| D $^{\circ}$ extreme | 56 | 10 |
| Depth of hold to lower gun deck | 17 | 9 |
| From lower deck to underside of main deck beams | 5 | 6 |
| Ports on lower gun deck | 34 |  |
| D $^{\circ}$ main D $^{\circ}$ | 36 |  |
| D $^{\circ}$ spar $\mathrm{D}^{\circ}$ | 36 |  |

## Gun Powder

A cubic inch weighs half an ounce
A cubic foot weighs 54 pounds
One pound gun powder measures 32 inches
Gunpowder
A cubic foot of gunpowder weighs 54 pounds
A pound of gunpowder contains 32 solid inch
A cubic foot of bread (hard) will weigh 19 pounds made with ale

Dimensions of the ships Hibernia \& Caledonia

|  | Hibernia | Caledonia |
| :---: | :---: | :---: |
| Length between perpendiculars | 2014 | 205 |
| Breadth | 53 | 536 |
| Hanging of the gundecks | 2 3112 | 18 |
| Depth of keel - main | $181 / 2$ | 18 |
| - false | 111 | 0 |
| Depth of hold | 22423 | 2 |
| Height from the upper side of the main keel to lower side of midship port | 26 11½ | 27 9½ |
| Draft of water when completed |  |  |
| to 5 months - aft | 299 | 26 |
| -foreward | 257 | 2410 |
| Broke from the sheer when launched | 3 | $2^{1 / 2}$ |
| D ${ }^{\text {o }}$ when loaded | 7 | 5 |
| Lower side of midship port above |  |  |
| water when compleat | 48 | 56 |
| Displacement of water by the inch at the height of 14 feet 5 inches | $20^{16} / 35$ tons | $20^{6} / 35$ tons |
| Displacement at 22 feet $31 / 2$ inches as above | $23^{14} / 35$ | $23^{10} / 35$ |
| Total displacement per plan at a height of 22 feet $31 / 2$ inches from the upper side of main keel | 4647 | 4557 |
| Entire displacement or weight of the ship and all its contents when completed to 5 months | 4701 | 4506 |
| Weight of the hull when launched | 2561 | 2456 |

Iron used on the US Ship North Carolina

196-3 length between perpendiculars
53 moulded beam
22 depth of hold
226.596 lbs round iron
92.863 lbs flat $\mathrm{D}^{\circ}$
25.470 lbs square $\mathrm{D}^{\circ}$
21.943 lbs foreign iron
336.872 total of iron used on the North Carolina
for plumbing \& equipment \&c
See 2 leaves ahead

Iron \& copper used in the Frigate Susquehannah was on the stocks 175 between perpendiculars 45 beam

NOTE - The ship is on the stocks finished as [empty] 14 stakes of bottom plank on each side. The butt bolts are not drove. The false keel is not on, neither is the center step. The decks are all laid - the rail on \& the ship finished empty as before mentioned

| Round iron | 99.3654 | Round Copper | 26.204 |
| :--- | :---: | :---: | :---: |
| Square iron | 2.011 | Spike copper | $\underline{13.661}$ |
| Flat iron | 4.182 | Total copper lbs | $\underline{39.465}$ |
| Spike iron | $\underline{4.928}$ |  |  |
| Total of iron | 110.485 lbs |  |  |

The additional for comings for the bilge strakes are not in nor are those for thick strakes at first futtock heads nor the $7 / 8$ bolts intended as a substitute for trenails, augering thru for scarph \& drifts which are in.

427 patent augers used
Novemb. 1823

## Cancer

John Goring had been for some time afflicted with a Cancer on his underlip. He applied to several physicians in Philadelphia who gave as their opinion that there was no use for him for him but by cutting the Cancer out this he refused to submit to. In the month of February he took dry Spanish Oak Barke and burnt it to ashes which produced about one peck which he put into a tow linen bag \& then into a pot \& covered the bag with water and boiled it till all the strength of the ashes was boiled out. He then took out the bag with the ashes and boiled the lye down to about half a Pint \& of the consistency of molasses which he then spread on some lint the size of the Cancer and kept it on $3 / 4$ of an Hour. He removed the plaster four (4) times keeping each Plaster on about 45 minutes. Which effects the Cure. He then applied a poultice of bread \& milk with a little flax seed which extracted the cancer nearly the size of the small end of a mans little finger as black as a Coal, he then applied some healing salve $\&$ in two weeks he was perfectly cured.

The above facts were related by John Goring to Thomas Humphreys of Delaware County in the Spring of 1823.

Cancer
A Physician recommended in the London Paper as an ascertained Cure for Cancer the application of a strong vegetable ointment with Hemlock to the scirrus tumour a vegetable diet exclusively and the copious use of Sarsaparilla \& other vegetable beverages.

Weight of Iron Tanks for Water put on board US Ship North Carolina 1n 1822. (Tank for the Pennsylvania weighed more

25 Tanks Weight 24.027 lbs contain 9364 gallons, equal to $256 / 100$ lbs weight to each gallon of content

One tank containing 163 gallons weighed 494 lbs
One tank containing 656 gallons weighed 1399 lbs
Tanks for the Pennsylvania weighed 3 32/100 lbs to the gallon
The North Carolina had on board 147 tanks weighing 157.848 at 18 each 28412 64/100 lbs These tanks held 63000 gallons of water.

For your tanks say $21 / 2 \mathrm{lbs}$ of iron for one gallon of water, water casks say $9 / 10 \mathrm{lbs}$ of cask for one gallon.
The tanks on board the Brandywine weigh about 2 lbs to the gallon

## Joshua Humphreys Notebook



Samuel Humphreys

Weight of Round Iron

| $17 / 8$ weighs 9 lbs to the foot | $15 / 8$ | $667 / 100$ |
| :--- | :--- | :---: |
| Weight of round iron | $11 / 2$ | $575 / 100$ |
| Weight in 12 inches lineal measure | $13 / 8$ iron | $486 / 100$ |
| D $^{\circ}$ | $11 / 4 \mathrm{D}^{\circ}$ | $398 / 100$ |
| D $^{\circ}$ | $11 / 8 \mathrm{D}^{\circ}$ | $346 / 100$ |
| $\mathrm{D}^{\circ}$ | $1 \mathrm{D}^{\circ}$ | $260 / 100$ |
| $\mathrm{D}^{\circ}$ | $7 / 8 \mathrm{D}^{\circ}$ | $206 / 100$ |
| $\mathrm{D}^{\circ}$ | $3 / 4 \mathrm{D}^{\circ}$ | $156 / 100$ |
| $\mathrm{D}^{\circ}$ | $1 / 2 \mathrm{D}^{\circ}$ | $75 / 100$ |
| $\mathrm{D}^{\circ}$ | $5 / 8 \mathrm{D}^{\circ}$ | $112 / 100$ |

12 nine inch spikes weigh 7 lbs .8 inch spikes 2 to the pound, 7 inch spikes 3 to the pound

## Rule for the weight of Anchors

500 lbs is allowed for every hundred tons of a ships measurement for a merchant vessel.
Ships above 500 tons do not require so great a proportion.
Proportion for Cables
For each foot of half the extreme breadth of the ships Beam allow one inch of circumference for the Best Bower Cable. Thus a ship of 32 feet Beam will require a 16 inch Cable.

Hawse Holes
Twice \& one half the diameter of the Cable
3/15 inch cable

| $\frac{5}{2}$ | $3 / \underline{24}$ |
| :--- | :--- |
| $\frac{10}{\underline{21 / 2}}$ | 8 |
| $\underline{16}$ | $\underline{20}$ inch hole rather small |

$12^{1 / 2}$ inch hole rather small
Dry Measures
The standard Gallon dry measure contains $2684 / 5$ cubical inches.
The bak or Trinchester Bushel 2150 2/5 inches.
The Dimensions of the Trinchester Bushel are 8 inches deep \& $181 / 2$ inches wide.
The Ale \& Milk Gallon contain 282 cubic inches.
The Wine gallon contains 231 cubic inches \& it is remarkable that the Wine \& Ale gallons have the same proportion to each other as the Troy \& avoirdupois pounds have - that is as the pound Troy is to one pound avoirdupois, so is one Wine gallon to one Ale gallon.

## English Rule of measurement

Rules observed in measuring the tonnage of ships in the Kings English-Merchant service.
$1^{\text {st }}$ Let fall a perpendicular from the fore side of the stem at the height of the Hawse Holes \& another perpendicular from the back of the Stern Post at the height of the wing transom.
$2^{\text {nd }}$ From the length between these perpendiculars deduct $3 / 5$ of the extreme breadth $\otimes$ likewise as many 2 $1 / 2$ inches as the wing transom is high from the upper edge of the keel \& the remainder is accounted the keel for tonnage. Then multiply the keel for tonnage by the extreme breadth $\&$ that product by half the extreme Breadth; then divide by 94 the quotient will be the burthen in what is denominated Builders Tonnage.

Q By the extreme Breadth is meant the Breadth taken From timber to timber outside with the thickness of the bottom on each side added on which is the same thing, the thickness of the bottom plank added to the moulded breadth

Proportion for the depth of throats of floor timbers moundling size of heads for vessels from 100-400 tons and depth of throat in inches equals one half of the beam in feet, floor head $2 / 3$ of the throat. This rule applies to vessels having thus floor length equal to half the beam.

A vessel of 24 feet beam will have 12 inch throat and 8 inch at floor head. Vessels more than 400 tons will require less throat than this same rule.

Weight of Round Copper Bolts
$11 / 2 \quad$ 678/100
$13 / 8$ inch round copper weighs $\quad 56 / 10$ to the foot
$11 / 4$
$11 / 8$
1
7/8
$47 / 10$
$3724 / 1000$ to the foot
3 lbs
$2225 / 1000$ to the foot
$15 / 10$ to the foot

Size of the Water barrel

|  | Length of Staves |  | Diam. Bilge <br> Ft |  | In | Ft | In |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Powder Barrel (1853)
A Powder Barrel calculated to hold 100 lbs of Powder is 23 inch long \& its greatest diameter including the Hoop is $16 \frac{1}{2}$ inches.
(DuPonts Powder Barrel made in 183521 inches long 17 inch bilge \& 15 inch head)

## 42 pdr Carronade port

A 42 Pdr carronade requires the depth of the Port to be 3 ft 7 or 43 above [cell] above the bed when at its greatest elevation \& allowing for the difference that may arise in the height of the ports. Let the under part of the upper side of the port be 2 feet 5 inches aboce the bed or top part of the cannonade carriage.

| 2 ft 3 inches above the bed or carriage say | 2 ft | 3 |
| :--- | :--- | :--- |
| Add thickness of skids \& bed | 1 | 2 |
| Allow the gun to be diam of the rail |  | 1 |
| Depth of port | 3 | 6 |
| Portside from deck |  | 8 |
| Under side of rail above deck | 4 ft | 2 in |

January 1836
A 42 Pdr carronade weighs $\longrightarrow$
A $32 \mathrm{Pdr} \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad$ about 1 ton
An English Long 18 Pdr weighs about 37 cwt 12 qr
A Bushel of English Coal weighs 88 lbs
To store powder barrrels according to DuPonts rule as above will require for one height of barrels 1 ft 6 , two heights bilge head [tiers] 2-9 $1 / 2$ - three high 4 - four high $5-5$, five heights 6 feet $8 \frac{1}{2}$ inches, six heights 8 feet
(Jan 1842) Boxes proposed to carry powder in cylinders 2 feet long 17 inches square

## Proportions for Long Iron Guns

The length of the Gun calculating from the hind part of the Base ring is 16 calibers
The length is then divided into 7 equal parts.
The length of the first reinforce two of these parts.
The length of the second reinforce is one \& 15/16 of 76 caliber
The chase is four wanting $15 / 16$ of the caliber
Center of trunnion is $3 / 7$ of the gun length from the [indecipherable text]
The length of [pomiglion] or [caseable] is one $\& 13 / 16$ of a caliber
The caliber of the gun being divided into 16 equal parts
The thickness of metal at the bar ring from the base is 18 5/10
At the end of first reinforce
At the end of second reinforce
At the same place for the beginning of the chase
At the end of the chase [indecipherable] muzzle the moulding is sided 9
At the swelling of the muzzle/meaning the extra is reinforce

US Frigate Guerriere

| Draft of water Forward - bowsprit in | $11-2$ |
| :--- | :--- |
| $\mathrm{D}^{\circ}$ D $\mathrm{D}^{\circ}$ Aft | $16-6$ |
| Height of middle port | $17-5$ |
| Height of midship port | $13-7$ |
| Height of aftermost port | $13-5$ |

Frigate Brandy launched at Washington
Draft of water when launched Aft 16-6
Forward 12-6
Depth of Keel clear of Bottom plank 2-4

Boats of US Ship North Carolina with the cost of wages paid for each boat.

| Boat | Length | Breadth | Depth | Cost |
| :--- | :--- | :--- | :--- | :--- |
| Launch | 38 | $10-6$ | 4 | 285 |
| First Cutter | 36 | $8-10$ | $3-6$ | 195.50 |
| Second Cutter | 32 | $8-3$ | $3-6$ | 181.75 |
| Third Cutter | 29 | 7 | $3-4$ | 110 |
| 2 Quarter Boats | 27 | $6-6$ | $2-10$ | 138 |
| Gig | 30 | $5-3$ | $2-10$ | 144.30 |
| Stern Boat | $29-6$ | 7 | $2-11$ | 120.57 |
| Life Boat | 27 | 7 | 3 | $\underline{165}$ |
|  |  |  |  | 1340.12 |

The Launch, $1^{\text {st }}, 2^{\text {nd }} \& 3^{\text {rd }}$ cutters are Carvel built, the remainder are clinker work. This includes pay of master boat builder.

Hammocks Netting for the North Carolina
4 feet 9 inches asunder, 2 feet wide \& as high as the poop deck.

Hawse pipes for chain cables
Multiply the diameter of the wire by 4 to which add one inch will make the diameter for one inch iron of 5 inches.

The present system of French Measures
Present measure weight Substitution Value in American Measure

The mrylametre or new [league] 10.000 meter or 10 miles 32509 feet 2 inches or
6 miles $11 \frac{1}{2}$ feet 2 inches
The mile or kilometer
1000 metre
The present [puck] or decimeter 10 metres
3280 feet 11 inches

The metre
one forty millionth part 39.3702 inches or about of a meridian of the Earth three and one third feet

Corrected Metre
The palm or decimeter The doight or centimeter
39.3927 inches
one tenth metre nearly 4 inches one hundredth of metre or 10 milimeters nearly four tenths of an inch

Nails for making moulds
Quantity required for making a set of
44 gun ship molds
Error: It cannot take 80,700 nails for the set of
28,000 of 4 penny frigate moulds
52,700 of 6 penny
80,700 Total required for one set of frigate moulds

290 nails 6 penny weighs one pound
933 nails 4 penny weighs one pound
Nails expended in making a set of frigate moulds excluding after fan \& after deadwood mounds in the [end plan]

Two thousand 6 penny
28 pounds 4 penny
Weight of Lead used for Frigate Guerriere

| Cwt | Qr | Lb |
| :--- | :--- | :--- |
| 222 | 1 | 1.9 |

Siding \& moulding size of Schooner Shark
Timbers

| Timber \& room | $213 / 4$ inches |
| :--- | :---: |
| Floor sided | $71 / 2$ inches |
| Futtocks sided | 7 inches |
| Throats of floors | 10 inches |
| Floor heads | $81 / 2$ inches (too big) |
| Gunwale | $33 / 4$ inches (rather small) |

Mast Timbers for Sloop of War Vandalia

|  |  | Upper End | Lower End |
| :--- | :--- | :--- | :--- |
| Main Mast | 1 piece 80 feet | 9 by $171 / 2$ | 26 by 26 |
| 2 cheeks | each 76 ft long | $71 / 2$ by 20 | 4 by 12 |
| 1 Paunch | 76 feet long | 5 by $121 / 2$ | 5 by $121 / 2$ |
| Foremast | 1 piece 72 ft long | 8 by 17 | 23 by 23 |
| 2 cheeks | each 68 ft long | 6 by 19 | 3 by 11 |
| 1 Paunch | 68 feet long | $41 / 2$ by 11 | $41 / 2$ by 11 |

One pound of light drawing nails or sheathing nails will completely fasten 8 feet of sheathing. That is a vessels bottom measuring 2400 feet will require 300 lbs sheathing nails.

Dimensions of the Santissima Trinidad, Spanish three decker - in English measure.
Length between perpendiculars 204 feet 9 inches, beam moulded 54 feet
What is the momentum of a ram falling from any given height?
Answer- the square of the height of the fall in feet multiplied by the weight of the ram in pounds. Suppose the fall of the ram is 20 feet, the weight of the ram 1500 lbs . What weight would a pile thus drove be capable of sustaining without moving perpendicularly

| 20 | 400 |
| ---: | :---: |
| $\times \underline{20}$ | $\underline{200000}$ |
| 400 | $\underline{400000}$ |
|  | po0000 |
|  |  |

Tonnage of Ship of the Line Pennsylvania
Made out for Comm Stewart- June 1829

| Keel for Tonnage Custom House Measurement | 183 feet |
| :--- | :--- |
| Beam for $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$ | 57 ft 9 |
| Burthen in tons Custom House Measurement | $321218 / 95$ (say 3241 tons corrected tonnage) |
| Burthen in Tons Sheer carpenters (old) measurement | $294083 / 95$ Tons |
| Length between perpendiculars from the aft side of |  |
| Rabbet of Stem to fore side of Rabbet of post <br> at crossbeam | 210 feet |

Deduct Thickness of apron \& Transom 3 feet 6 inches will leave the length of Gun deck 206 feet 6 inches. Length of Spar Deck 220 feet 8 inches Tread of the deck.
Length between perpendiculars 210 feet
Beam moulded $\quad 56 \mathrm{ft} 9$
Depth of Hold $\quad 22 \mathrm{ft} 3$
Length of Keel Carpenters tonnage 173 feet 6 inches
Beam D ${ }^{\circ}$ D $^{\circ} 56$ feet 9 inches

To measure the tonnage of any Ship or vessel the surveyor or such other person as shall be appointed by the Collector of the district to measure the same, that if the said ship or Vessel be double decked take the length thereof from the fore part of the main stem to the after part of the Stern Post above the upper side the Breadth thereof at the broadest part above the main [wales] half of which breadth shall be around the depth of such vessel then deduct from the length three fifths of the breadth - multiply the remainder by the breadth and the product by the depth and shall divide the last product by 95 , the quotient whereof shall be deemed the true content or tonnage of such Ship or Vessel and if such Ship or vessel be single decked the said Surveyor or other persons shall take the length and breadth as above directed in respect to a double masted ship or Vessel shall deduct from this same length Three fifths of the breadth and taking the depth from the underside of the deck planks to the ceiling in the hold shall multiply and divide as aforesaid and as the quotient shall be deemed the tonnage of such Ship or Vessel.

March $2^{\text {nd }} 1799$
Ship of the Line North Carolina

Height of Eye Bolt for gun tackle of cannonade above spar deck 1 foot 8 inches
Height of Center of Scupper for breaking above the spar deck 2.5
Dimensions of Vessels from the Treasury Books 1829

|  | On Deck | Beam | Hold | Tons |
| :--- | :--- | :--- | :--- | :--- |
| Brig Georgianna | 77 | 22 ft 1 | 9 ft 1 | 134 |
| Brig Pilot | 83 ft 6 | 20 ft 10 | 9 ft 6 | 147 |
| Schooner North Branch | 81 | 24 | 7 ft 7 | 127 |
| Brig Shawmut | 76 | $21 \mathrm{ft} \mathrm{2}{ }^{1 / 2}$ | $9 \mathrm{ft} 8^{1 ⁄ 2} 2$ | 137 |
| Schooner Only Daughter | 60 ft 4 | 18 ft 7 | 7 ft 4 | 70 |
| Brig Sea Island | 82 ft 5 | 23 ft 11 | 12 ft 5 | 212 |

The above are Eastern Vessels belonging to Boston

| Schooner Eclipse | 87 ft 6 | 22 ft 6 | 9 ft 3 | 163 Built on the Eastern Shore of Maryland |
| :--- | :--- | :--- | :--- | :--- |
| Economy | 76 | 22 | 8 | 116 tons Built in Delaware |
| James Monroe | 60 ft 5 | 20 ft 9 | 7 | 73 Cape May |
| Mount Vernon | 69 | 22 ft 10 | 8 ft 10 | 115 Salem Mass |

## Swedish Weight

A Skeppund, iron weight, is 320 lbs Swedish
18 Skeppund iron weight is equal to one last of 5700 lbs Swedish

## Gun Powder

A pound of gun powder measuring 32 inches
A cubic foot of gun powder weight 54 pounds
A cubic inch of gunpowder weight half an ounce

## Live Oak Frames

A ship of the line 2400 tons takes
A 44 gun ship 1600 tons takes
A sloop of war of 700 tons takes
A schooner of 180 tons takes
13 cubic feet of mountain timber to pull from

| $12 \mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ |
| :--- | :--- | :--- | :--- | :--- |
| $12(12)$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ |
| $10(10)$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ | $\mathrm{D}^{\circ}$ |

## Joshua Humphreys Notebook

Oakum
A ship of the line 2400 tons takes 14 lbs oakum to the ton $=$ to $33,600 \mathrm{lbs}$ A 44 gun ship 1600 tons takes 13 lbs oakum to the ton $=20,800 \mathrm{lbs}$
A sloop of war of 700 tons takes 11 lbs oakum to the ton $=7,700 \mathrm{lbs}$
A schooner of 180 tons takes 7 lbs oakum to the ton $=1,260 \mathrm{lbs}$
The Store ships in Phila about 12 lbs to the ton

1832
Frigate Vernon (British) 175 foot gun deck- -52 foot Beam projected by Captain Symond surveyor of the Navy

The ship with her masts, shot \&c (no guns) draws 3 inches more water forward than aft --- She is to sail against the Castor a 32 gun frigate projected by Sir Robert Sepping former surveyor of the Navy.

Dimension of the old Frigate Louisiana

|  | Feet | Inches |
| :--- | :--- | :--- |
| Depth of head of gundeck | 138 | 8 |
| Breadth extreme including both wales | 39 | 8 |
| Distance between gundeck ports | 7 |  |
| Height of ports | 3 | 4 |
| Frigate Congress |  |  |
| Depth of the head of gun deck | 165 | 4 |
| Breadth extreme including both wales | 41 | 1 |
| Distance between gundeck ports | 7 | 6 |
| Height of ports | 3 | 4 |

Memorandums taken on the dimentions of Frigate Constitution September 1833


The ports abaft the $5^{\text {th }}$ port were about 22 inches. The hang of sheer of ports sills fore about 17 inches
Top gundeck beam as it now stands is
219
gundecks planks to be
41/2
The old beam springs only $2^{1 / 2}$ inches add $21 / 2$ inches more for the men
$2^{1 / 2}$
224
Height of port sill from thwarts of floors
$23 \quad 11$
Decks below port sill
2 .
$21 \quad 11$
Add spring of beam


Height of present deck, say from top of gundeck plank to underside of spar deck beam at $\otimes$ $6 \quad 1$
Height forward at bowsprit bitts 63

See letter to Comm ${ }^{\text {n }}$ Jesse D. Elliott September 16, 1833
By act of the legislature of Pennsylvania -
Bbl flour head $161 / 2$ inches at the head the staves 27 inches long - 196 lb flour
Half bbl of flour head $12^{1 / 2}$ inches at head staves 23 inches long
Corn meal holds 800 lbs
Diameter of head 27 inches Diameter at bung 31 inches Staves forty one inches long

Dimensions of a flour barrel 26 inches long This is the entire dimensions
20 $1 / 2$ inches diameter at bulge
$181 / 2 \mathrm{D}^{\circ} \mathrm{D}^{\mathrm{o}} \mathrm{D}^{\mathrm{o}}$ at head

Whole bbls diam head 17 inches length staves 27 inches
Half bbls length of staves 22 inches diameter hd 13 inches

| Iron Spikes |  |  |  |
| :---: | :---: | :---: | :---: |
| 6 inch spikes | 4 to the |  |  |
| Half crown nail | 4 inches |  |  |
| 20 penny nails | $3 / 4$ inches |  |  |
| Deck nails | 5 inches |  |  |
| Two shilling nails | 4 inches |  |  |
| Tenpenny nails | 23/4 inch |  |  |
| Dimensions of US Brig Spark |  |  |  |
| Length between perpendicularsbeam moulded |  | 100 feet |  |
|  |  | 26 |  |
| Depth of hold |  | 11 | 6 |
| Dimensions of US ship Hornet |  |  |  |
| Length of gundecks |  | 106 |  |
| Beam moulded |  | 29 | 7 |
| D ${ }^{\text {o extreme }}$ |  | 31 | 4 |
| Height between decks |  | 5 | 3 |
| Ship Wasp |  |  |  |
| Length of gundecks |  | 117 | 11 |
| Beam moulded |  | 31 | 4 |
| Hold |  | 14 | 6 |

The English estimate that their ships carry to sea only $2 / 5$ of the timber purchased for their construction
Annotated Maritime of 1824
The timber necessary to put a vessel in frame is about $1 / 3$ of the whole quantity required for her
White Oak Difference between the rough quantity \& that put into the Ship is as 97 to 42

Yellow Pine Difference between the rough quantity \& that put into the Ship is as 76 to 43
Live Oak Live Oak frames after being cut to moulds the proportion is as 42 to $36---$ - better multiply the rough quantity by .83

Timber produced (that is cut to moulds) from trees is about one fourth of the contents of the trunk of the tree

Live Oak Trees \& their produce
It is supposed that in live oak land south and west of Cape Florida there is only two trees to one acre of land \& that each tree will produce 30 cubical feet of moulded timber flat for the Navy (say for ships of the Line, Frigates \& large Sloops of War) equal to 60 cubical feet to each acre.

Schooner Guerriere
Draught as originally drawn by Mr. Eckford
Length between perpendiculars
92.2

Distance on gun deck from the perpendicular to centre of foremast 16.3
Distance on gun deck from the perpendicular to center of main mast
54.6

Distance on gun deck from center of main mast to after perpendicular


Take half of the first, twice the second \& half the third, add them together \& divide by 2 . The product will then be multiplied by the distance between the first \& third cosine multiply the verified sine 3 feet by the chord \& take $2 / 3$ for the cosine
$3 \stackrel{4}{12}$
$4 \times 24=96$
$\frac{24}{72}$
The parallelogram 48 feet
The Segment-------48

Dimensions of masts and spars of Sloop Peacock as she was fitted for the Polar expedition 1828

|  |  | Length |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Ft In | Diam ${ }^{\text {r }}$ | Yardarm |
| Main | mast | 700 | 23 | 122 |
|  | topmast | 420 | $13^{2 / 10}$ | 7 |
|  | topgallant | 210 | $79 / 10$ |  |
|  | Royal | 162 | $59 / 10$ |  |
| Fore | mast | 630 | $20^{7 / 10}$ | 1010 |
|  | Topmast | 379 | $11^{9} / 10$ | 63 |
|  | topgallant | 1810 | $7^{1 / 10}$ |  |
|  | Royal ${ }^{\text {o }}$ | 145 | $53 / 10$ |  |
| Mizenmast upper end of mast on a level with |  |  |  |  |
|  | Main X trees |  | $15^{3 / 10}$ | 99 |
| Mizen | topmast | 337 | 92/10 | 57 |
|  | topgallant mast | 1610 | 5 5/10 |  |
|  | royal mast | 1211 | $4^{1 / 10}$ |  |
| Main | Yard | 578 | $13^{2 / 10}$ | 211 |
|  | topsail yard | 276 | $6^{1 / 10}$ | 15 |
|  | Topgallant yard | 184 | 41/10 | 11 |
| Fore | yard | 513 | $11^{9} / 10$ | 29 |
|  | topsail yard | 385 | $85 / 10$ | 33 |
|  | topgallant yard | 245 | $56 / 10$ | 13 |
|  | royal yard | 183 | $36 / 10$ | 10 |
| Crossjack yard |  | 433 | 92/10 | 42 |
| Mizen topsail yard |  | 3011 | $6^{9} / 10$ | 2 |
| Mizen topgallant yard |  | 198 | $4^{4} / 10$ | 110 |
| Royal yard |  | 131 | 3 | 08 |
| Sprit sail yard |  |  |  |  |
| Bowsprit outboard |  |  |  |  |
| Gibboom |  |  |  |  |
| Flying gibboom |  |  |  |  |
| Spanker |  |  |  |  |
| Mizen Gaft |  |  |  |  |
| Fore Gaft |  |  |  |  |
| Main Gaft |  |  |  |  |
| Lower swinging boom |  |  |  |  |
| $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ yard |  |  |  |  |
| Fore topmast steering sail boom |  |  |  |  |
| $\mathrm{D}^{\circ} \mathrm{D}$ | $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \quad$ yard | 115 | 3 |  |
| Foretop gallant studding sail boom |  |  |  |  |
| $\mathrm{D}^{\circ} \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \mathrm{D}^{\text {o }}$ y yard |  |  |  |  |
| Main topgallant steering sail boom |  |  |  |  |
| $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad$ yard |  |  |  |  |
| Main top breadth 15 feet, fore \& aft <br> foretop $\mathrm{D}^{\circ}$ $136 \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$ <br> Mizen 1010 |  | 10 feet |  |  |
|  |  | 9 |  |  |
|  |  | 73 |  |  |
| Main trestletrees in depth |  | 111/2 inches thickness | 53/4 inches |  |
| Fore $\mathrm{D}^{\circ} \mathrm{D}^{\circ}$ |  | $10^{1 / 2} \mathrm{D}^{\circ} \mathrm{D}^{\circ}$ | 51/4 $\mathrm{D}^{\text {o }}$ |  |
| Mizen | D ${ }^{\circ}$ ~ | $73 / 4 \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$ | $4 \mathrm{D}^{\circ}$ |  |


| Foretop mast trestle trees in depth | 6 inches thickness3 inches |  |
| :---: | :---: | :---: |
| main $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$ | $66 / 10$ thickness $33 / 10$ |  |
| Mizen | $46 / 10 \quad$ Do ${ }^{\text {o }}$ 3/10 |  |
| Foretopmast trestle trees in length | 31 |  |
| Main $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \mathrm{D}^{\circ}$ | 35 |  |
| Mizen $\mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ} \quad \mathrm{D}^{\circ}$ | 25 |  |
| Foretopmast X trees | After crosstree in length | $8 \quad 1$ |
|  | Middle $\mathrm{D}^{\circ}$ | 69 |
|  | Forward D ${ }^{\text {o }}$ | 58 |
| Main topmast $X$ trees | After crosstree in length | 9 - |
|  | Middle ${ }^{\text {o }}$ | 76 |
|  | Forward D ${ }^{\text {o }}$ | 63 |
| Mizen top X trees | After crosstree in length | 66 |
|  | Middle Do | 55 |
|  | Forward D ${ }^{\text {o }}$ | 46 |

This ship Peacock was hauled up in the Brooklyn Navy Yard \& rebuilt by a new draught.
J Humphreys Aug 3 ${ }^{\text {rd }} 1828$
Ship of the Line Ohio
At 25 feet draft of water she will displace 4120 Tons
15.. 2 forward 19.. 4 abaft 17.. 3 in 2170 Tons

Had in then 200 tons kentledge, keel \& false keel
At 24 feet water it requires 22 tons 164 pounds forward to settle her one inch
At 20 feet 6 inches it requires 20 tons, 1643 pounds $D^{\circ}$

A comparison of the foot \& other measure of length
in different countries, namely the number of feet \&c in each place corresponding to 100 English feet; \& also the length of a single measure of each denomination in English inches \& hundreths of an inch.

|  | $\begin{array}{l}\text { Number of each ength of a single } \\ \text { Equal to 100 } \\ \text { English feet }\end{array}$ |  |
| :--- | :---: | :---: |
| measure of each |  |  |$)$

Joshua Humphreys Notebook

Remarks of Mr. Buchanan of Pennsylvania
on the Tariff bill in Congress April 1828

Let us now Sir examine the calculation which the gentleman has made for the purpose of proving that our navigation cannot sustain the additional duties proposed by the bill upon foreign hemp iron - -

House in January 1, 1821 addressed certain questions to the Mercantile Society of New York two of which with the answers I shall take leave to read to the committee:
"Question - What is the cost of a British ship of say 300 tons, what of an American of the same force \& burthen; \& generally the difference is the price of shipping by the ton in each country completely equipped?

Ans: A British ship of 300 tons equipped for sea will cost 24,000 dollars or 80 dolls per ton. An American ship of the same quality will cost 18,000 dolls or 60 dolls per ton.
"Question - The quantity of iron \& cordage to the 100 tons of shipping Answer: It will require 4 tons of iron 1500 lbs copper bolts $41 / 4$ tons of cordage \& 20 bolts of duck to the 100 tons -

In answer to another question to the same society state that "foreign vessels would not have a preference in our ports over American built vessels unless at a reduction in freight of 25 percent or [advantage] equivalent at the port of destination

